

HALL MAGNETIC SENSOR DEVICES

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and

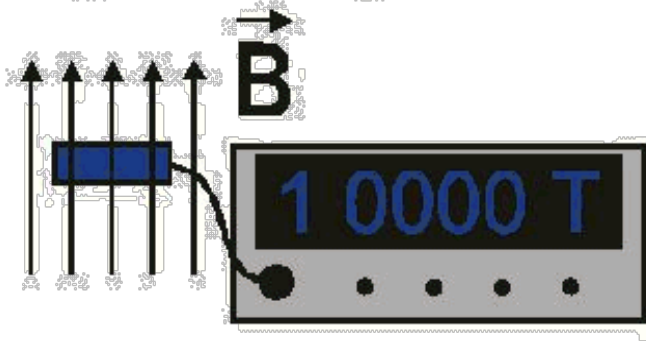
SENIS AG, Zug, Switzerland

Why HALL MAGNETIC SENSORS?

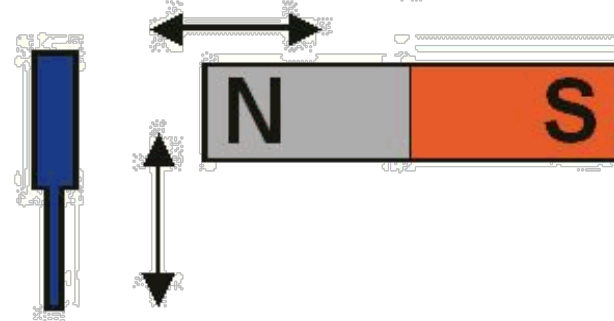
- **High measurement range: from $<10\mu\text{T}$ to $>20\text{T}$**
- **High spatial resolution: $<1\mu\text{m}$**
- **Broad bandwidth: DC to $>1\text{MHz}$**
- **Vector sensitivity**
- **Compatible with IC technologies**
- **Good performance – cost ratio**

Typical Applications of Hall Devices

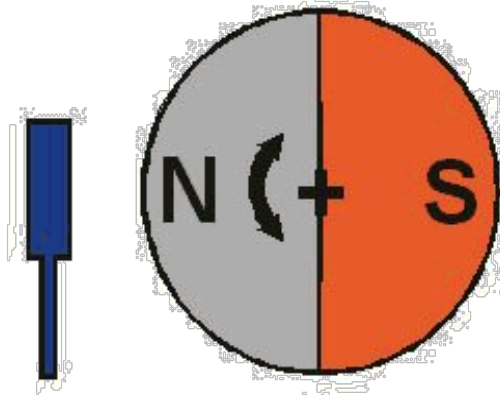
Magnetometry



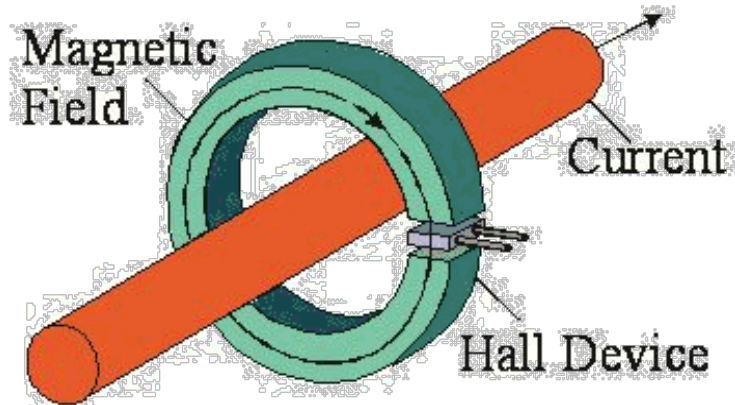
Translation Displacement



Rotary Displacement



Current Measurement



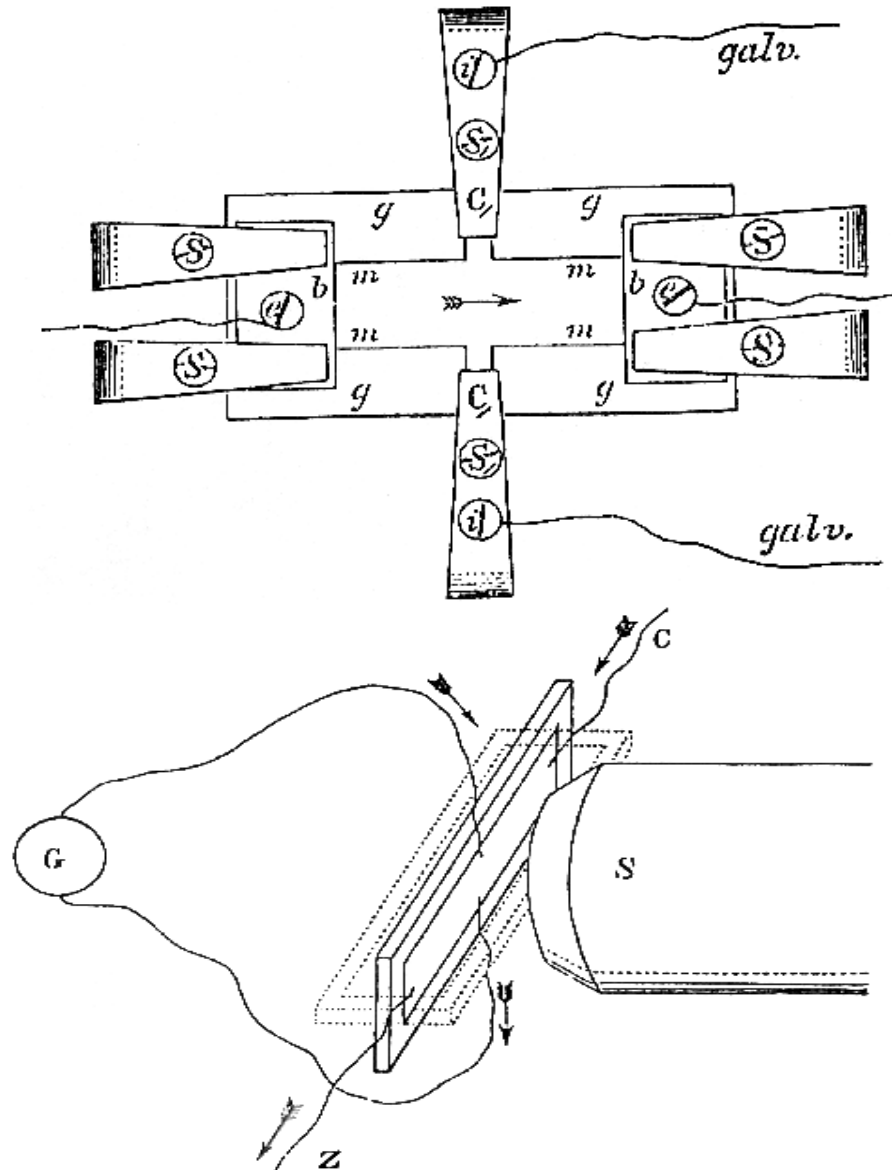
Outline

- **The Hall Effect**
- **Magnetic Sensitivity**
- **Technology and Geometry**
- **Horizontal and Vertical Hall Devices**
- **3-Axis Hall Magnetic Sensor**
- **Parasitic Effects**

The Hall Effect

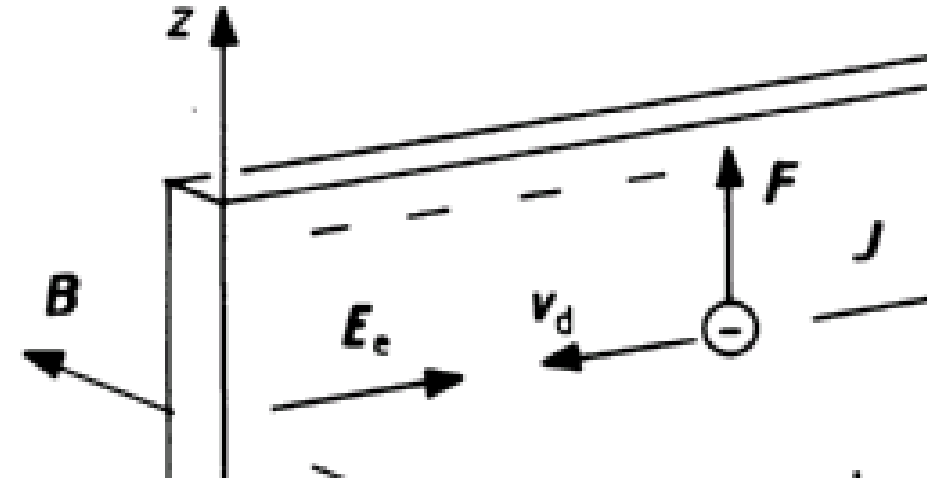
Edwin Hall:

“On a new action of the magnet on electric current” Am.J.Math. 2 (1879) pp.287–92



$$V_H \propto I \cdot B$$

The Hall Electric Field



Lorentz Force: $F = e\mathbf{E} + e[\mathbf{v} \times \mathbf{B}]$

Electron Drift: $\mathbf{v}_{dn} = \mu_n \mathbf{E}_e$

$$\mathbf{J}_n = q\mu_n n \mathbf{E}_e$$

Force || z = 0: $e[\mathbf{v}_d \times \mathbf{B}] + e\mathbf{E}_H = 0.$

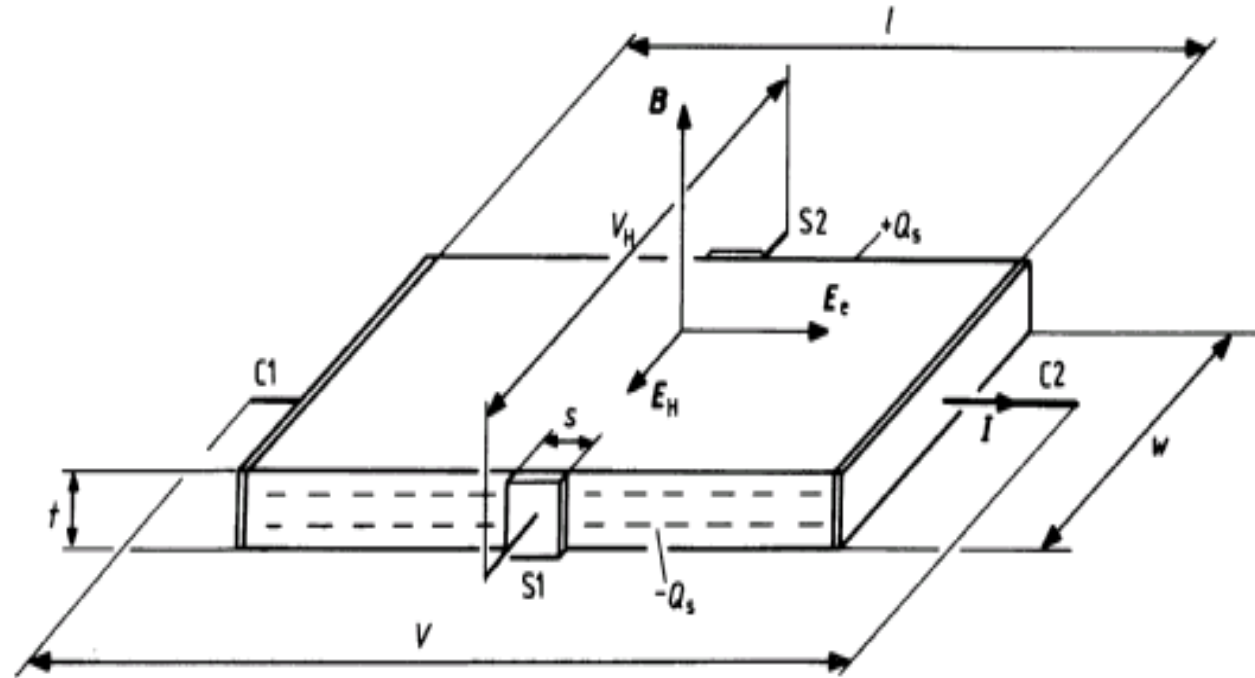
Hall Electric Field: $\mathbf{E}_{Hn} = \mu_n [\mathbf{E} \times \mathbf{B}]$

$$\mathbf{E}_{Hn} = \frac{1}{qn} [\mathbf{J} \times \mathbf{B}]$$

Hall Coefficient: $R_{Hn} = -\frac{1}{qn}$

$$\mathbf{E}_H = -R_H [\mathbf{J} \times \mathbf{B}]$$

Hall Voltage & Magnetic Sensitivity



Hall Voltage: $V_H = \int_{S1}^{S2} \mathbf{E}_H \, dw$

$$V_H = E_H w$$

$$\mathbf{E}_{Hn} = \mu_n [\mathbf{E} \times \mathbf{B}] \Rightarrow V_H = \mu_n \frac{V}{l} w B_{\perp} \Rightarrow V = RI = \frac{1}{q\mu_n n} \frac{l}{wt} I$$

$$V_H = S_V V B_{\perp}$$

$$V_H = S_I I B_{\perp}$$

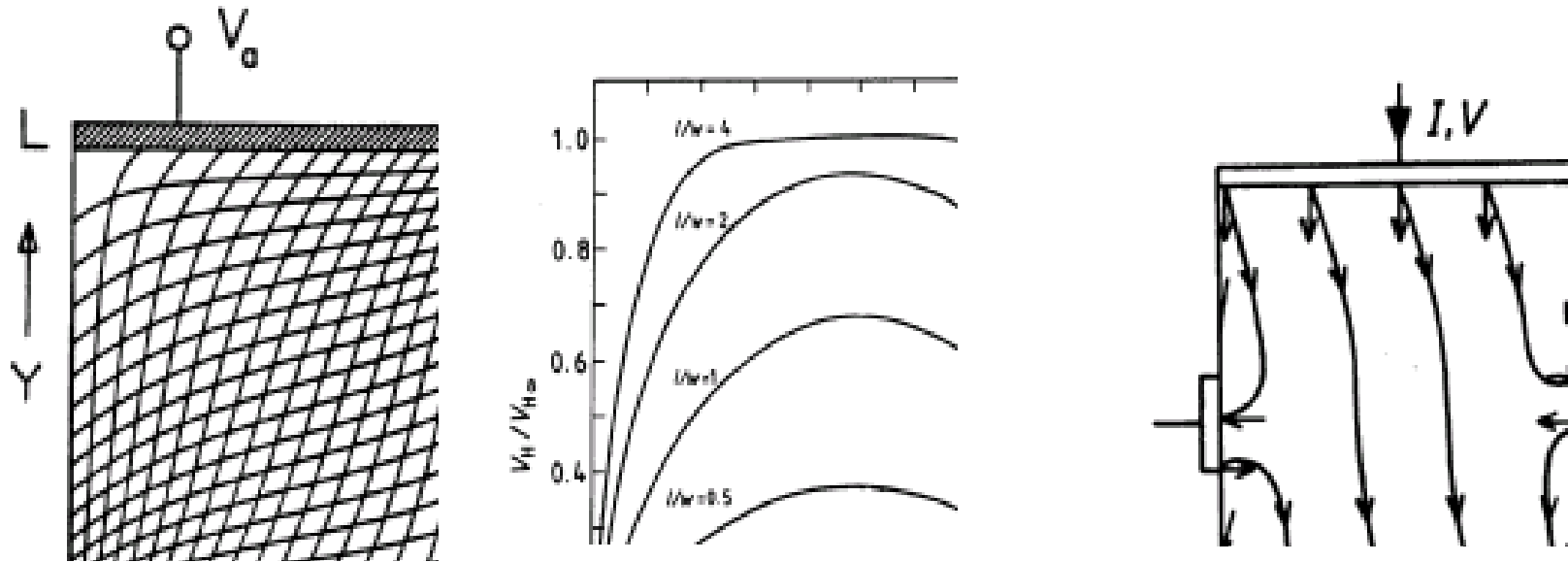
Voltage-Related Sensitivity:

$$S_V \approx \mu_n \frac{w}{l}$$

Current-Related Sensitivity:

$$S_I \approx \frac{1}{q n t} \approx \frac{R_H}{t}$$

Geometrical Factor of Hall Voltage



Short – circuiting effects by the electrodes!

