

Characterisation of a novel super-polished bimorph mirror

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Outline

- **Motivation & Concept**
- **Metrology testing (Diamond-NOM)**
- **X-ray testing (Beamline B16)**
- **Summary and future**

The “ideal” synchrotron mirror

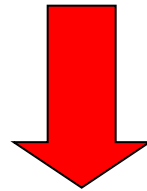
- “Pure” focal spot
 - Ellipse with slope & figure error $\sim 100\text{nrad}$ & $\sim 1\text{nm rms}$
- Adaptive
 - Change focal distance / size
 - Correct upstream optical errors
 - Remove heat-load / mounting deformations

Can this be realised???

“Next generation” adaptive optics

No single technique can provide flexibility & quality, so combine two!

- Super-polished substrate: mid & high spatial frequency roughness (**JTEC**)
- Piezo bimorph (8 channels): figure / slope error (**SESO**)



Adaptive optic with exceptional quality

→ *Micro- & nano-focussing*

Coherence preservation

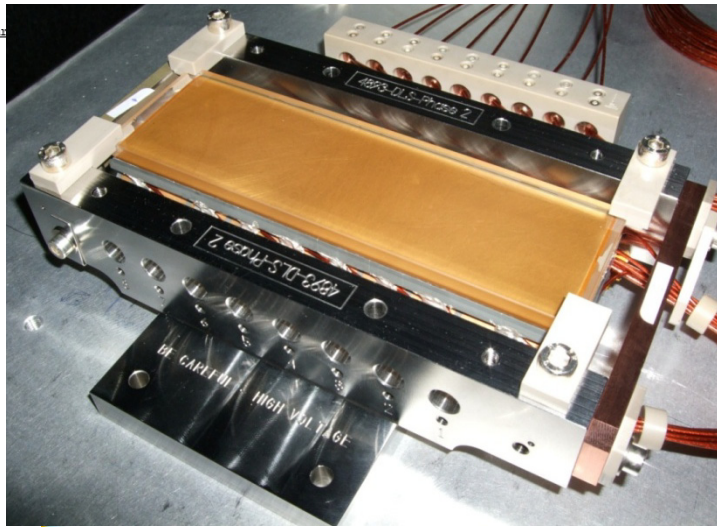
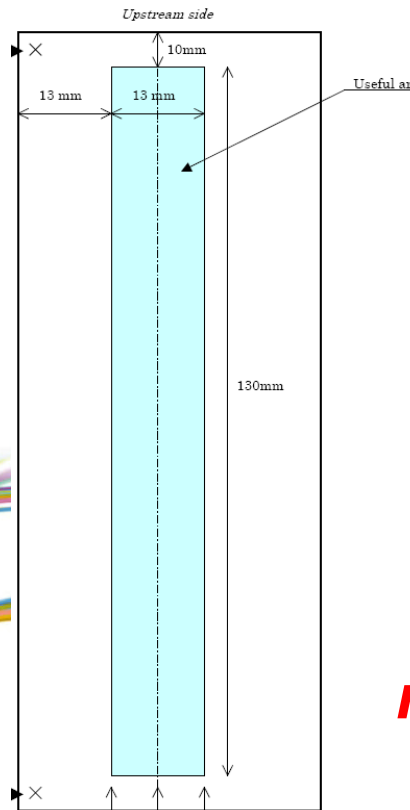
Wavefront correction, ...

Super-Polished Bimorph

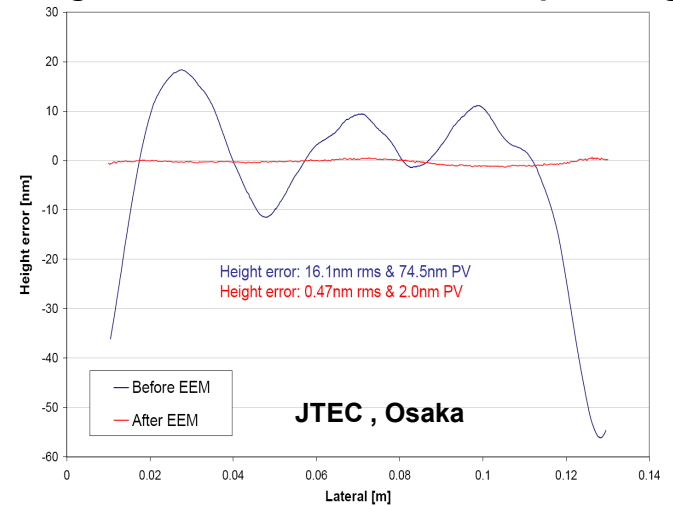
- 8 piezo bimorph (SESO), 150mm long, fused silica substrate
- EEM treatment (JTEC) on central ~120mm

[Figuring with sub nanometre-level accuracy by numerically controlled elastic emission machining, K Yamauchi et al, Rev. Sci. Instrum. **73**, 4028 (2002)]

- Elliptical pre-figure ($p=41.5\text{m}$, $q=0.4\text{m}$, $\theta=3\text{mrad}$)