$$G_H = V_H / V_{H\infty} \quad \rightarrow \quad V_H = G_H \frac{R_H}{t} I B_{\perp}$$

Typically, $G_H \approx 0.3 \dots 0.7$

Magnetic Sensitivity

- Absolute Sensitivity: $S_A = \left| \frac{V_H}{B_{\perp}} \right|_c$

- Relative Sensitivity

Current-related:

Voltage-related:

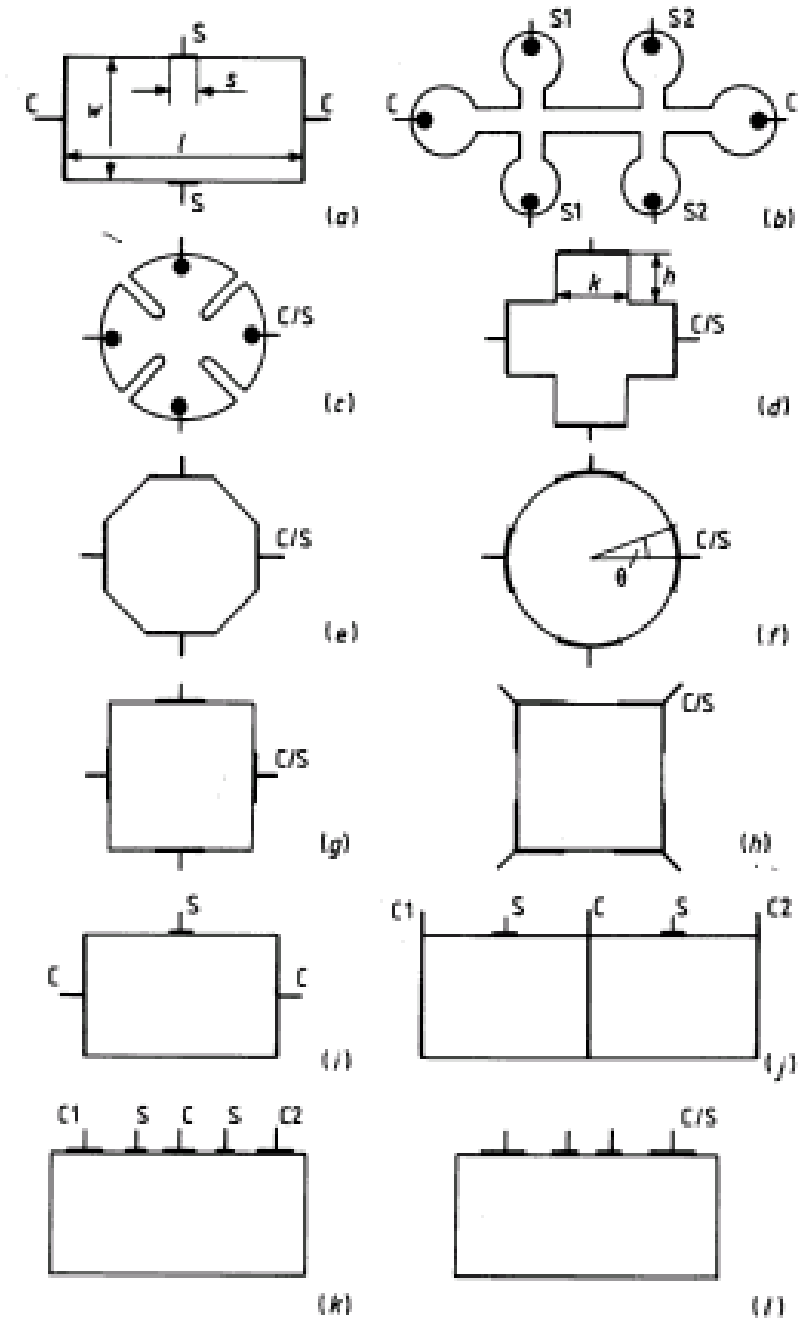
$$S_I = \frac{S_A}{I} = \left| \frac{1}{I} \frac{V_H}{B_{\perp}} \right| \quad S_V = \frac{S_A}{V} = \left| \frac{1}{V} \frac{V_H}{B_{\perp}} \right| = \frac{S_I}{R_{in}}$$

$$S_I = G_H \frac{|R_H|}{t} \quad S_V = \mu_H \frac{w}{l} G_H$$

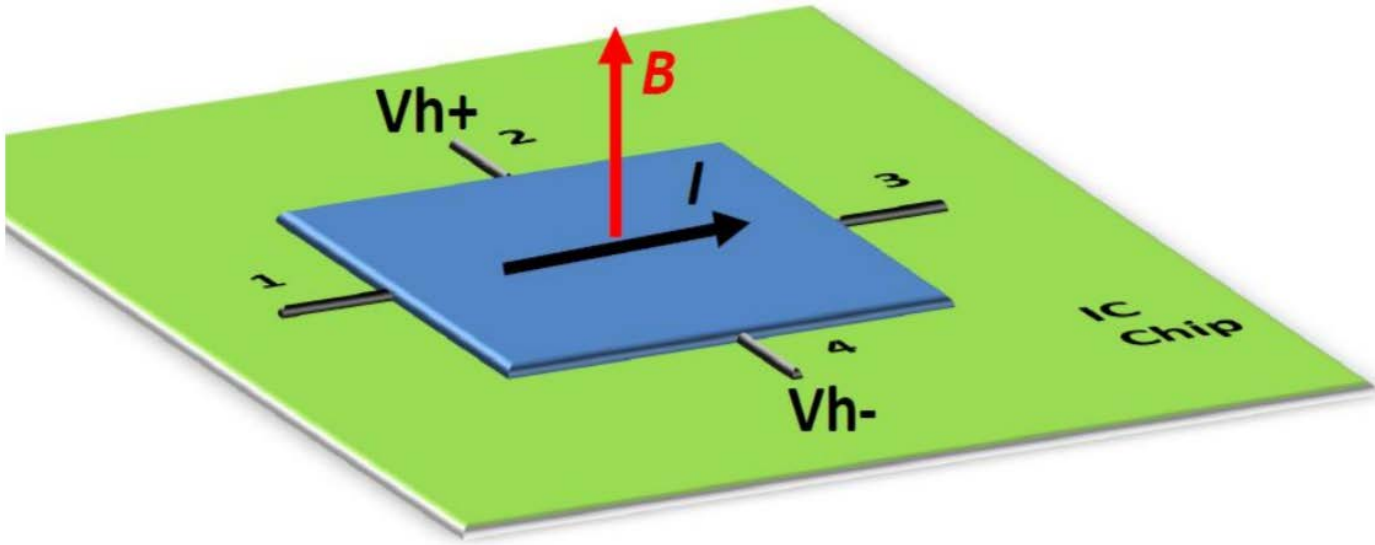
S_I [V/AT]: 10 ... 1000

S_V [V/VT]: 0.01 ... 0.05 (Si CMOS); 0.3 (GaAs); 1 ... 5 (InSb)

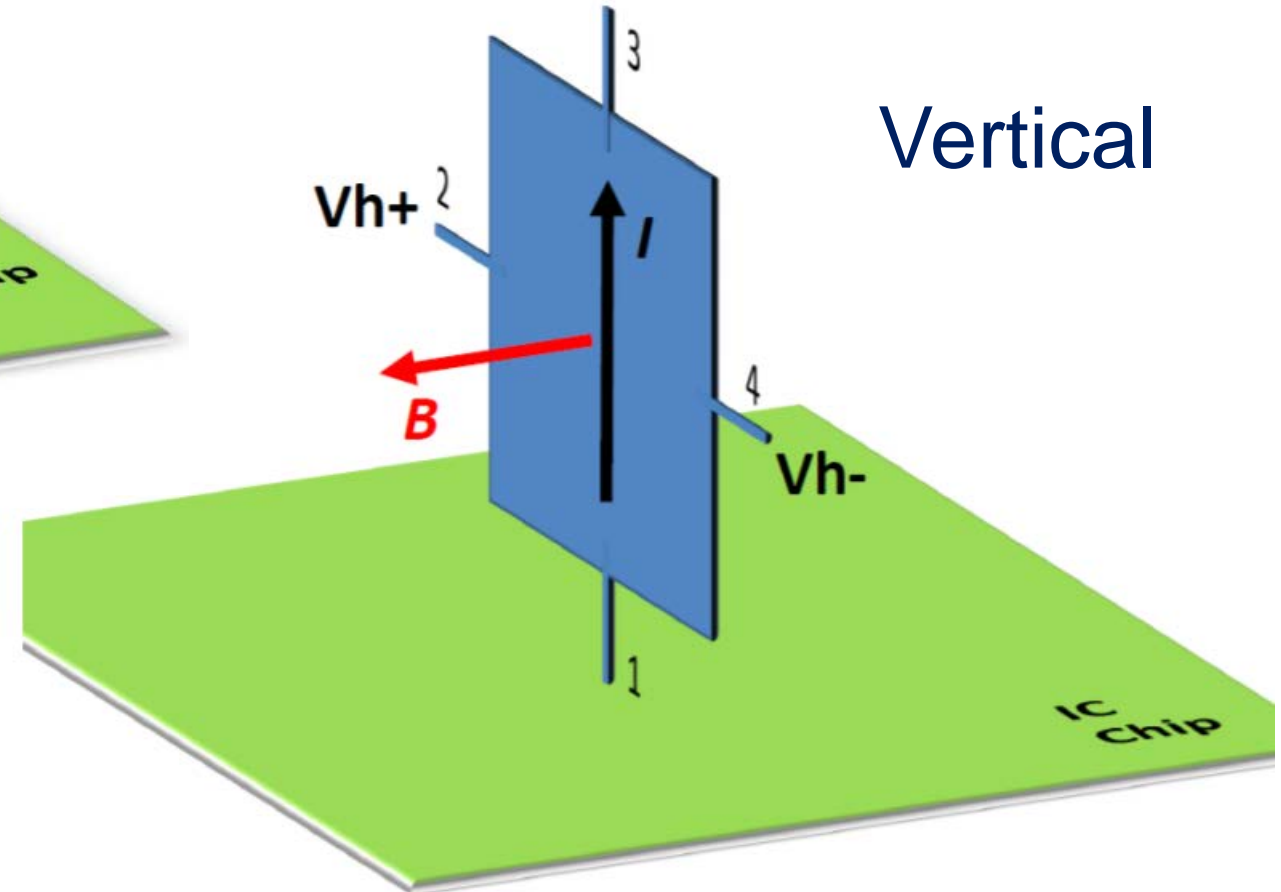
Shapes of Hall Devices



Positions of Hall Devices

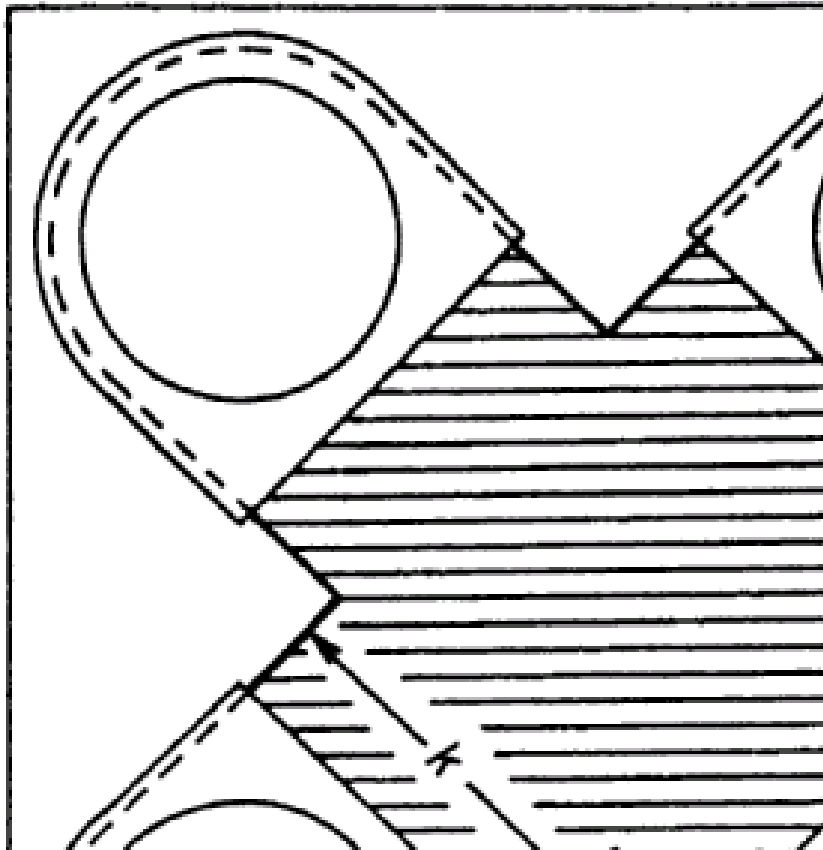


Horizontal



Vertical

GaAs Hall Device



1 : GaAs – active area

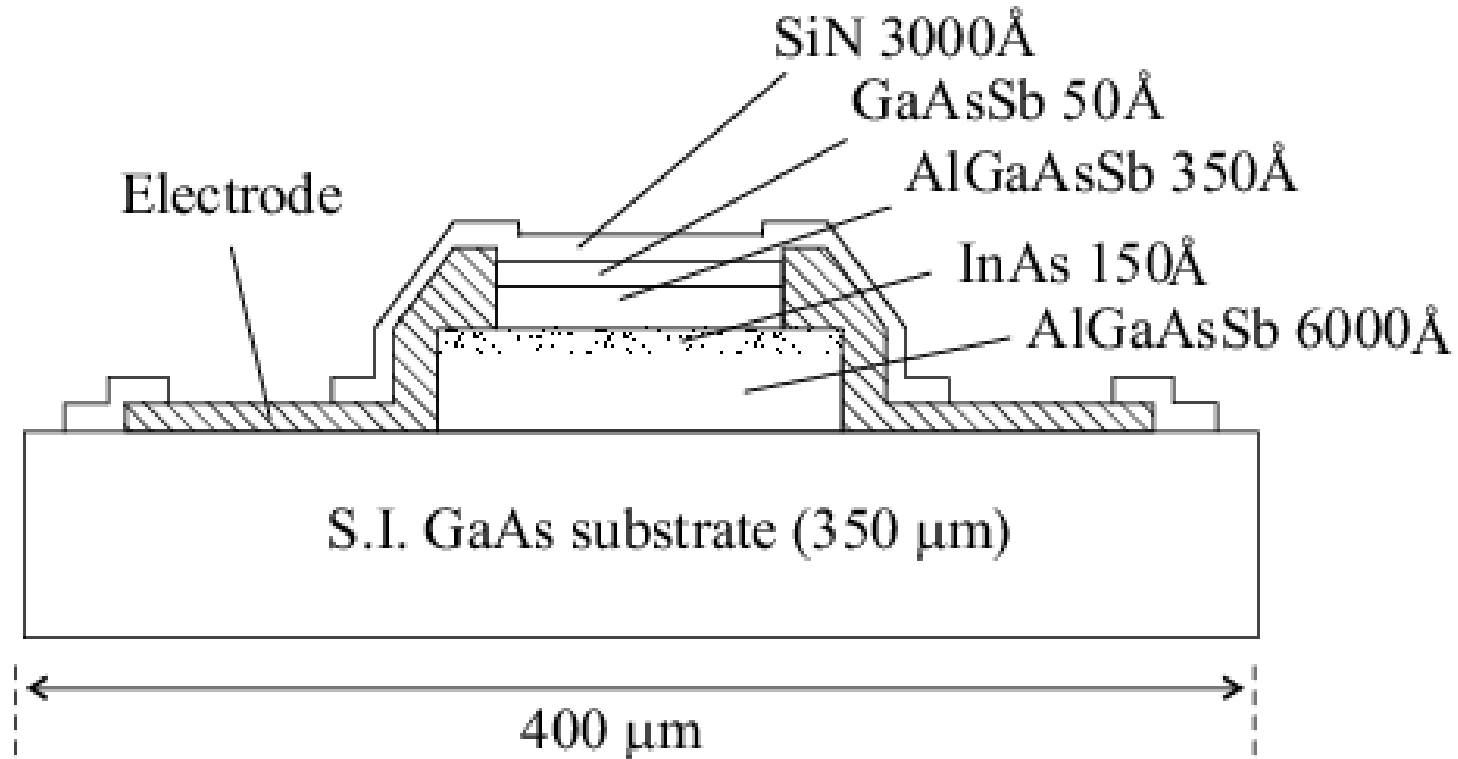
2 : Metalized region

3 : Contact region

Desired features of (1):

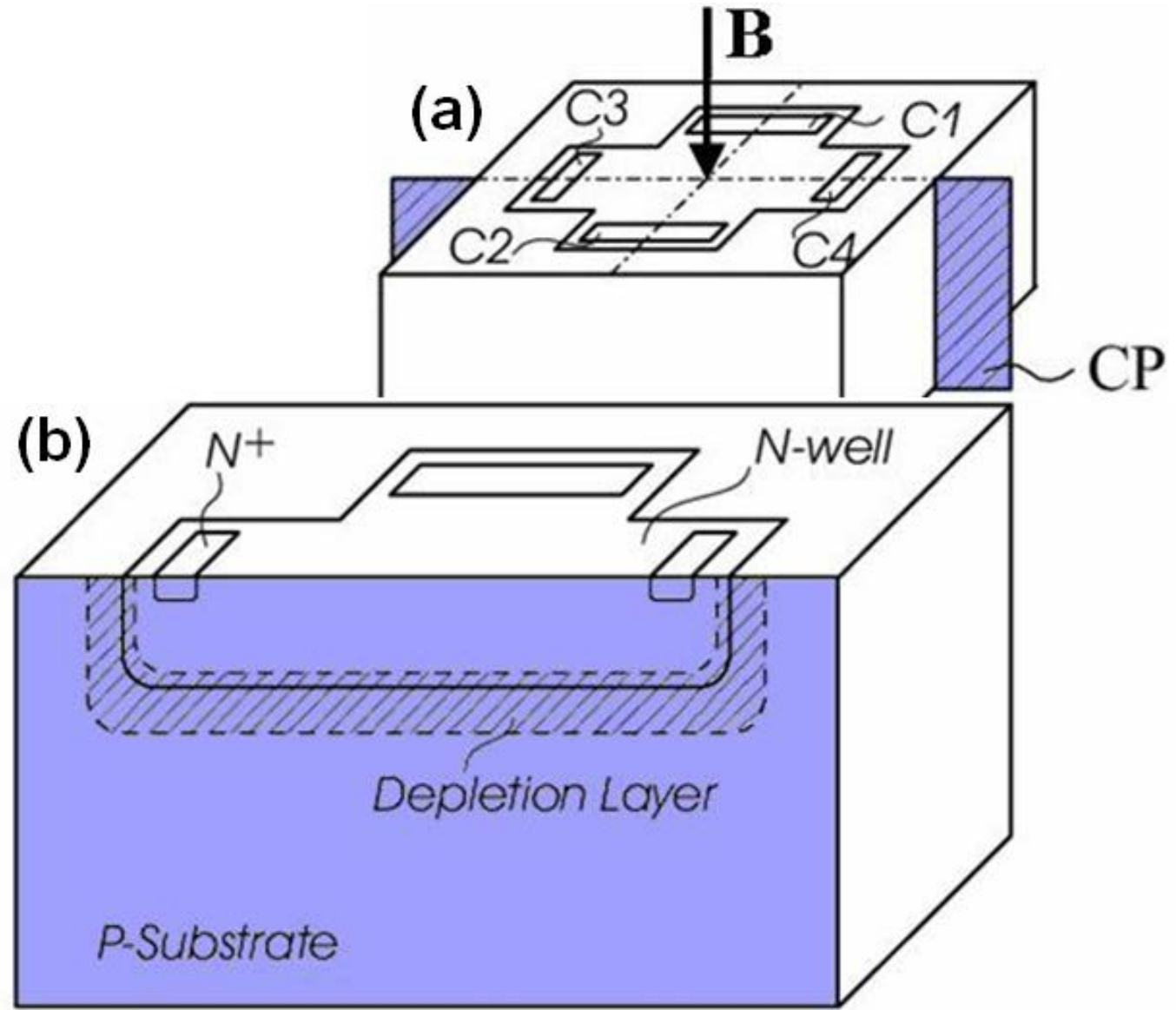
- High mobility
($\mathbf{E}_H = \mu [\mathbf{E} \times \mathbf{B}]$)
- Low carrier density
($\mathbf{E}_H = (1/qn) [\mathbf{J} \times \mathbf{B}]$)

High-mobility 2DEG Hall plate

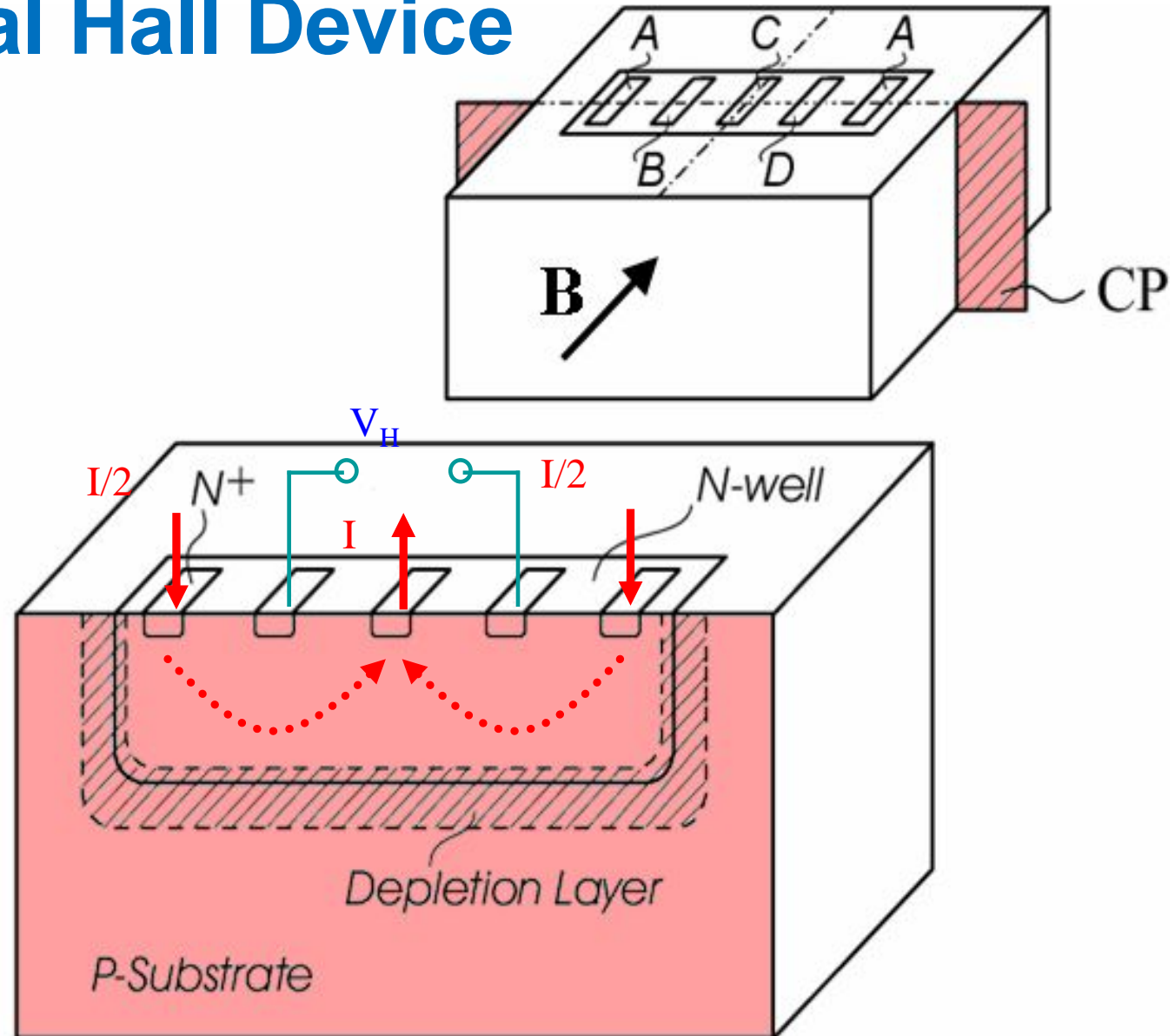
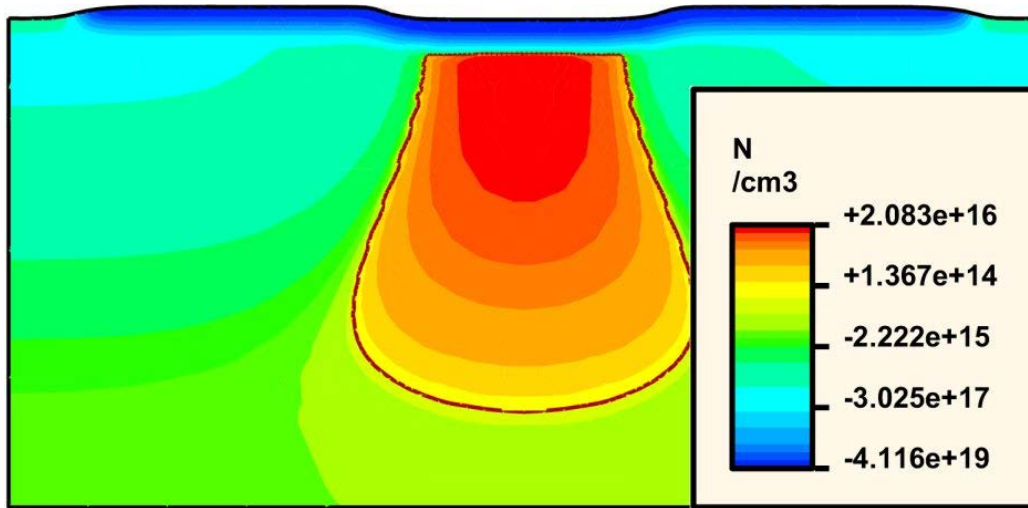


Silicon (Horizontal) conventional planar in Hall Device

- Sensitive to the perpendicular field component **B**
- CMOS Technology:
N-Well
- Depletion layer isolation

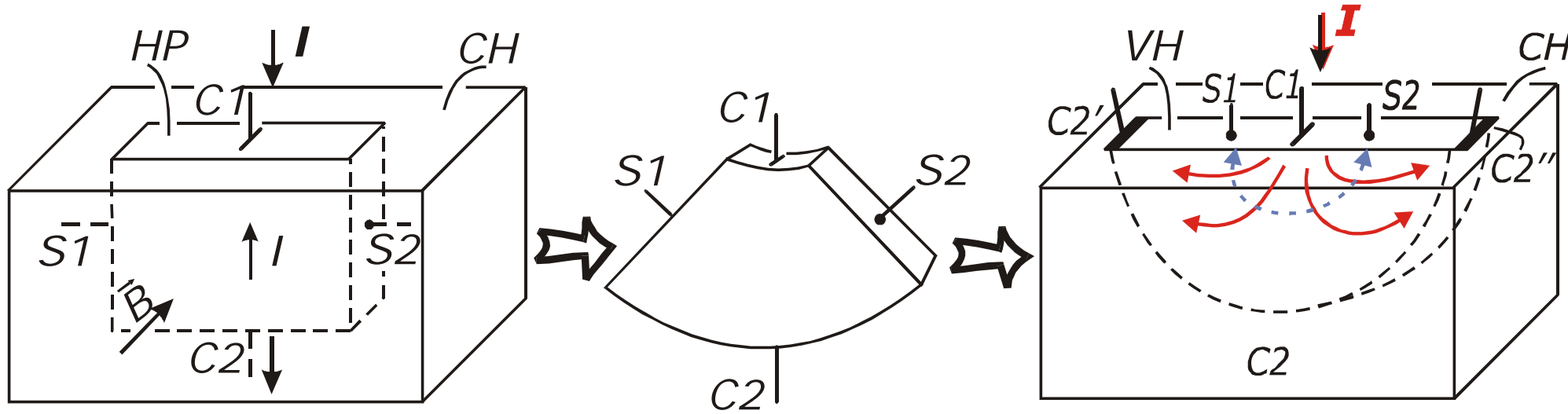


Silicon integrated Vertical Hall Device

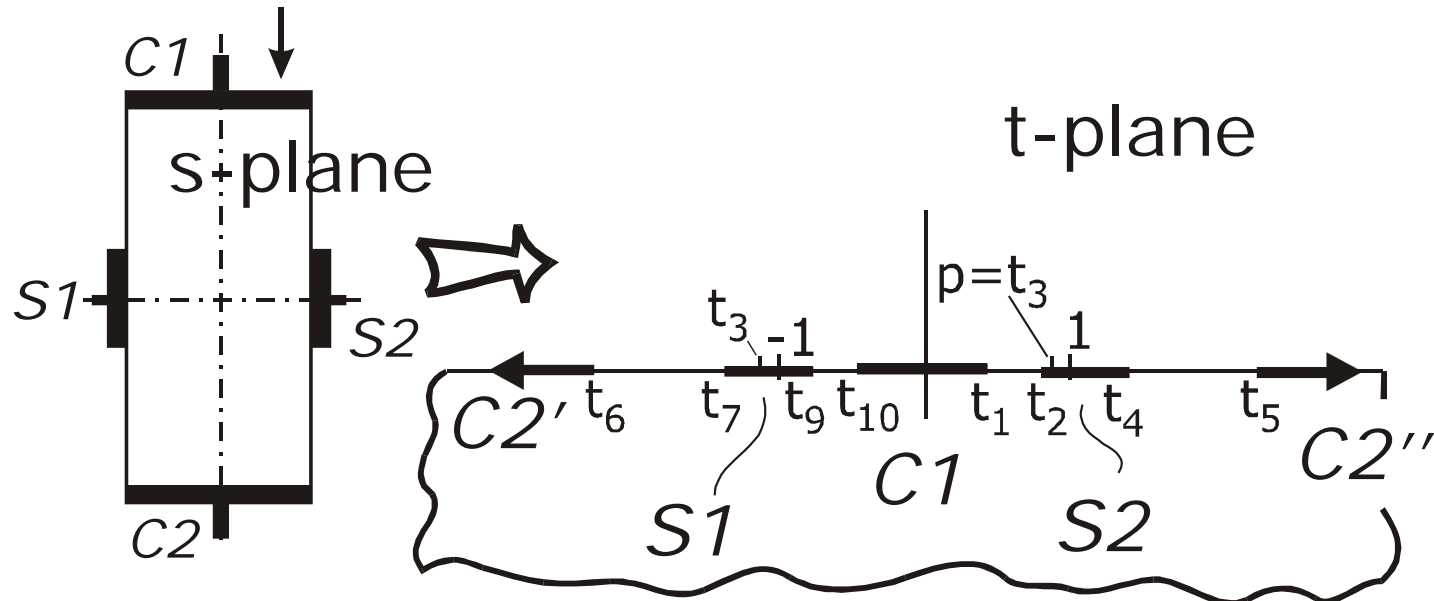


- Sensitive to in-plane field component B
- CMOS Technology: N-Well
- Depletion Layer Isolation