Height error before and after EEM polishing

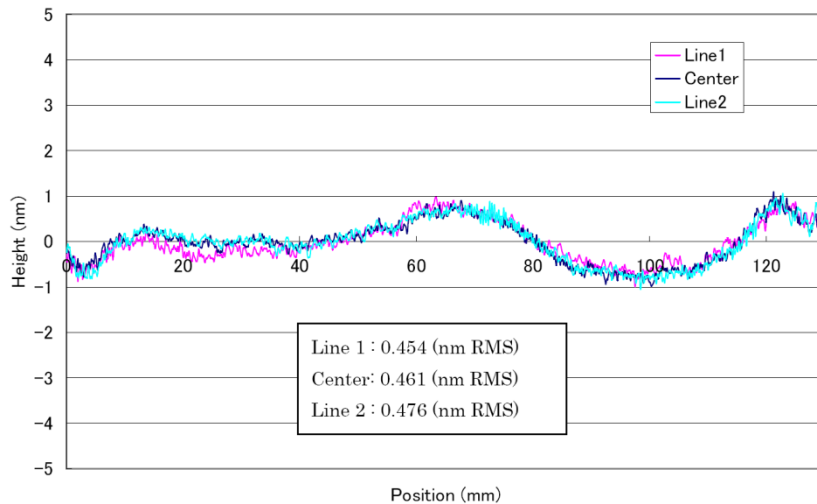


novel super-polished bimorph mirror

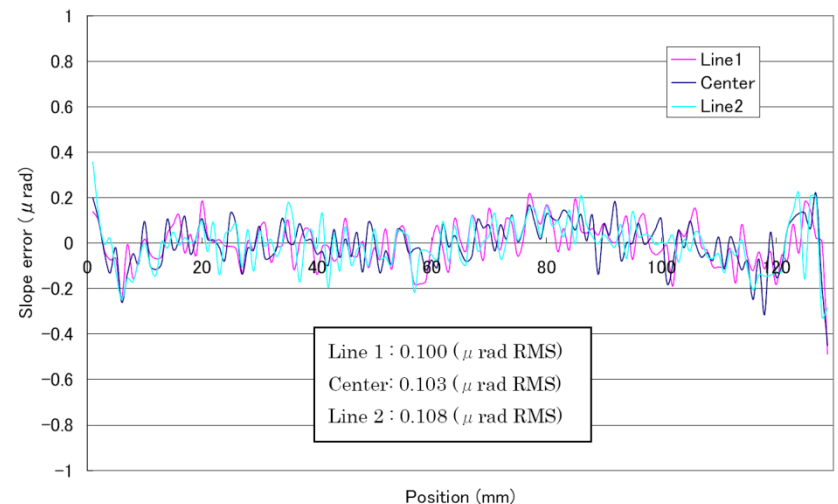


Super-Polished Bimorph

< 0.5 nm rms (< 2 nm PV) height error !



0.1 μ rad rms slope error !



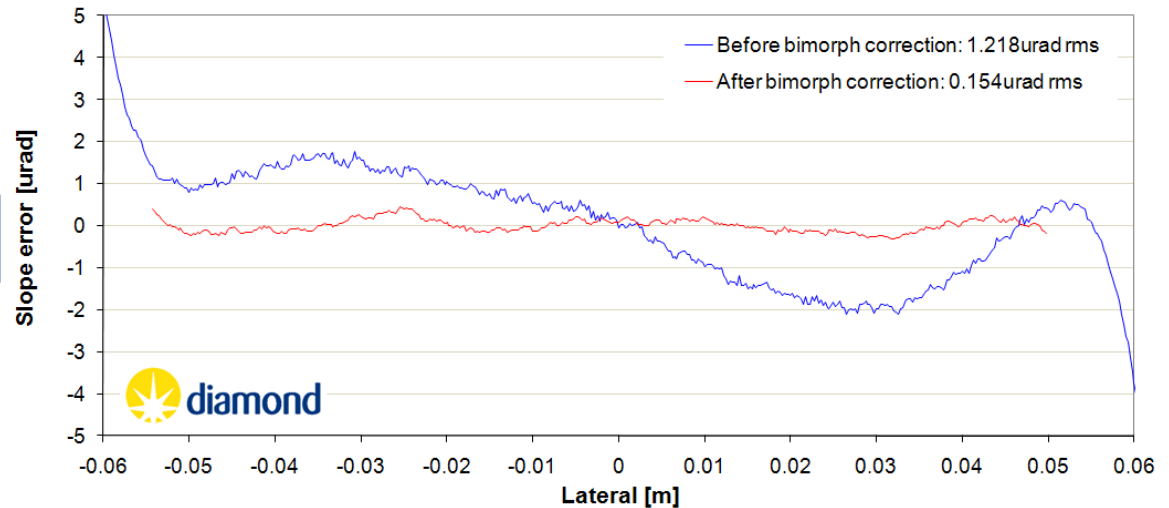
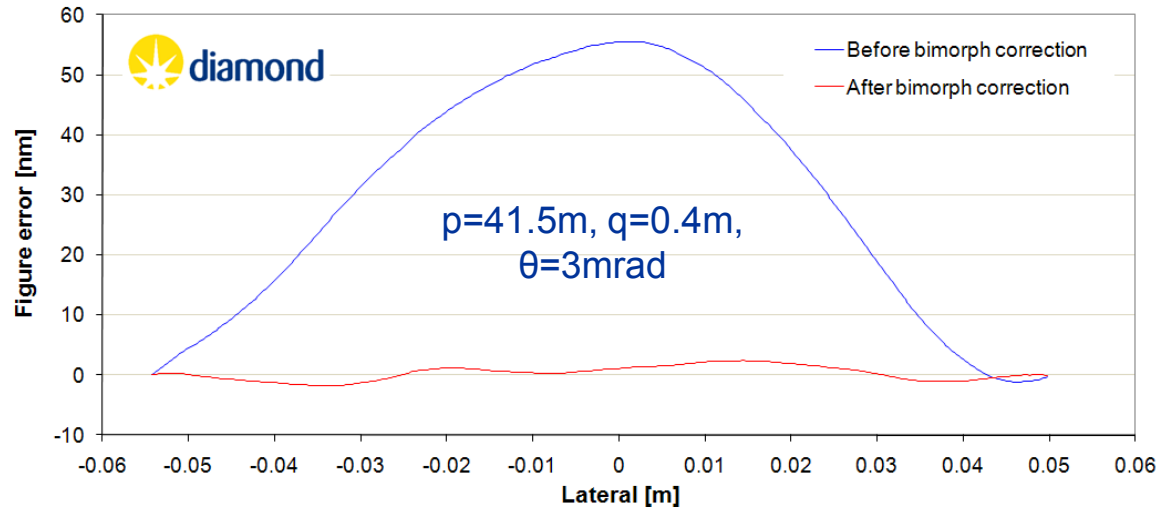
- Error profiles along the tangential direction from the nominal ellipse
- No bimorph corrections applied !