INTUITIVE: GENESIS OF THE VERTICAL HALL DEVICE

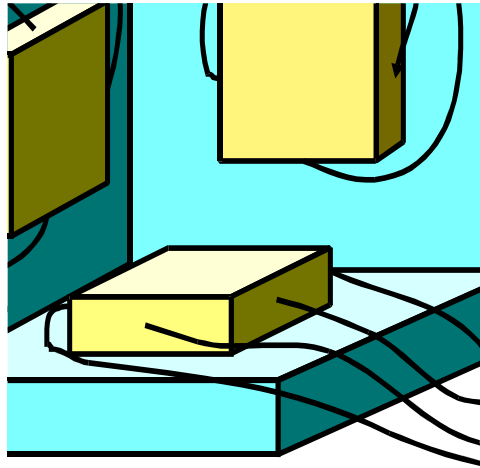


**BY
CONFORMAL
MAPPING:**



Multi-axis Hall magnetic sensors

Conventional: 3 Hall plates



- difficult alignment of axes
- pure spatial resolution
- many wires

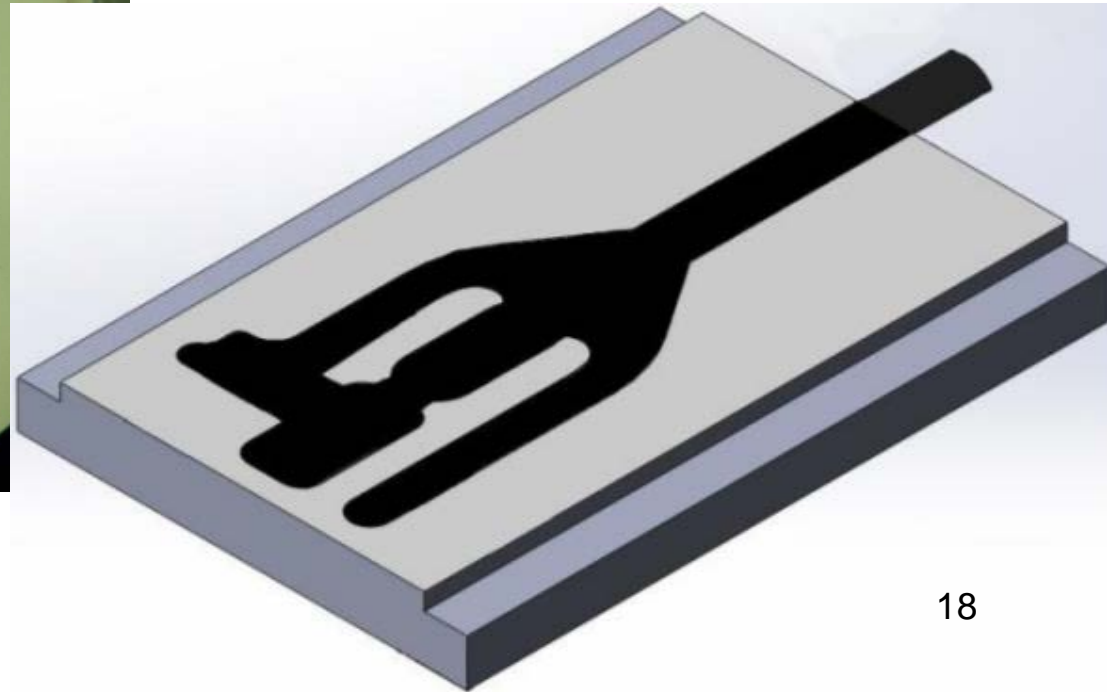
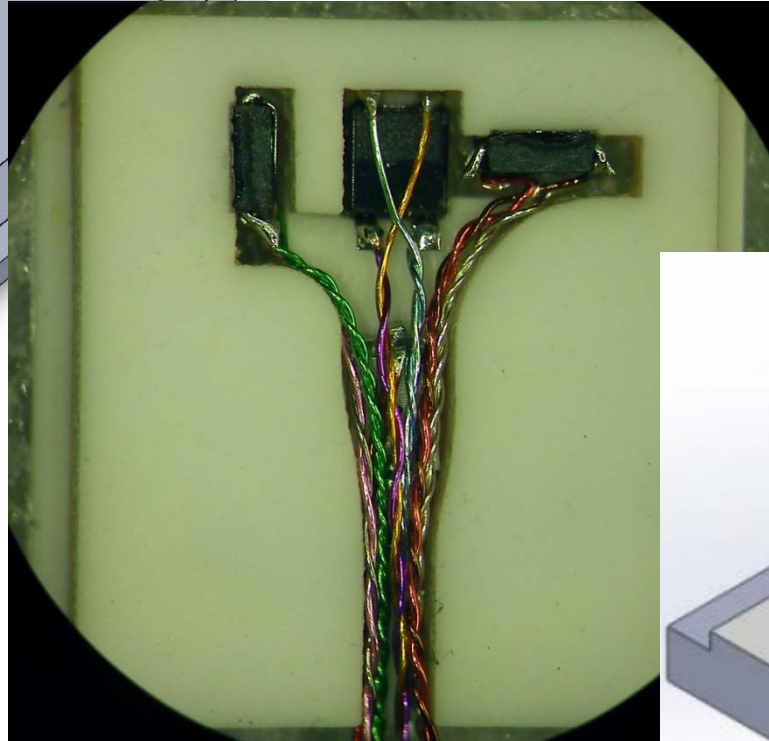
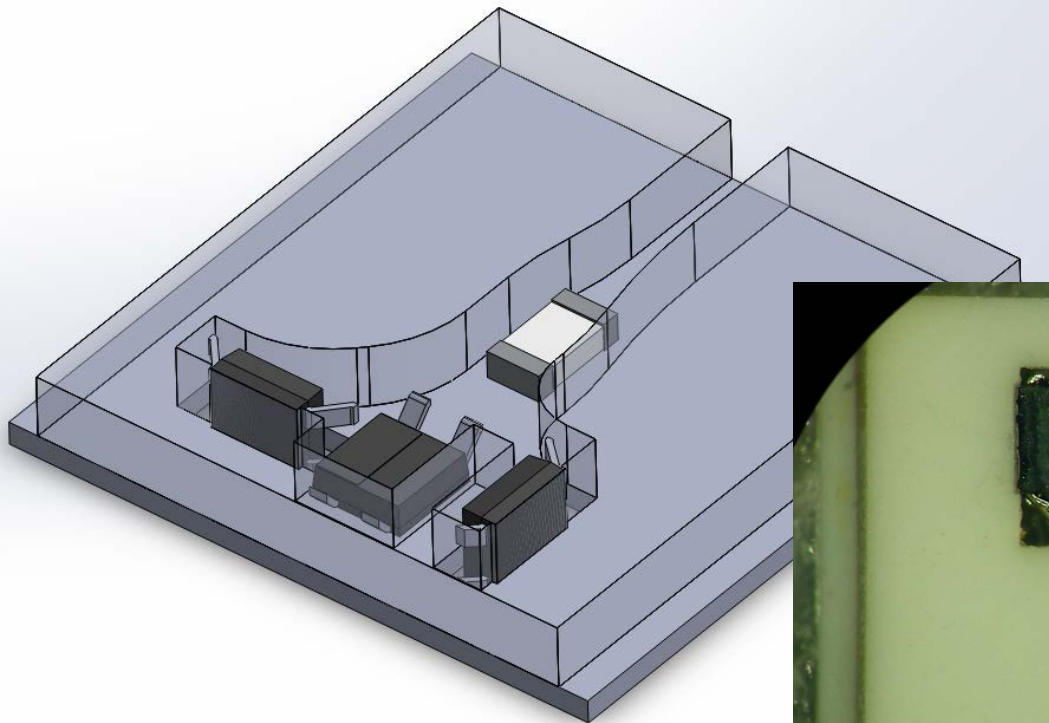
Integrated: Single Chip

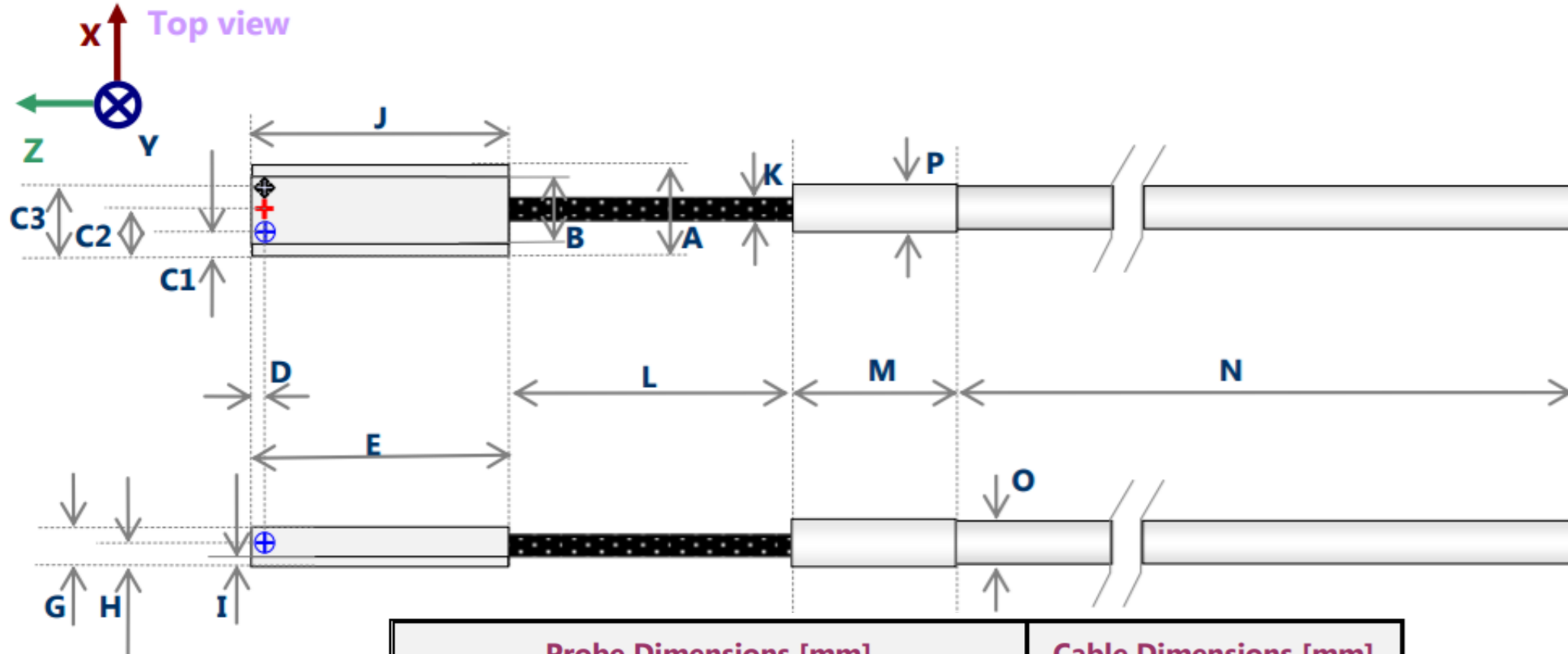
> VH + HH

> IMC - Hall

- perfect alignment
- high resolution
- shared wires

SENIS 3-axis Hall Probe S

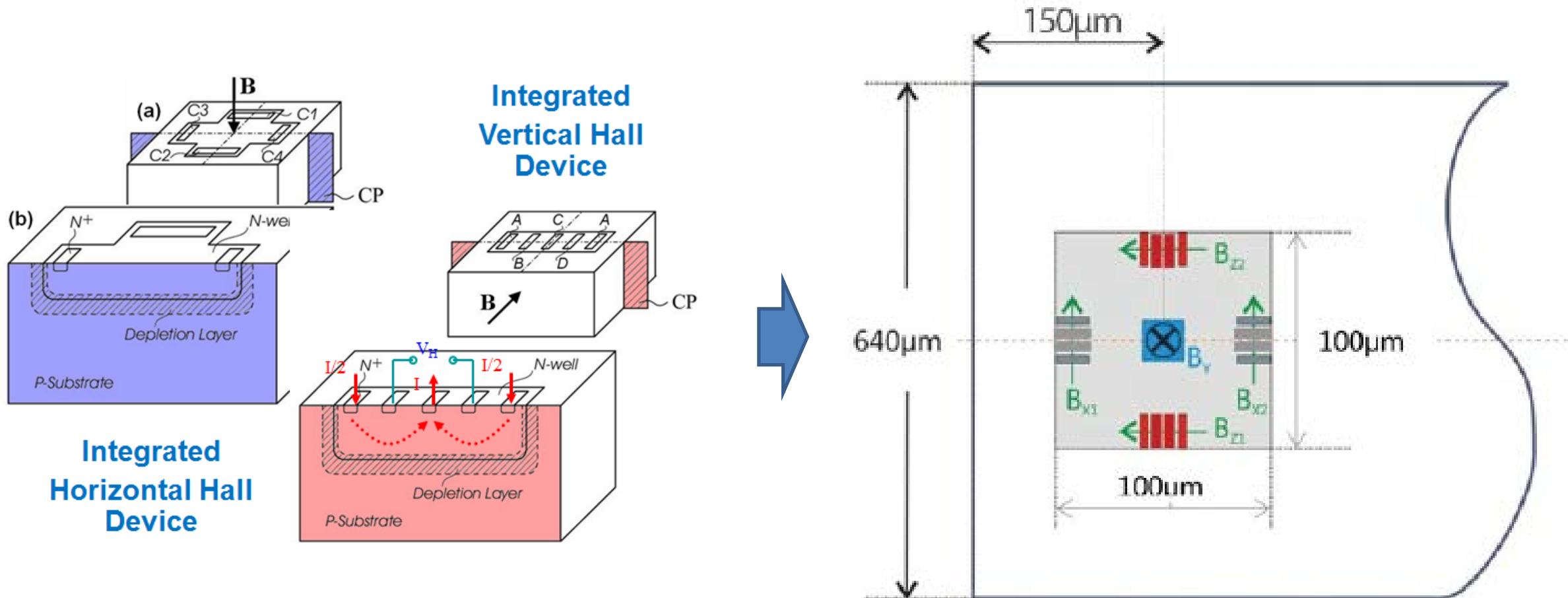




Probe Dimensions [mm]				Cable Dimensions [mm]	
A	10 ± 0.05	E	10 ± 0.05	K	1 ± 0.1
B	9.0 ± 0.05	F		L	200 ± 5
C1	3.0 ± 0.05	G	1.4 ± 0.05	M	20 ± 1
C2	5.0 ± 0.05	H	0.7 ± 0.05	N	10 000
C3	7.0 ± 0.05	I	0.38 ± 0.05	O	2.09
D	2.0 ± 0.05	J	10 ± 0.05	P	2.76

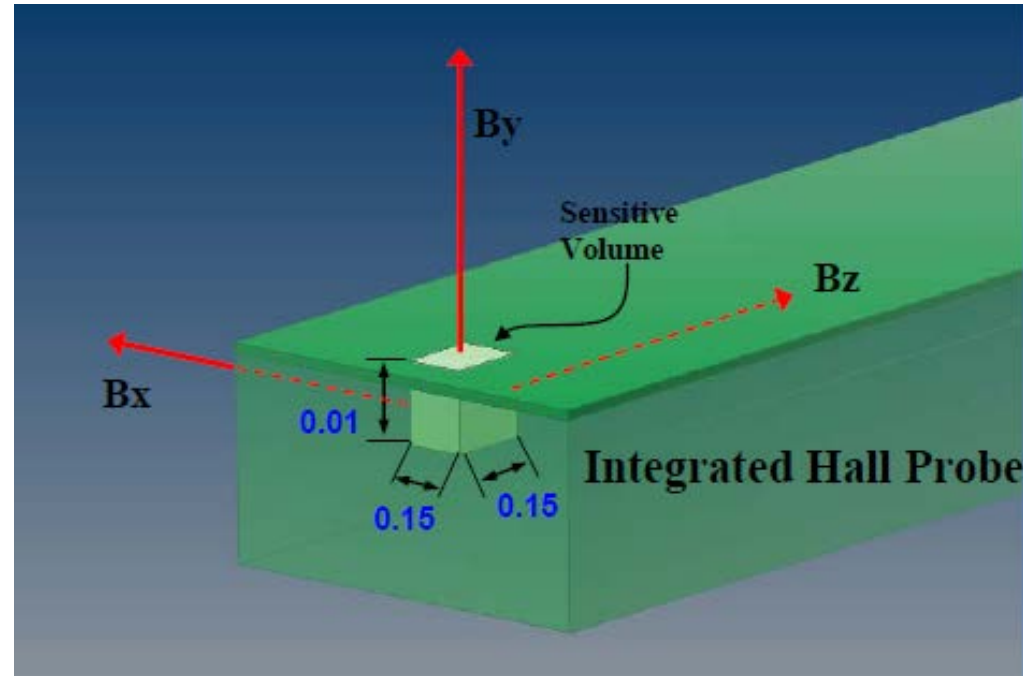
- ⊕ X-sensor
- + Y-sensor
- ⊗ Z-sensor

SENIS 3-Axis Integrated Hall Sensor



Magnetic field sensitive volume:
 $100\mu\text{m} \times 100\mu\text{m} \times 10\mu\text{m}$

Integrated 3-Axis Hall Probe

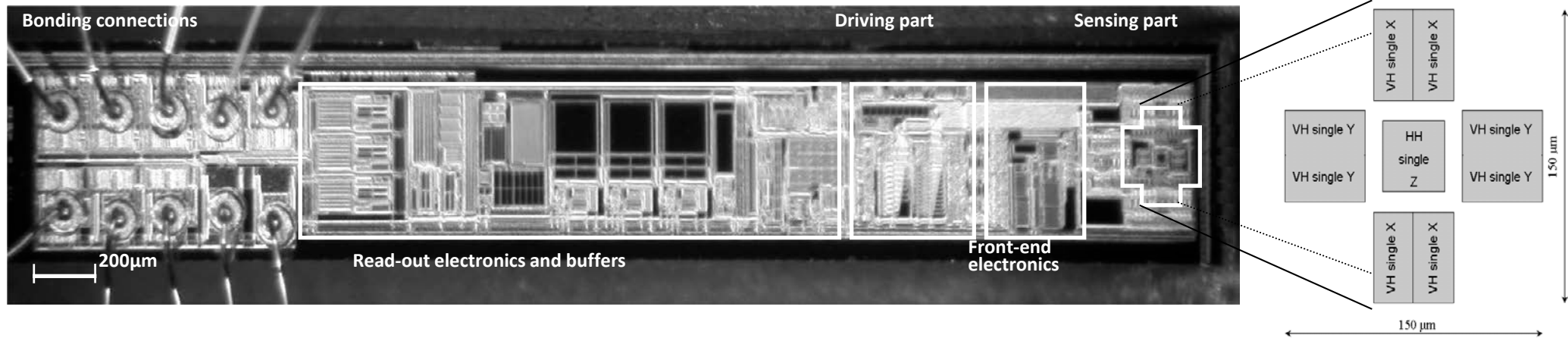


Sensing part composed of two types of micro-Hall sensors

- 4 planar Hall sensor – the perpendicular B-component
- 8 vertical Hall sensors – the in-plane B-components
- Mutual orthogonality: 0.1°

3D spatial resolution: $150\ \mu\text{m}$

SENIS fully integrated 3D Hall sensor



Precise 3D magnetic field measurements

- from militeslas up to tens of tesla
- in the frequency range from DC to 30 kHz
- spatial resolution of about 150 μm
- die dimensions: 4300 μm x 640 μm x 550 μm

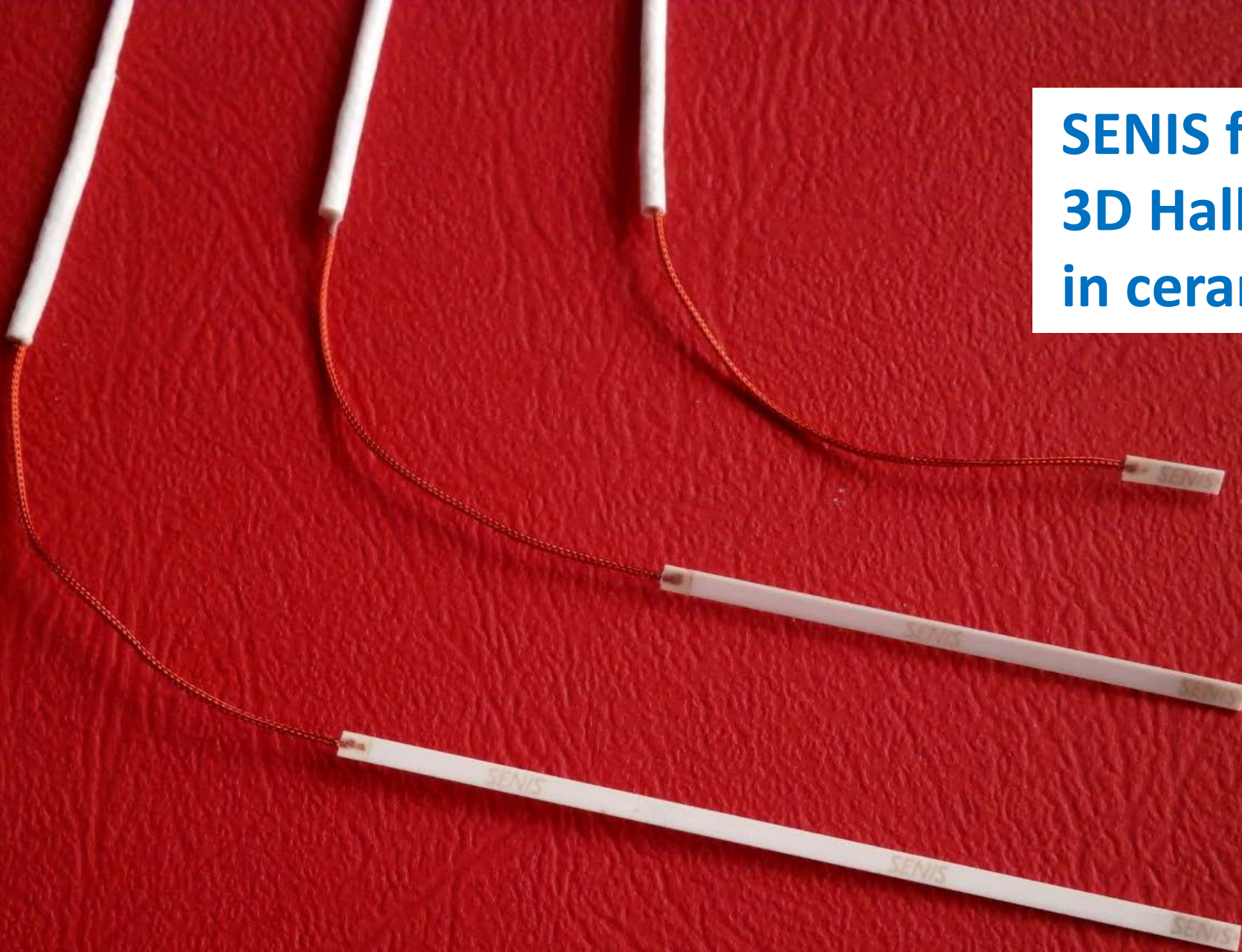
Sensing part composed of two types of micro-Hall sensors

- a planar Hall sensor – the perpendicular B-component
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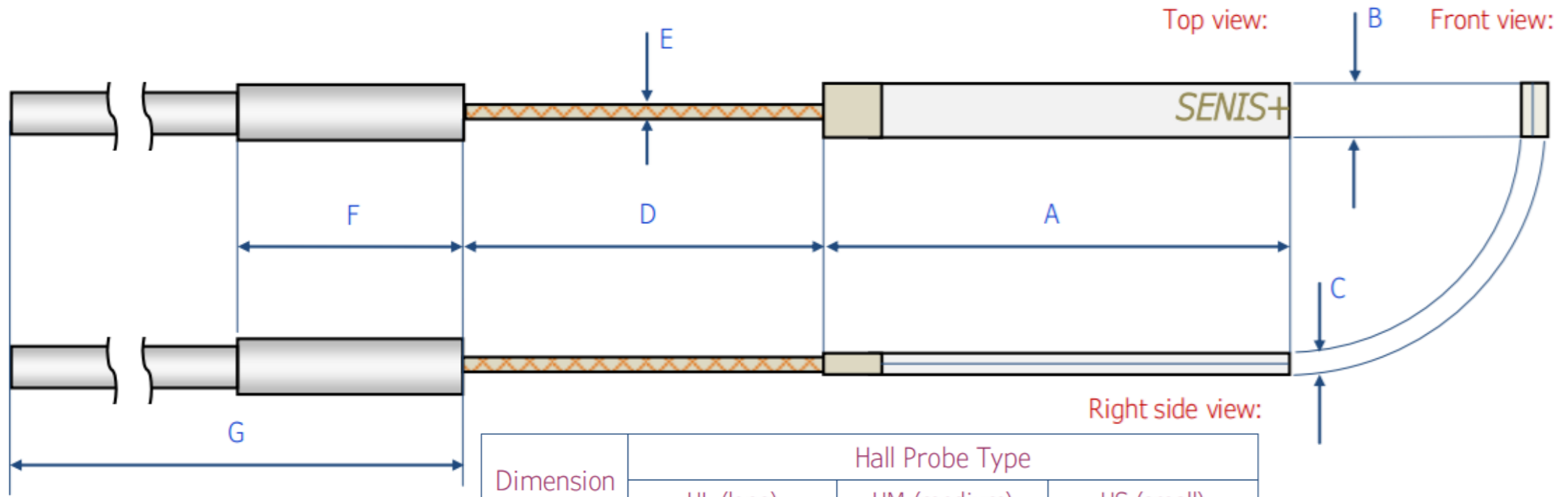
SENIS fully integrated 3D Hall probe in a ceramic package



**SENIS fully integrated
3D Hall probes
in ceramic packages**

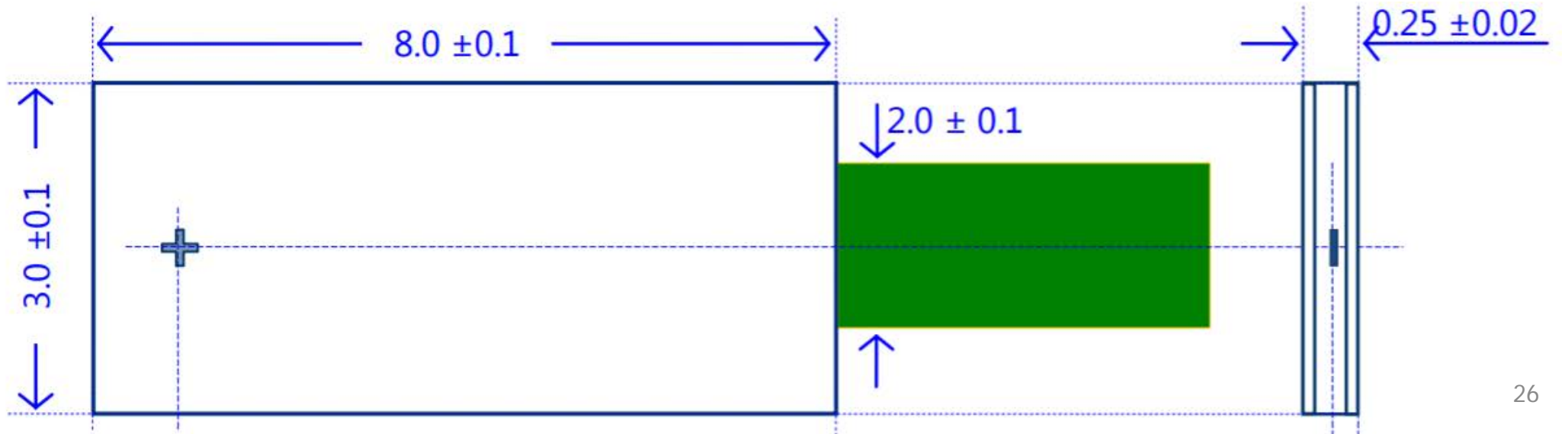
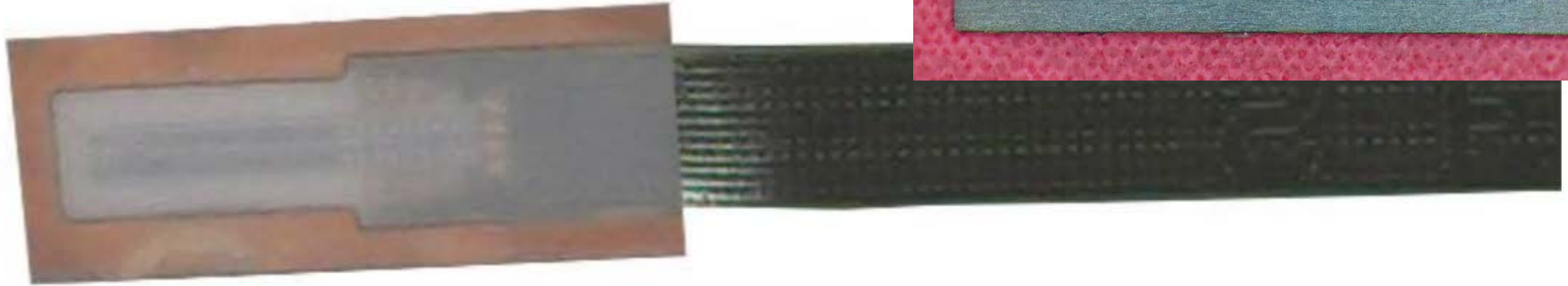


Fully integrated 3-Axis Hall Probe HL, HM, HS

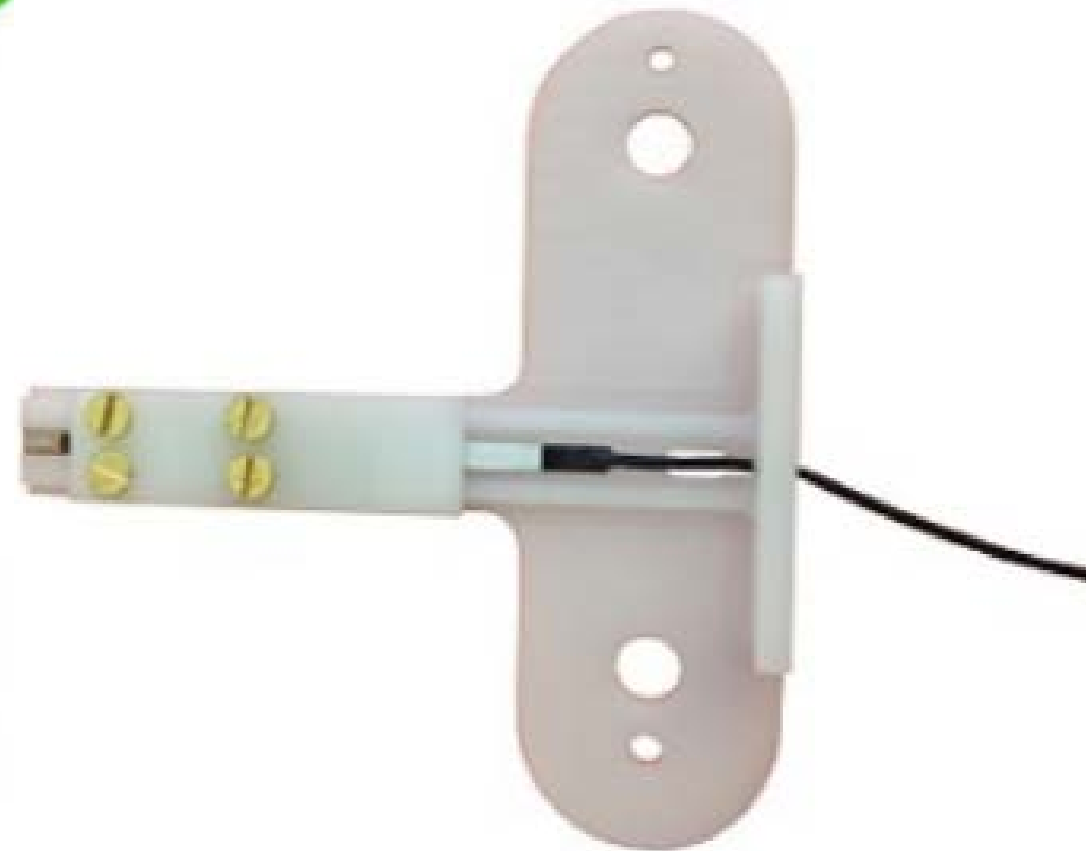


Dimension	Hall Probe Type		
	HL (long)	HM (medium)	HS (small)
A	71.0 ± 0.5 mm	46.0 ± 0.5 mm	8.0 ± 0.2 mm
B	2.00 ± 0.05 mm		
C	0.50 +0.05/-0.00 mm		
D	50 ± 1 mm		
E	Ø 0.8 ± 0.1 mm		
F	25 ± 2 mm		
G	The standard Cable lengths are: 2m, 5m and 10m. Optionally, different cable lengths are available, on a demand.		