Figure Error

Figure error < 1nm rms

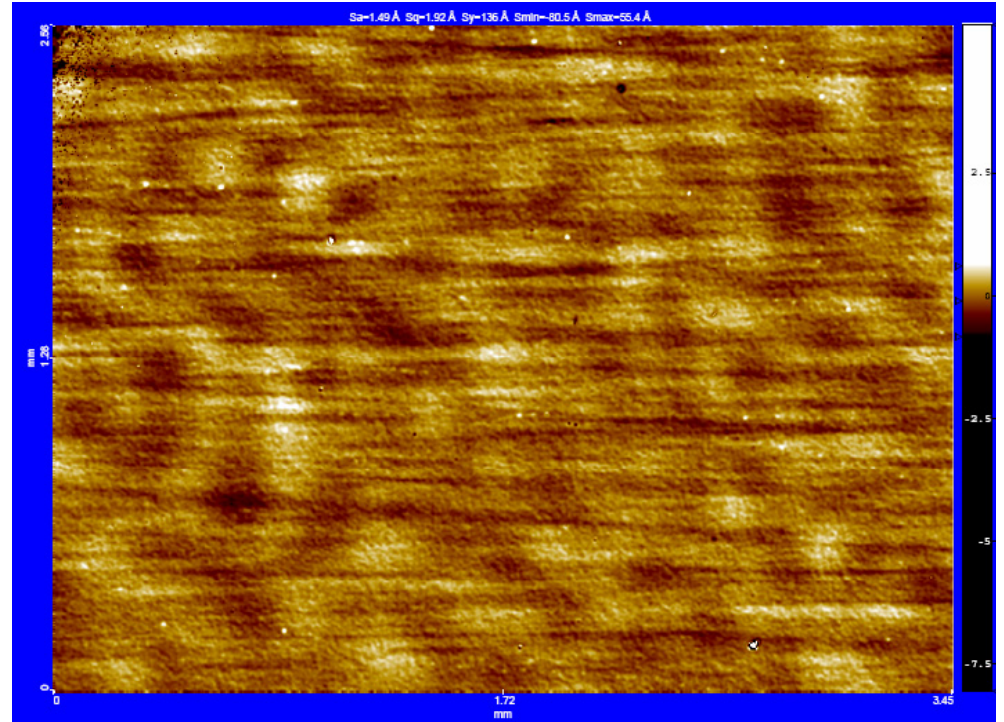
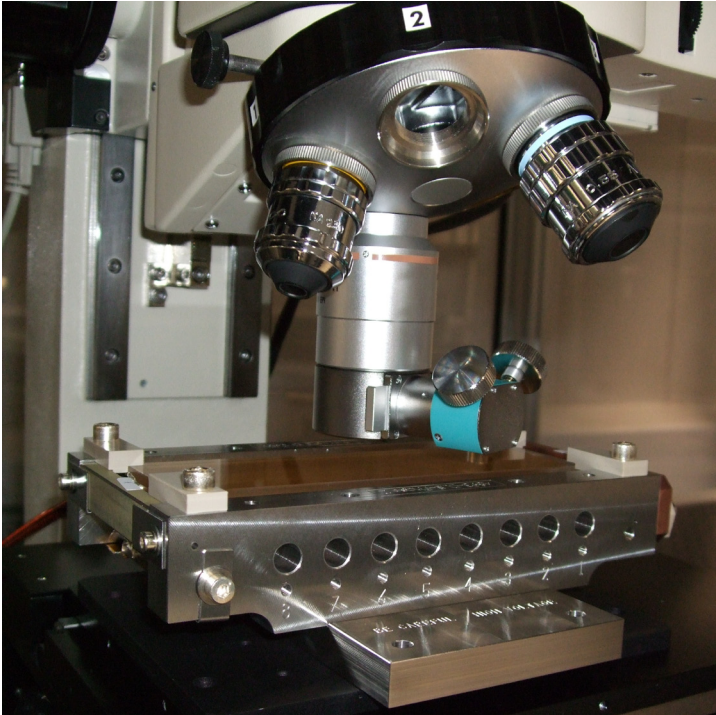
Diamond NOM

Slope error $\sim 0.15 \mu\text{rad rms}$



Micro-Roughness

Diamond Micro-interferometer



Objective

Field of View

EEM region Sq

Non-EEM region Sq

2.5X

3446 x 2563 μ m

1.92 \AA rms

No data

10X

864 x 643 μ m

2.03 \AA rms

1.83 \AA rms

50X

173 x 129 μ m

1.90 \AA rms

1.91 \AA rms

⇒ **No change in micro-roughness by EEM polishing**



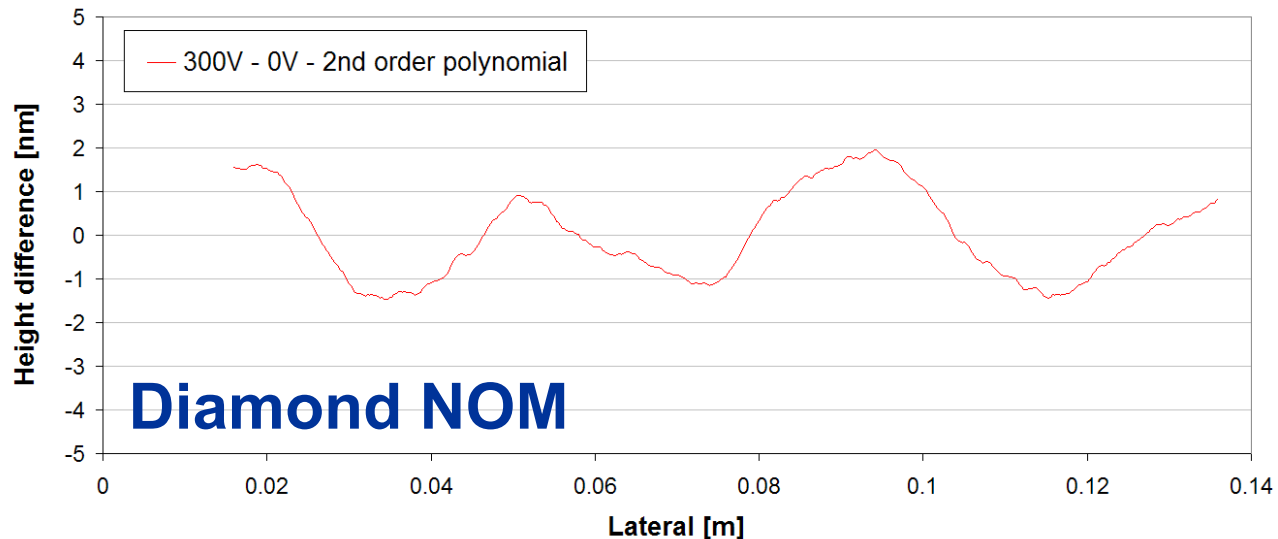
Range of Bending

	1	2	3	4	5	6	7	8	9	10	11
p (mm)	41500	40000	55000	40000	55000	55000	40000	41500	41500	41500	41500
q (mm)	400	400	400	350	350	475	475	290	270	425	200
α (mrad)	3	3	3	3	3	3	3	2,25	2	3,75	1,22
V2 (V)	0	-2	11	-398	-385	484	471	208	450	-740	1336
V1 (V)	0	-2	11	-1345	-1332	1355	1342	-1231	-1172	-1030	-1339