SENIS Very Thin fully integrated 3D Hall probes



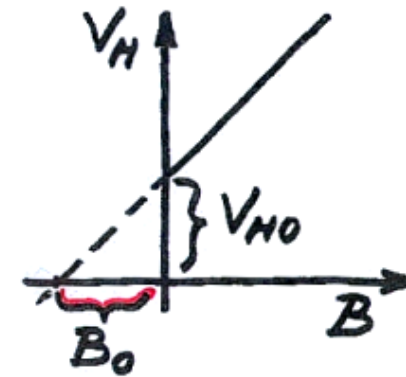
Probe Holders



Parasitic Effects in Hall Devices

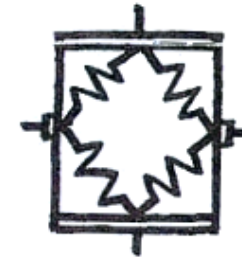
- **Offset**
- **Noise**
- **Planar Hall effect**
- **Non-linearity**
- **Temperature dependence**
- **Stress dependence**
- **Inductive effects**
- **...**

Offset in a Hall Device



$V_{H0} \equiv V_H \text{ at } B=0$
 B_0 \equiv apparent B_{meas} at $B=0$

CAUSES: ASYMMETRY DUE TO



- GEOMETRY
- DOPING
- TEMPERATURE GRAD.
- MECHANICAL STRESS
- SURFACE EFFECTS

TYPICAL VALUES:

$B_0 \sim 5 \dots 50 \text{ mT}$

OEMF: Offset-Equivalent Magnetic Field

$$OEMF = V_{\text{off}} / S_A$$

V_{off} : Output offset voltage [V]

S_A : Absolute magnetic sensitivity [V/T]

Basic OEMF:

- Si integrated Hall elements: 5mT – 50mT
- High-mobility Hall elements: ca. 1mT

Offset Fluctuations and Noise

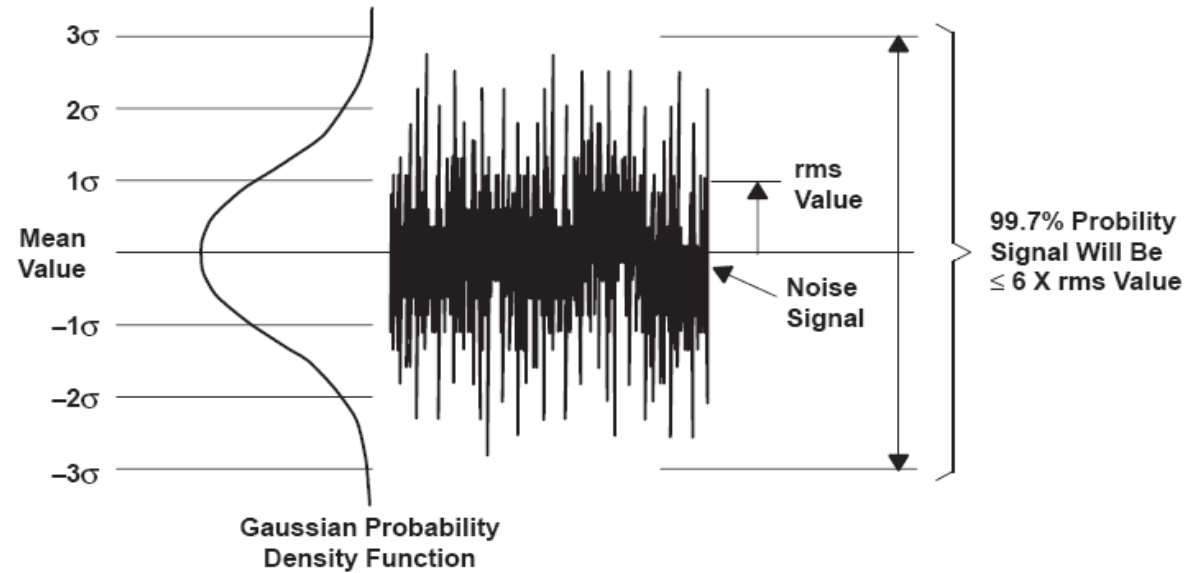


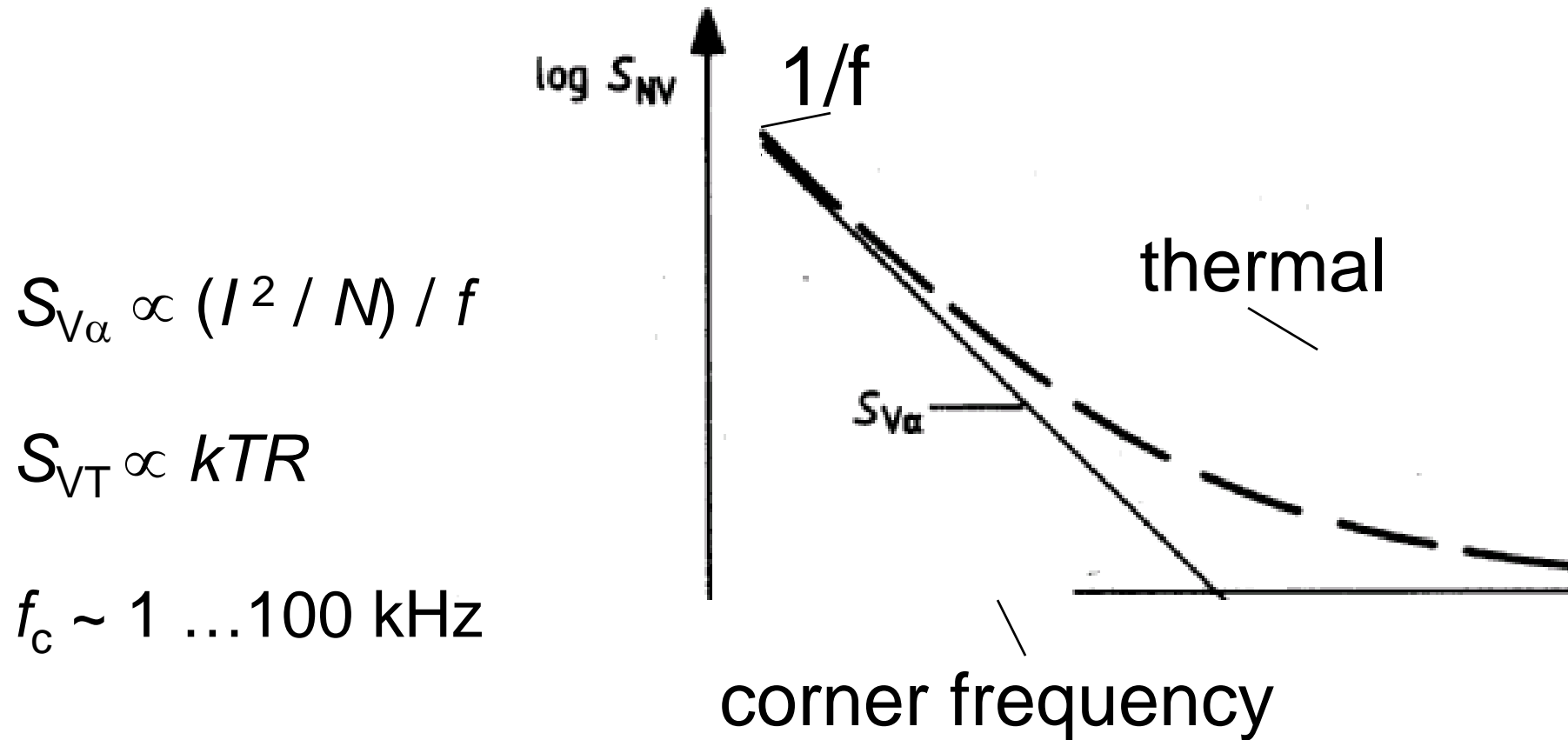
Figure 1. Gaussian Distribution of Noise Amplitude

- σ^2 : Variance
- σ : Standard deviation
- V_{nRMS} : Root Mean Square noise voltage
- V_{nP-P} : Peak-to-Peak noise voltage

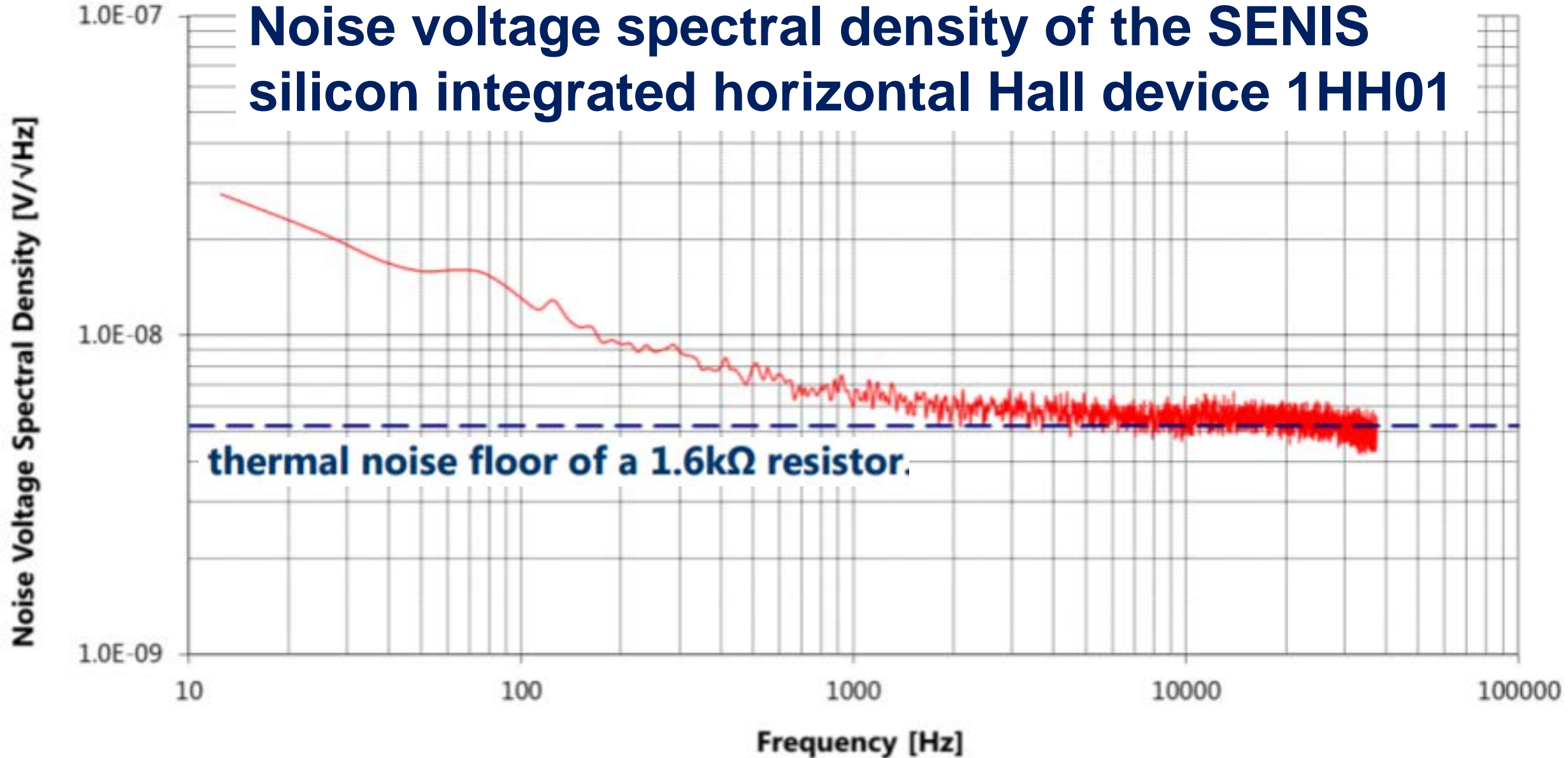
$$V_{nRMS} = \sigma$$

$$V_{nP-P} \approx 6 V_{nRMS}$$

Noise Voltage Spectral Density of a Hall Device



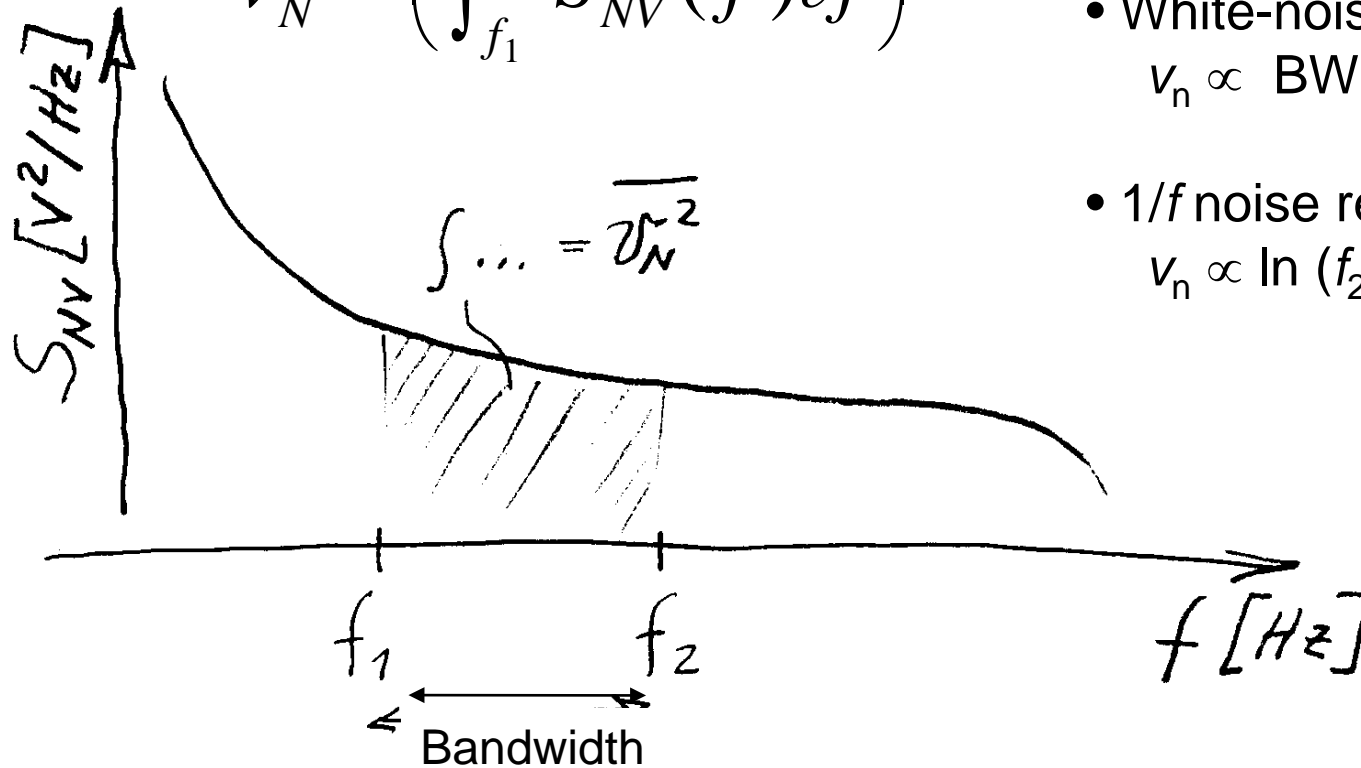
Noise voltage spectral density of the SENIS silicon integrated horizontal Hall device 1HH01



Noise Spectral Density and Noise Voltage

RMS noise voltage:

$$v_N = \left(\int_{f_1}^{f_2} S_{NV}(f) df \right)^{\frac{1}{2}}$$



- White-noise region:
 $v_n \propto \text{BW} = f_2 - f_1$
- $1/f$ noise region:
 $v_n \propto \ln(f_2 / f_1)$

NEMF: Noise-Equivalent Magnetic Field

$$NEMF = V_n / S_A \quad \text{or} \quad NEMF SD = V_n SD / S_A$$

V_n : Output noise voltage [V]

$V_n SD$: Noise voltage spectral density [V/ $\sqrt{\text{Hz}}$]

S_A : Absolute magnetic sensitivity [V/T]

NEMF[T] – depends on the frequency bandwidth

NEMF Spectral Density [T/ $\sqrt{\text{Hz}}$] – a detailed spec.

Typical values of NEMF SD

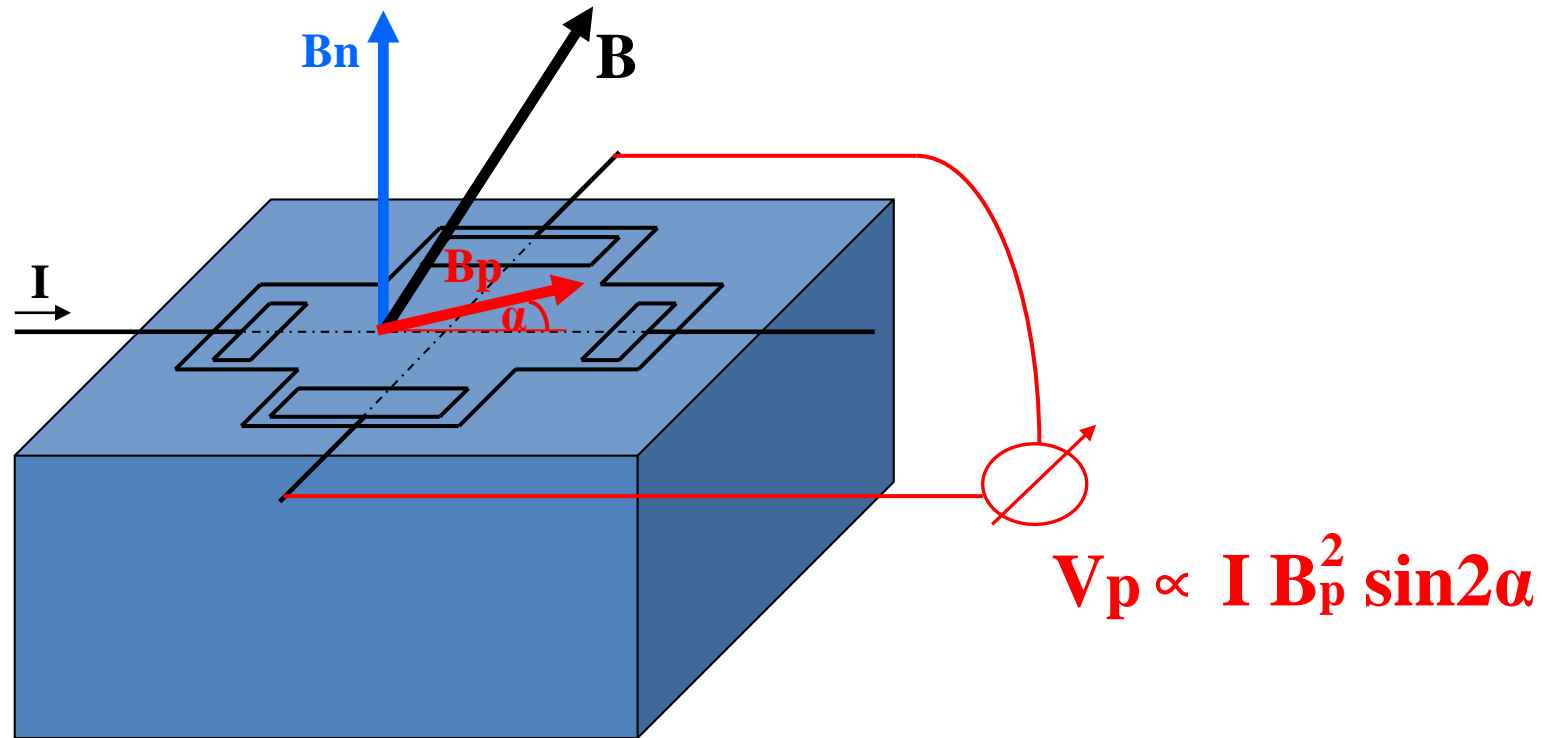
Thermal noise region, at room temperature:

- integrated silicon Hall elements: about 100nT/√Hz;
- GaAs epitaxial or 2DEG Hall elements: about 20nT/√Hz;
- high-mobility thin-film InSb Hall elements: about 1.5nT/√Hz.

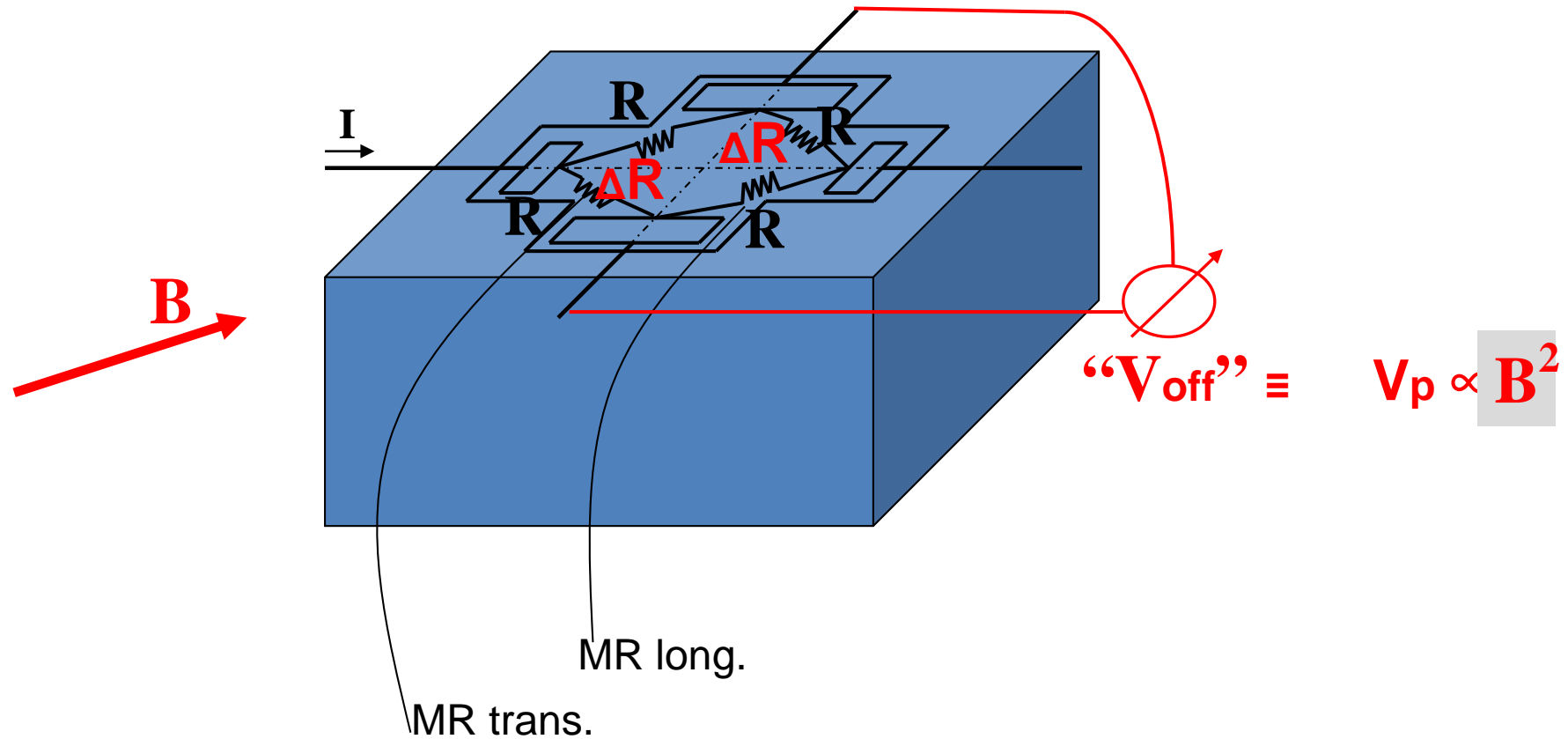
Parasitic Effects in Hall Devices

- Offset
- Noise
- **Planar Hall effect**
- Non-linearity
- Temperature dependence
- Stress dependence
- Inductive effects
- ...

Planar Hall Effect



MR Model of the Planar Hall effect



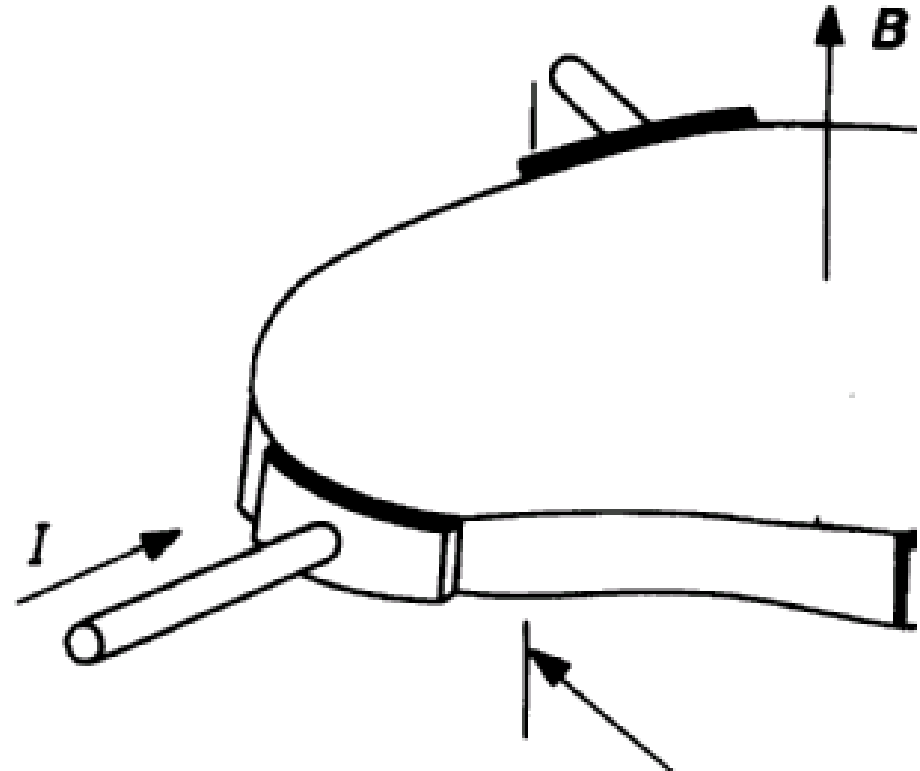
Summary

- Hall Plate:
4 Contacts, $\mathbf{B} \perp$ Plate

- Hall Voltage:

$$\begin{aligned} V_H &= V B_{\perp} \\ &= S_I I B_{\perp} \end{aligned}$$

- Errors: Offset, Noise, Planar Hall Effect, ...



Where to get more information

R S Popovic:

“Hall Effect Devices”