NOMINAL
CONFIGURATION

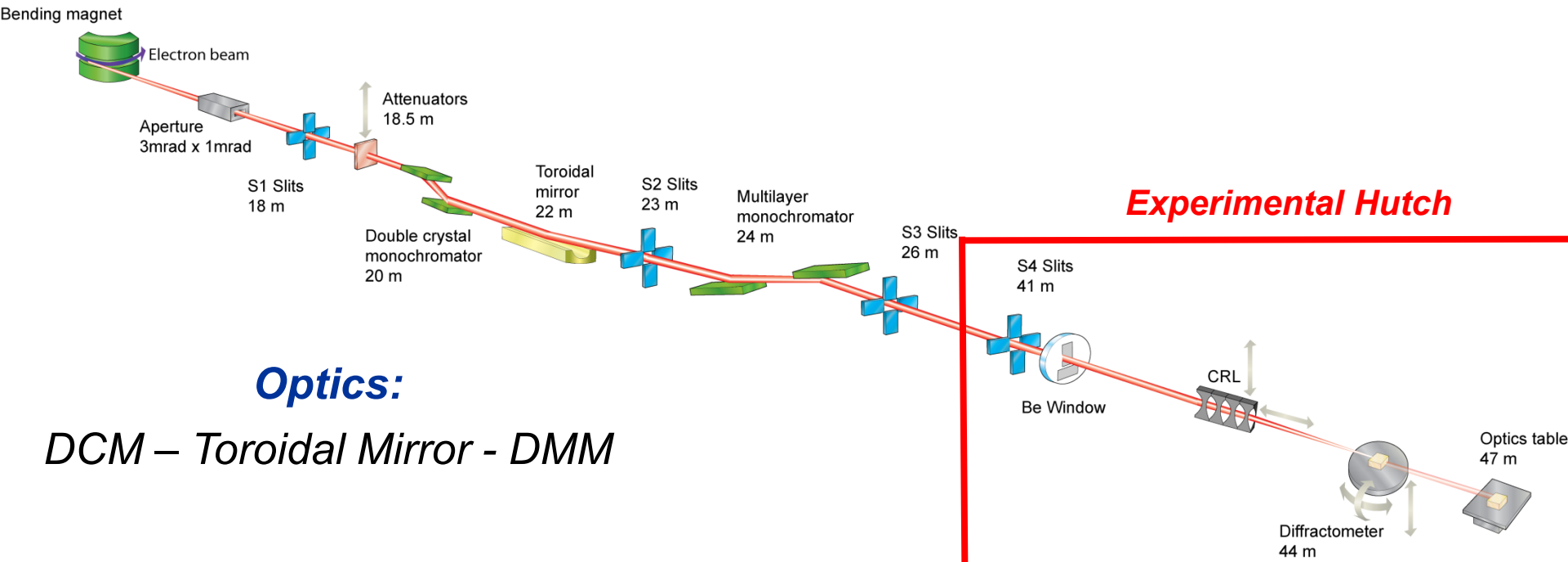
$p = 41.5 - 55m, q = 200 - 400mm, \theta = 1.22 - 3mrad$

Apply 300V. Does figure error worsen? Only by 1nm PV!



B16 Test Beamline

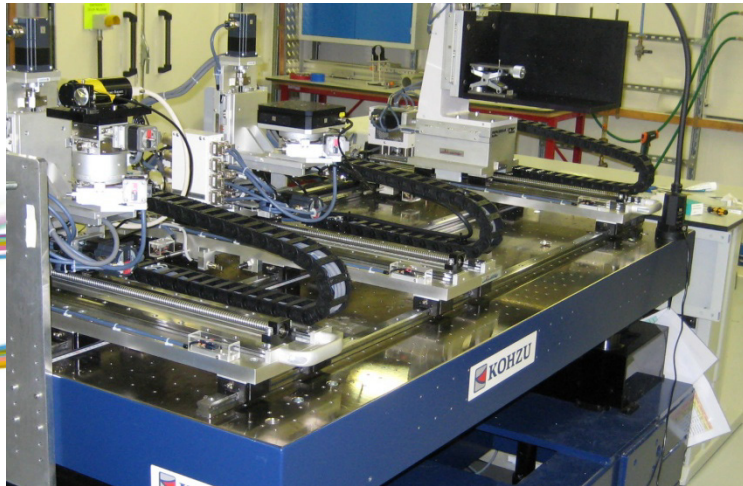
- *For testing optics & detectors*
- *For developing novel experiments & techniques*
 - *Flexibility & versatility to enable wide range of experiments*
 - *Large energy range (2 keV – 25 keV)*
 - *Several operational modes: mono, white, micro-focused, ...*
 - *Range of beam sizes : 1 micron to 100 mm*



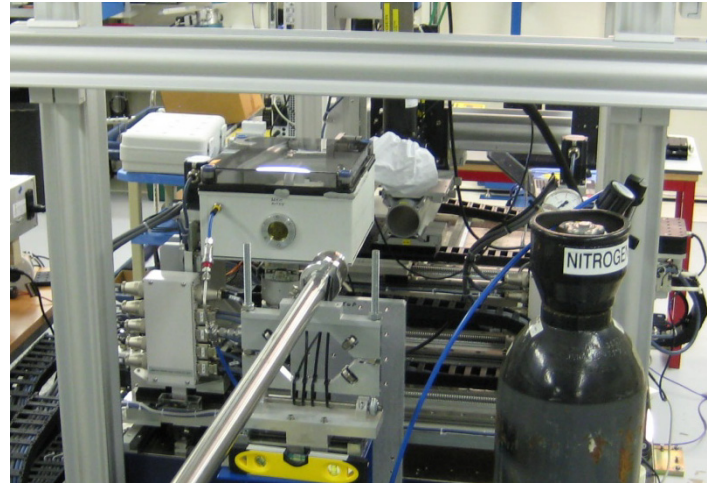
B16 experimental

- Monochromatic, unfocused beam: 8 keV
- Double Multilayer Mono (Ni/B4C) for higher order suppression
- Detectors:
 - Au-wire scan on piezo stage
 - X-ray eye camera (for initial alignment)
 - High resolution X-ray Microscope: (20x objective, 5 μ m-thick Eu:LuAG scintillator, PCO CCD camera, 0.18 μ m effective pixel size)

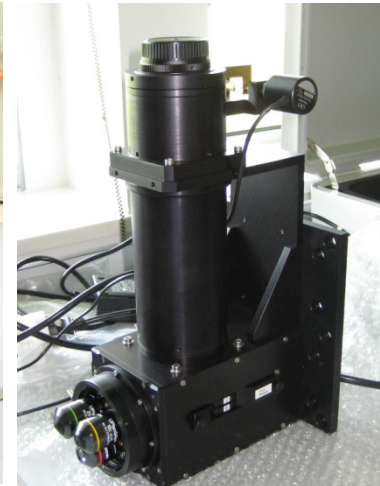
Optics Table



EEM Mirror



“Optique Peter”



Preliminary X-ray Measurements

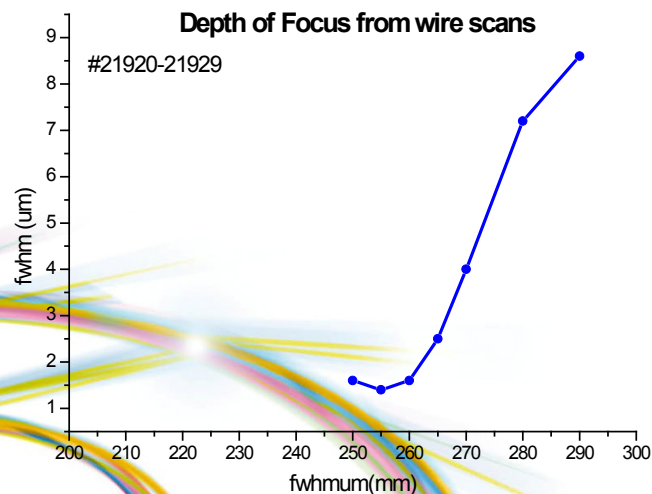
B16

Mirror parameters:

As fabricated : 41.4m 0.3m 3 mrad

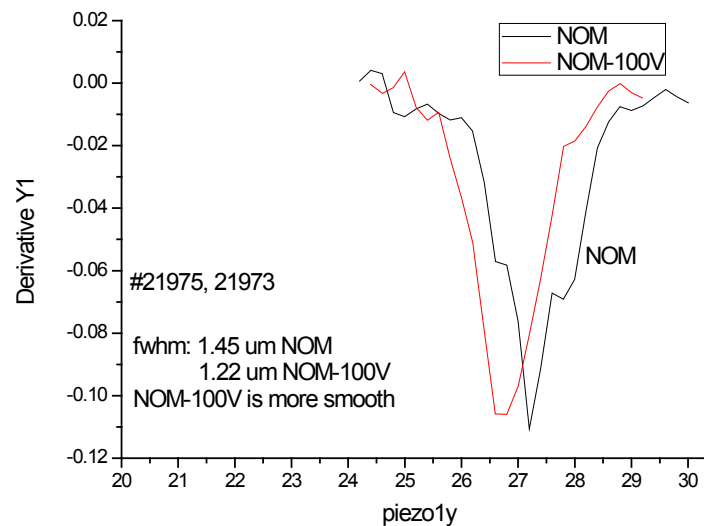
On B16 : **46.5m** 0.3m 3 mrad

Depth of Focus



Variation of Bimorph Voltages

All electrodes -100V of NOM

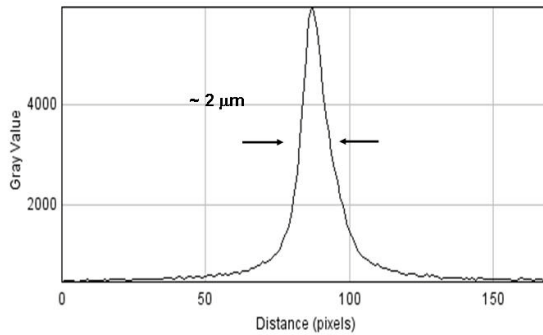
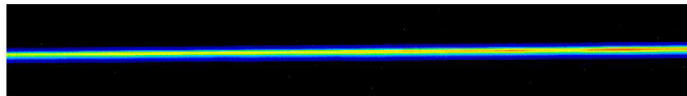


Focal spot $\sim 1.2 \mu\text{m}$ for NOM-100V

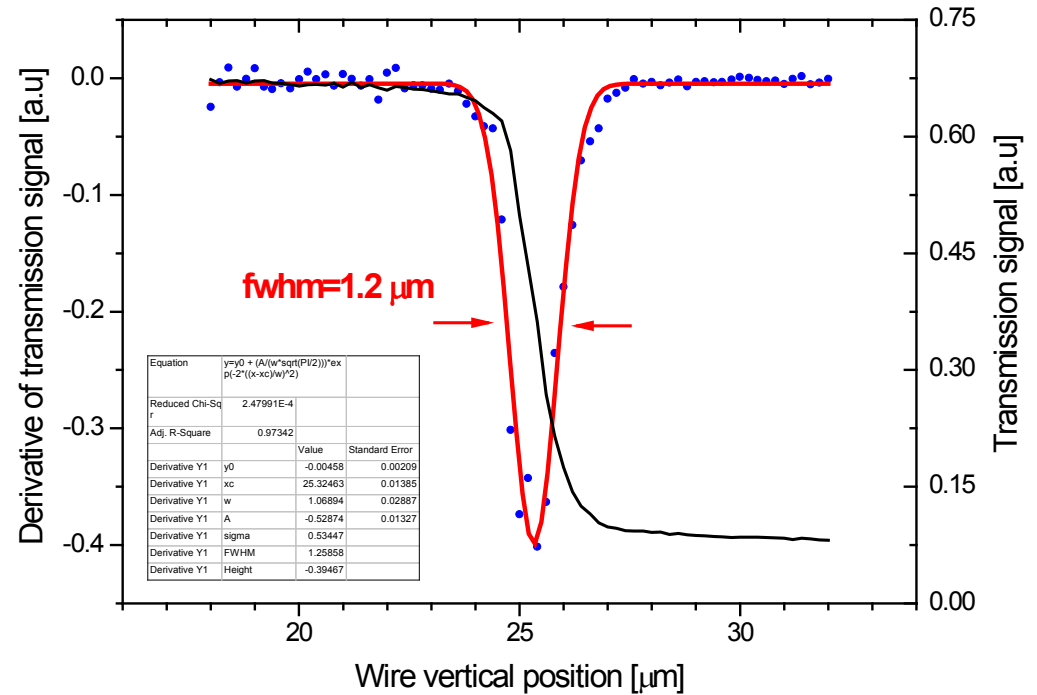
Measured Focus Size

B16

*Image & line profile
using "Optique Peter"
camera*

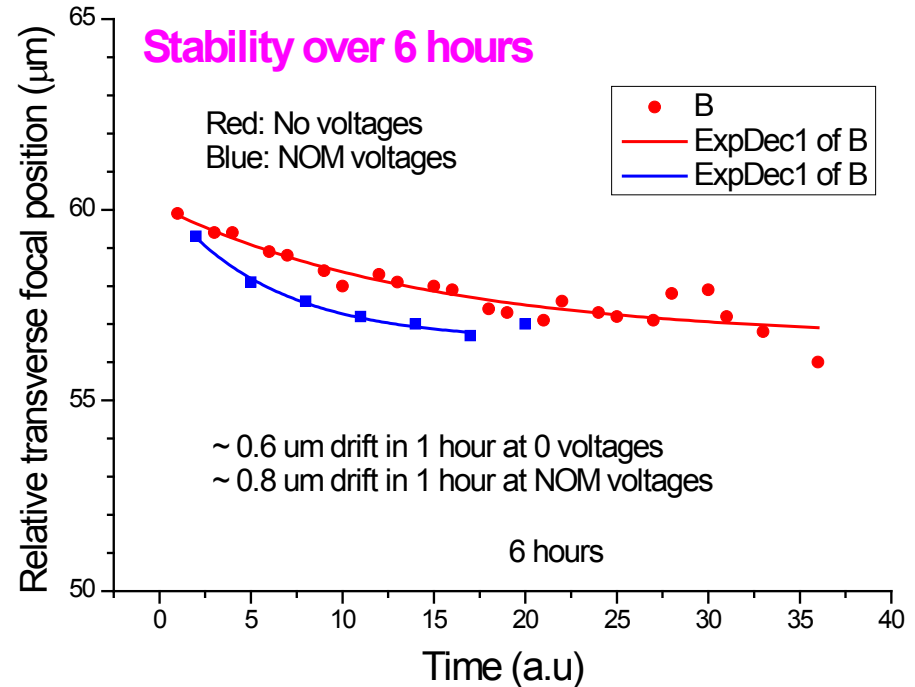
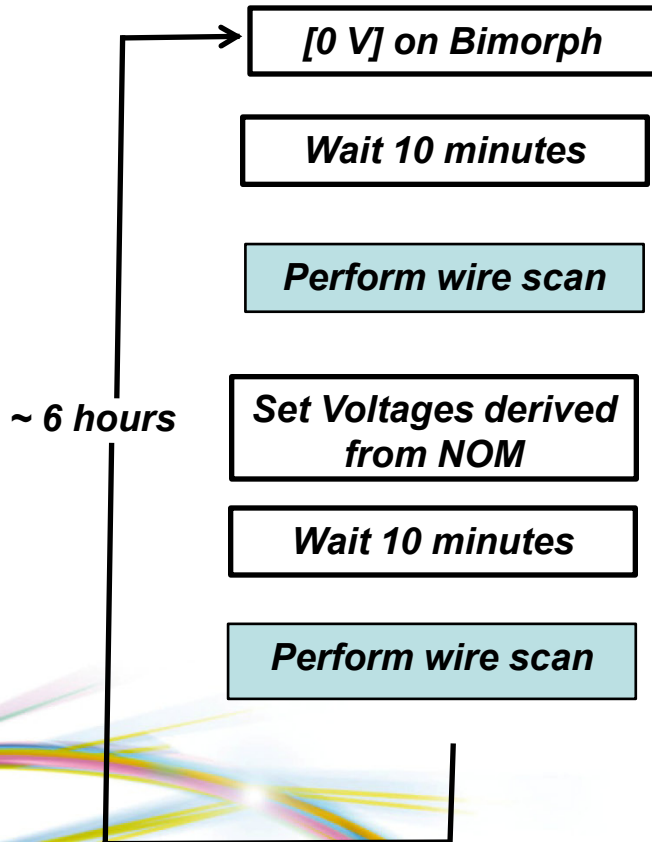


Au wire scan



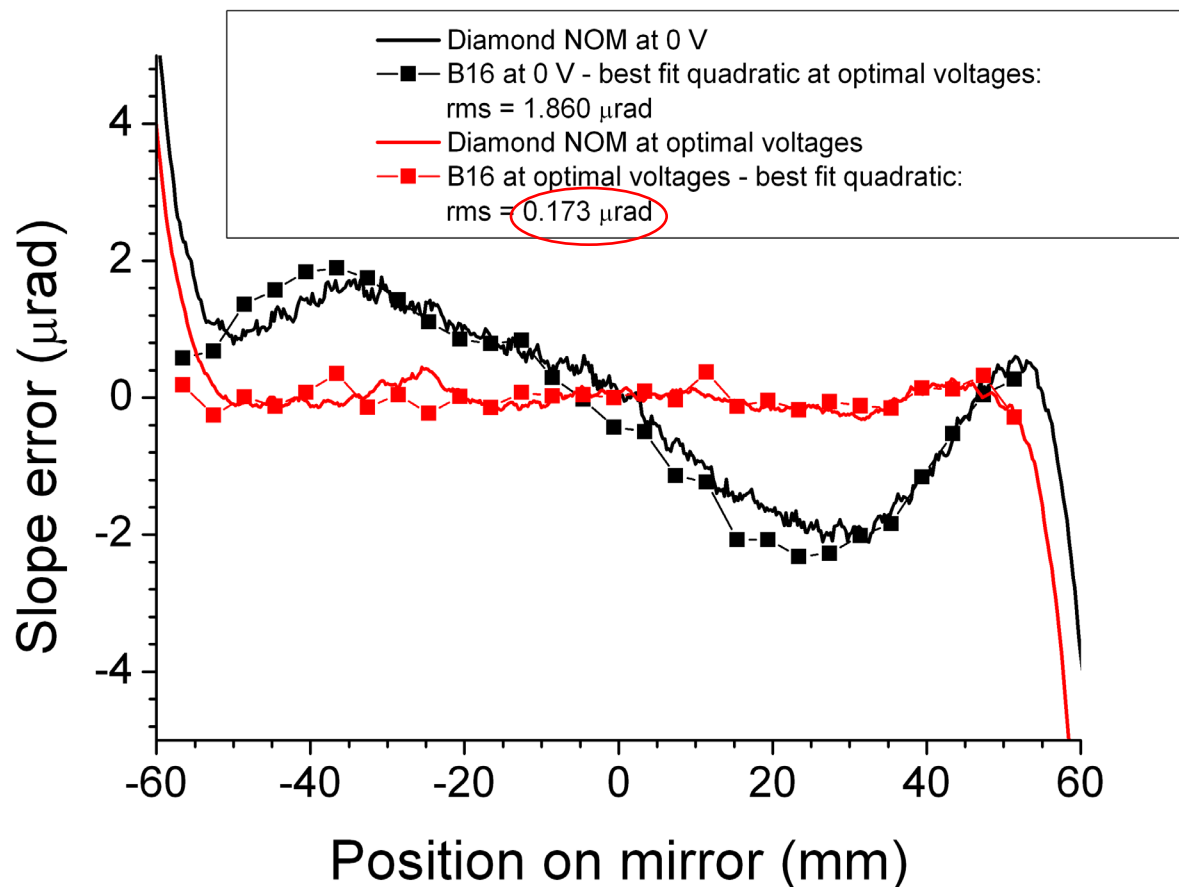
Stability/ Reproducibility Tests

B16



- No change in beam size
- Drift in peak position of $<1 \mu\text{m}$ in 1 hour
- Cause of drift: bimorph / beamline?

- Slope error measured by Diamond NOM and slit scans on B16



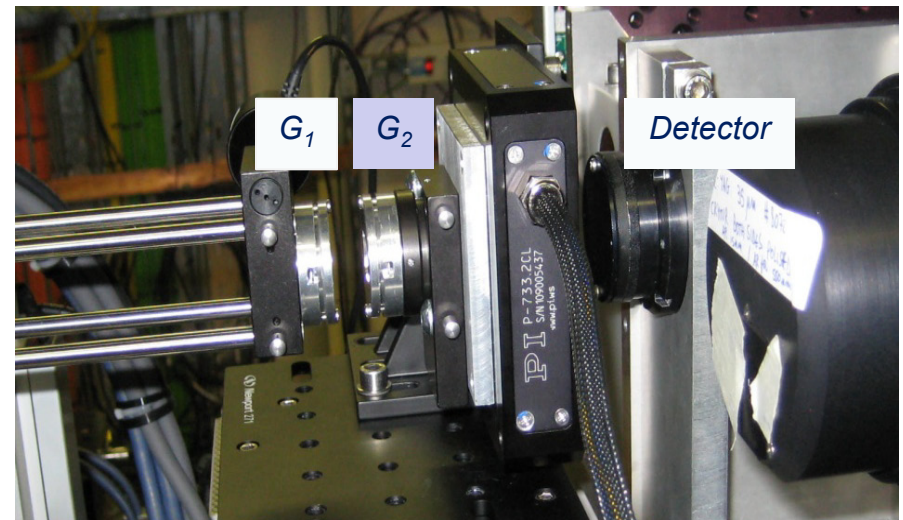
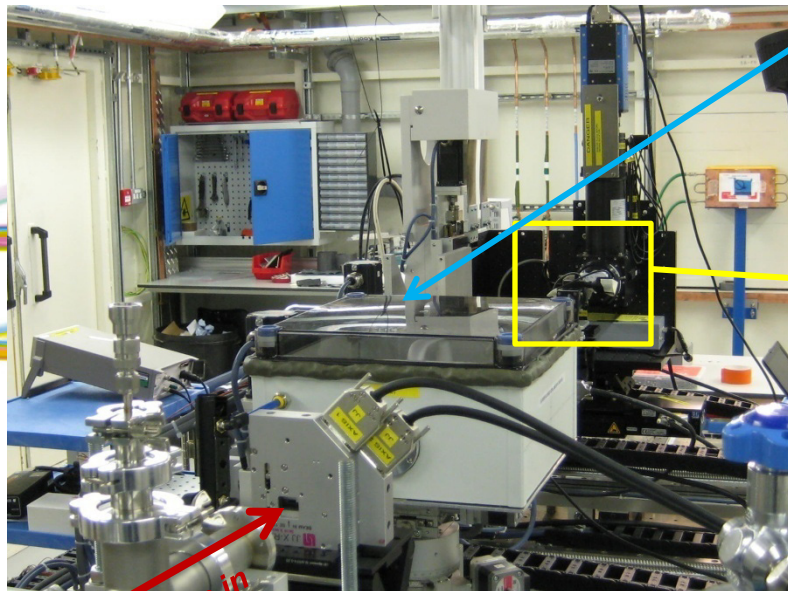
⇒ Good correlation between ex-situ (DLS-NOM) and in-situ (B16) measurements

Wavefront Characterisation using Shearing Interferometer

- Interferometer placed out of focus ($E=14.8\text{keV}$ $\theta=0.05^\circ$)



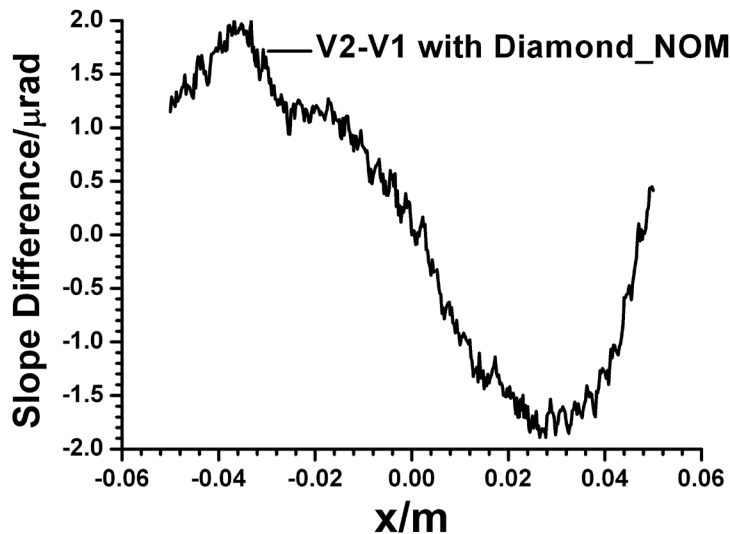
Interferometer



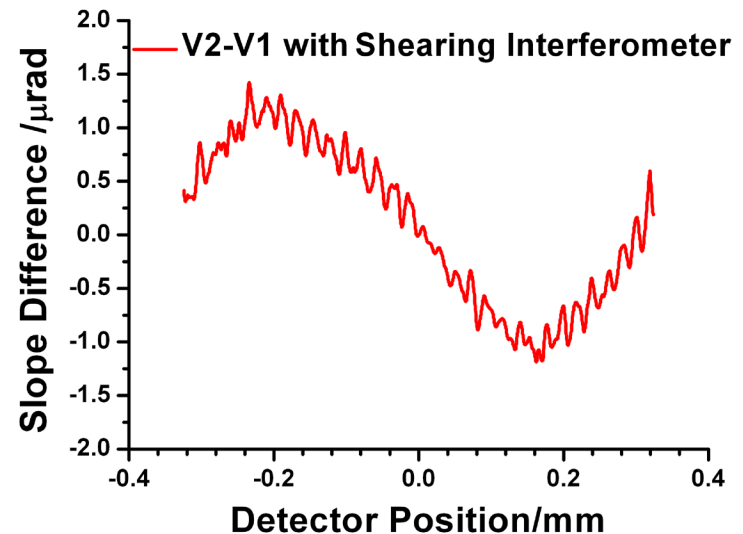
Shearing Interferometer: Moiré Fringe analysis method

- averages data along the whole width foV (~1.4mm)

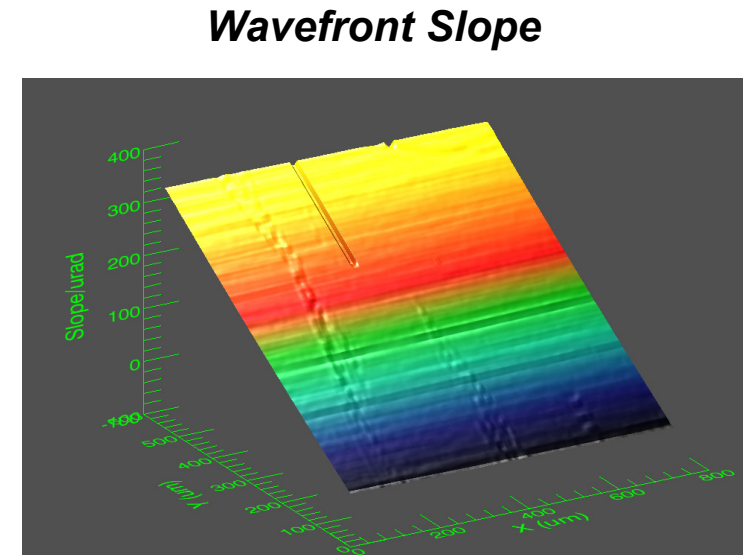
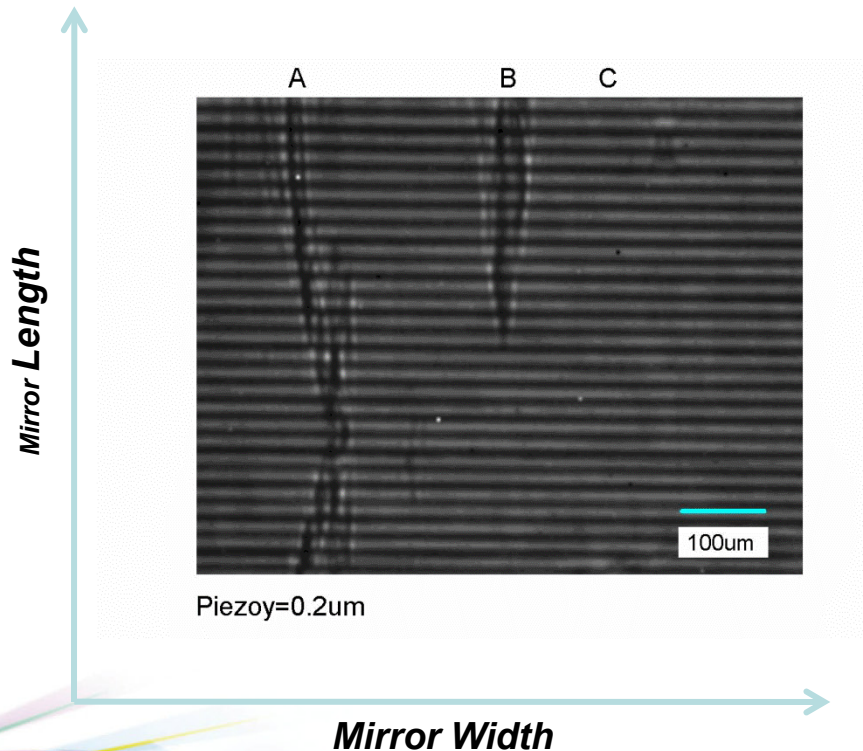
Mirror slope difference tested with Diamond_NOM



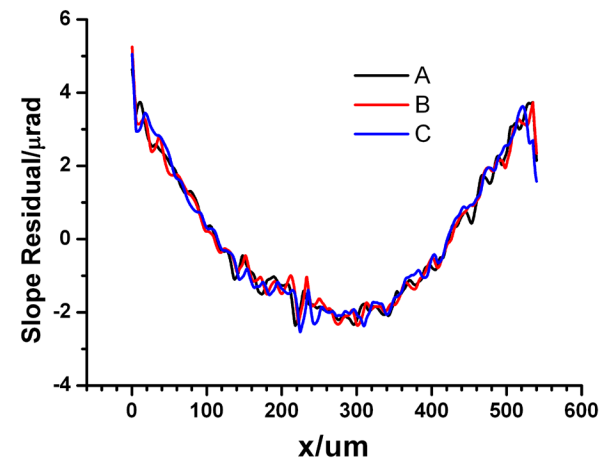
Wavefront slope difference tested with interferometer



Shearing Interferometer: Phase stepping method



- Phase stepping methods give high resolution for detailed information on wavefront
- divergence mismatch of the gratings
- Data still being processed



Summary / Future

- A novel “super-polished” bimorph mirror developed
- Characterised using Diamond-NOM and B16 Test beamline
- EEM gives elliptical shape with exceptional figure and slope error
- Bimorph provides wide range of elliptical shapes & sub-nm figure correction
- Preliminary X-ray tests performed on B16 Test beamline
 - Slit scans, wavefront analysis, ...
- Use an ID beamline
- B16 : vary focal distance
 - : out-of-focus beam (and minimise structures)
 - : Wavefront analysis using shearing interferometer
 - use divergence matched gratings
- More tests on B16 in July 2011

Acknowledgments

- B16: Igor Dolbnya, Andrew Malandain, Slava Kachkanov
- Geoff Ludbrook for micro-roughness data
- Lucia Alianelli
- Christian David, PSI for providing the gratings for the interferometer
- JTEC (Japan) for their expert EEM polishing skills
- SESO (France) for designing & manufacturing high quality, custom-built, bimorph optic
- Sincrotrone Trieste (Italy) for providing state-of-the-art, high voltage, power supply