2nd Edition, 2004

Institute of Physics Publishing, IOP, Bristol and Philadelphia

HALL MAGNETIC SENSORS - SIGNAL PROCESSING

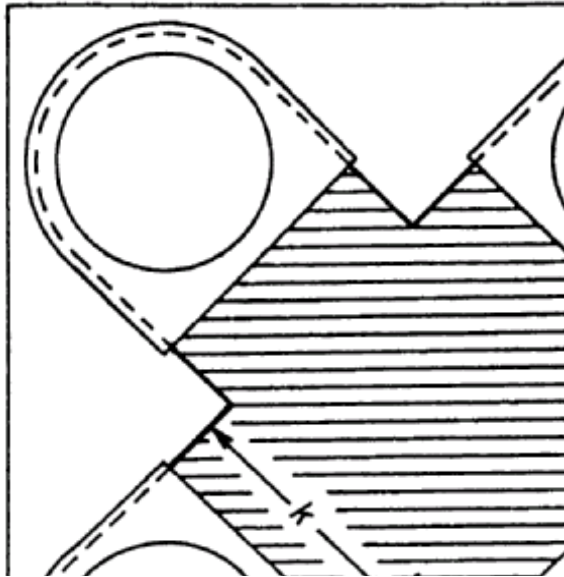
Radivoje S. Popovic

EPFL, Swiss Federal Institute of Technology
Lausanne, Switzerland,

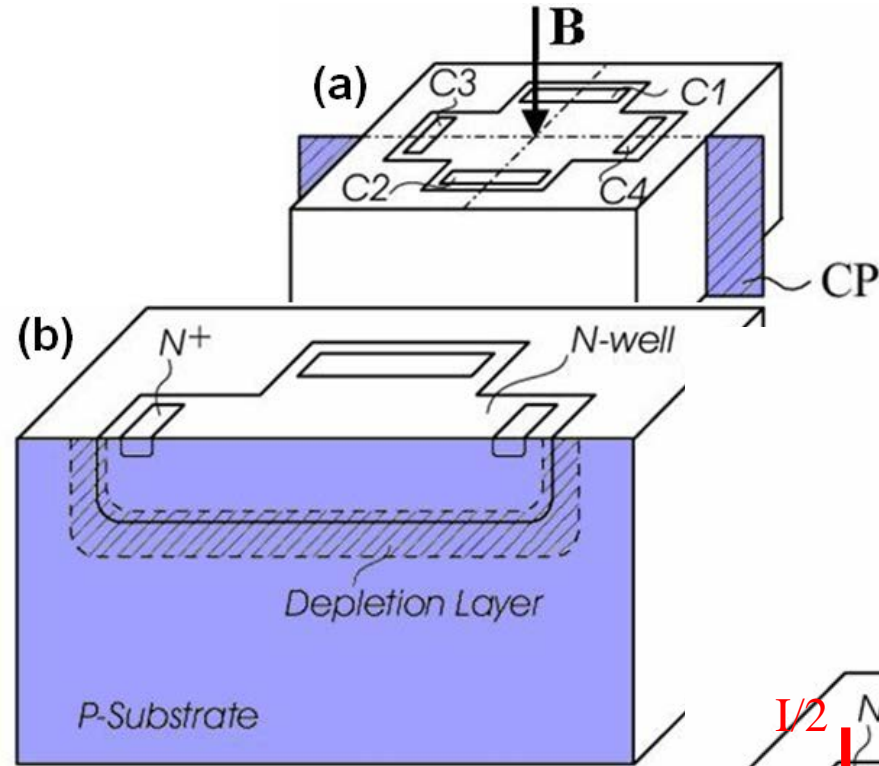
and

SENIS AG, Zug, Switzerland

Hall Devices

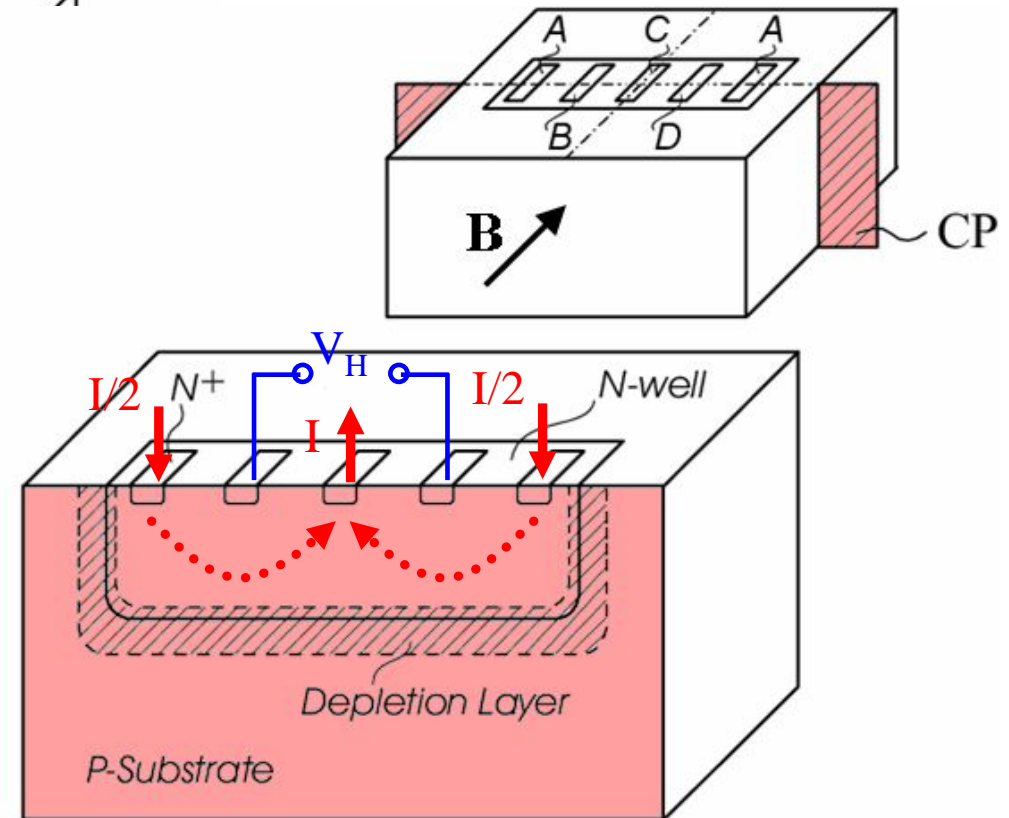


GaAs Hall Device



Integrated Horizontal Hall Device

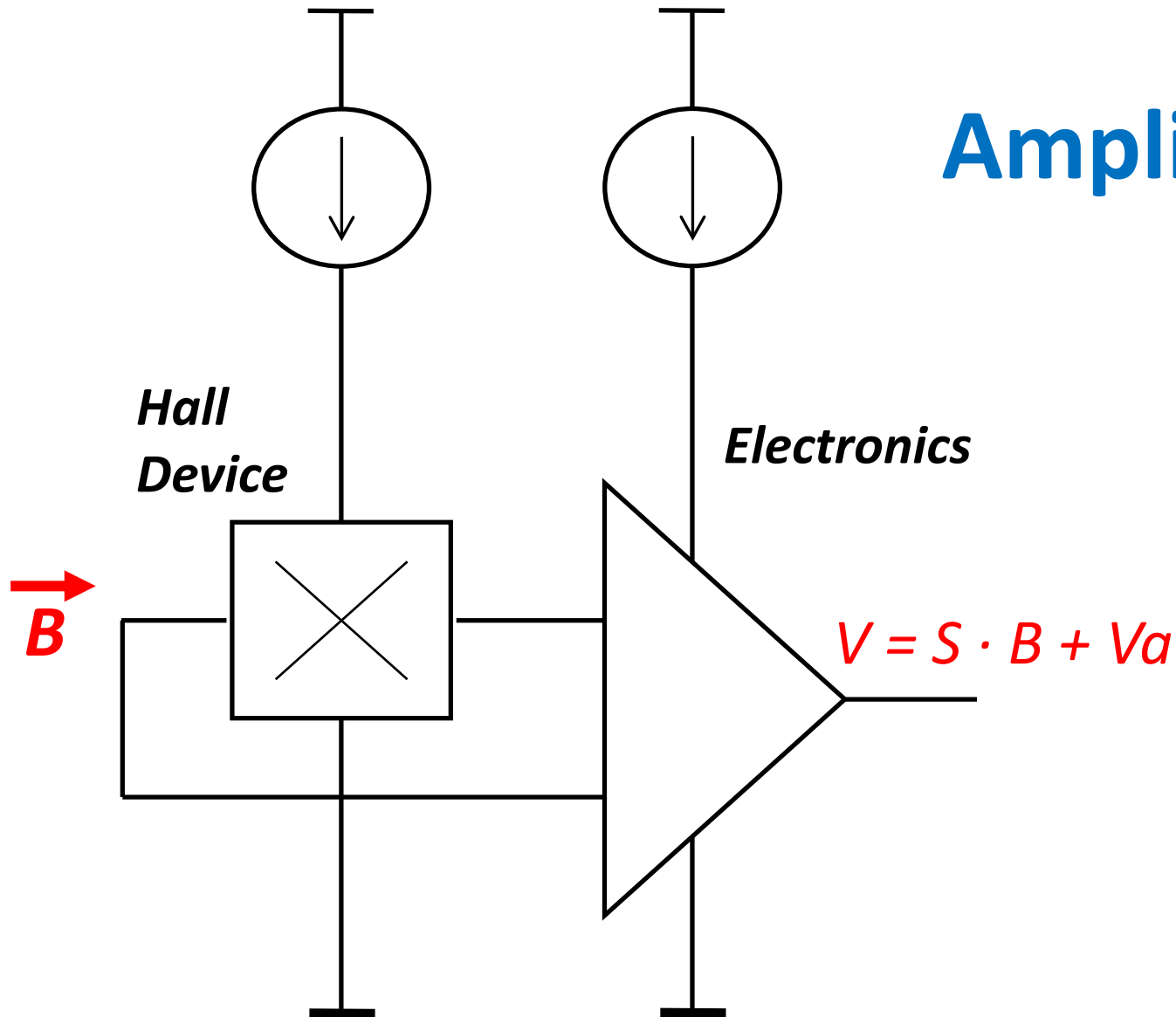
Integrated Vertical Hall Device



Outline

- **Amplification of the Hall voltage**
- **Reducing offset, low-frequency noise, planar Hall effect, inductive effects, ...**
- **Reducing angular errors**
- **Amplification of the magnetic signal**
- **Experimental Results**

Amplifying the Hall voltage



S : absolute magnetic sensitivity of the transducer

V_a : total artifact signal (noise voltage, offset, ...)

Resolution limit:
when $S \cdot B \approx V_a$, i.e.

$$B_{res} \approx V_a / S$$

Magnetic Resolution Limit

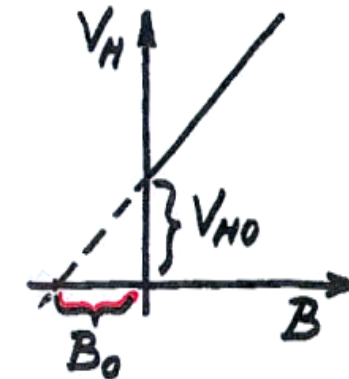
The magnetic resolution **limit** – when **Signal to Artifact Ratio** ≈ 1

$B_{res} \approx$ Artifact-Equivalent Magnetic Field, $AEMF = V_a / S$

V_a : artifact signal (noise voltage, offset drift, ...)

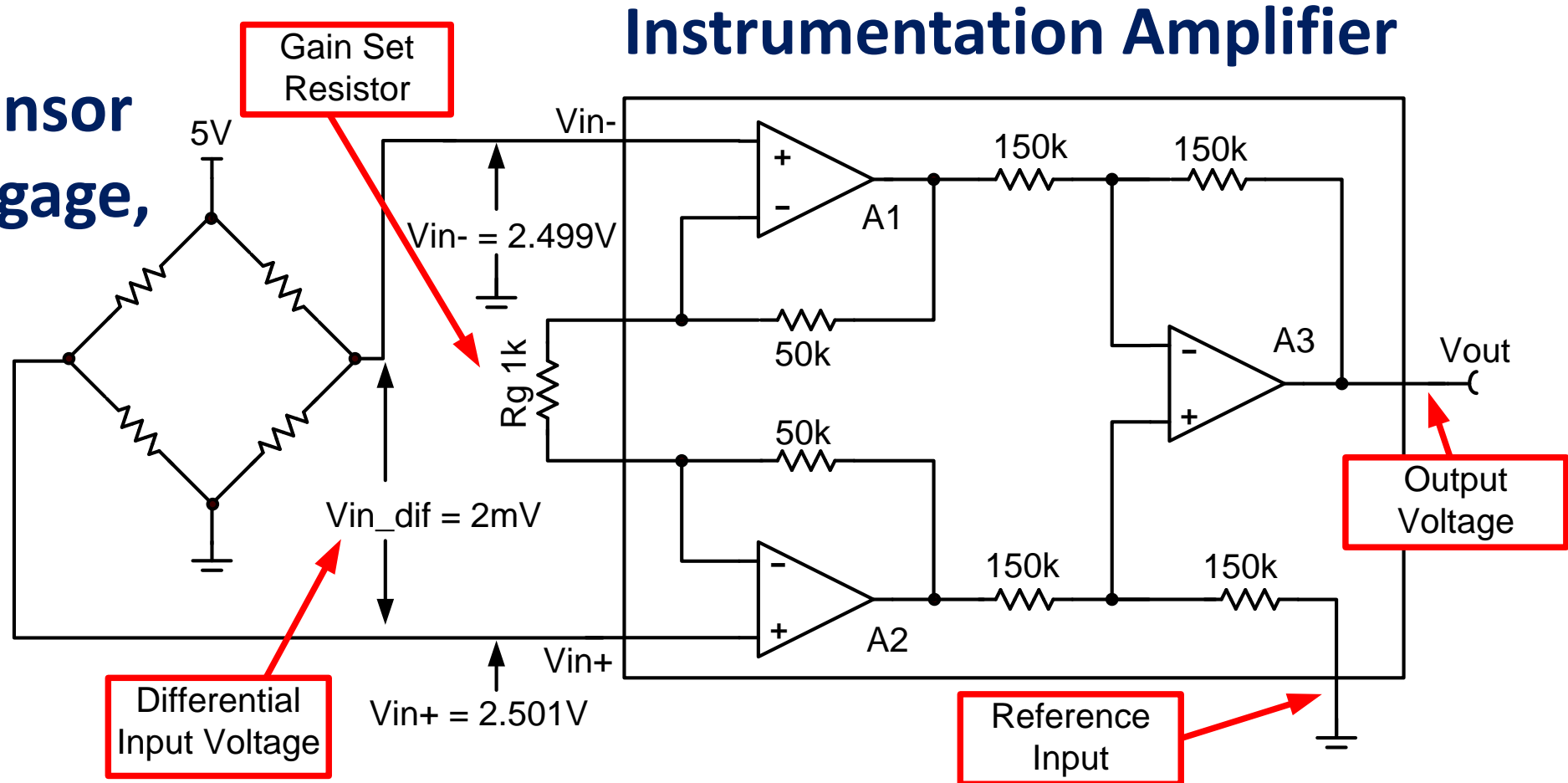
S : absolute magnetic sensitivity

- DC resolution: limited by
 - offset (if can not be zeroed)
 - offset drift (thermal, aging, ...)
 - offset fluctuations (BW: $\sim 0.1\text{Hz}$ to 10Hz)
- AC resolution: limited by noise
 - noise (thermal and $1/f$)
 - bandwidth

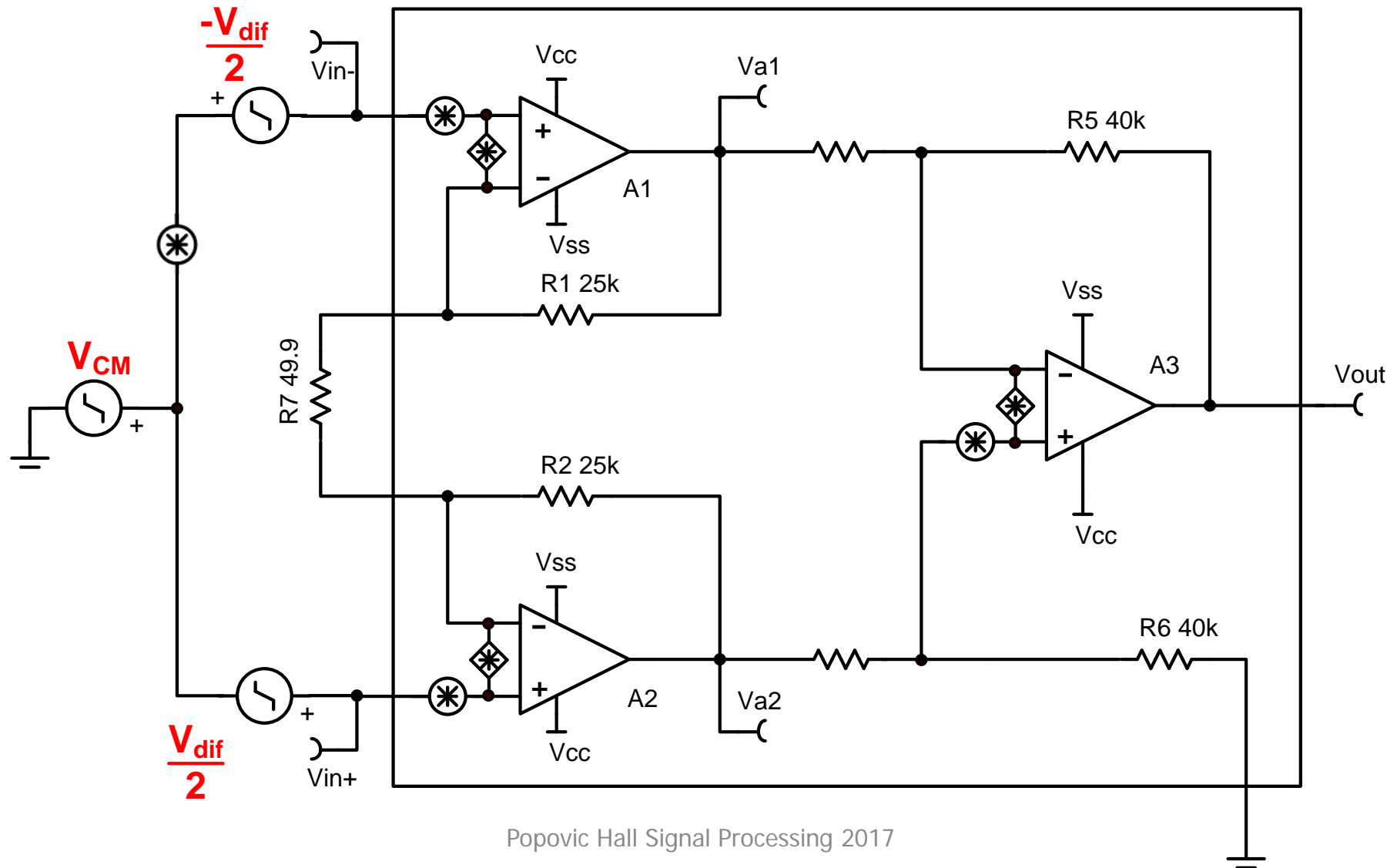


Amplifying the signal of a bridge-type sensor

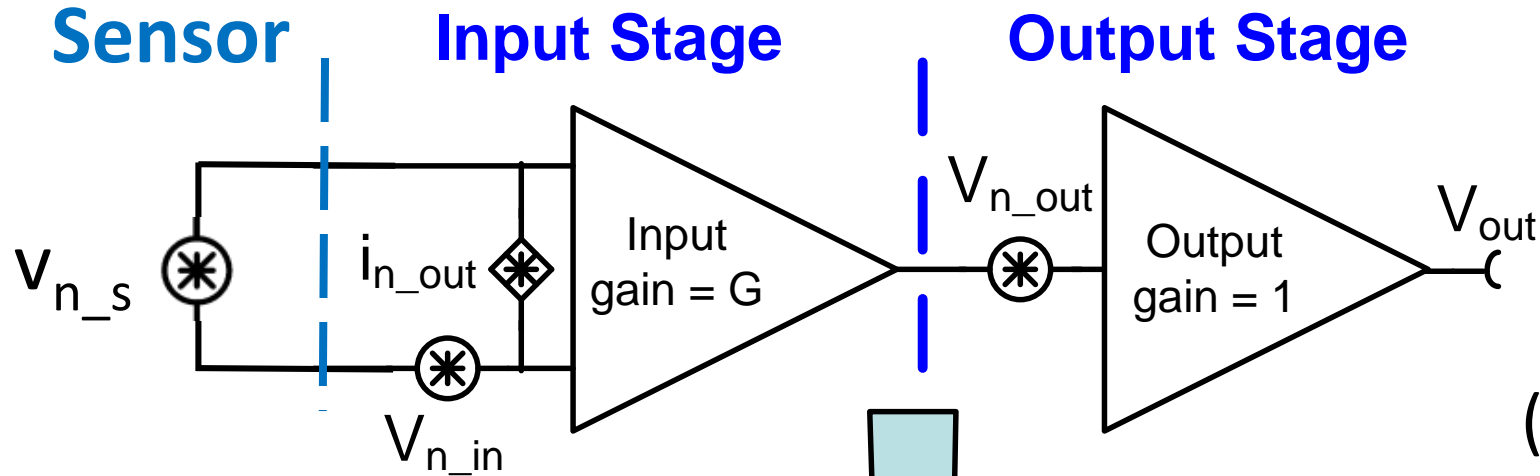
Hall sensor
Strain gage,
...



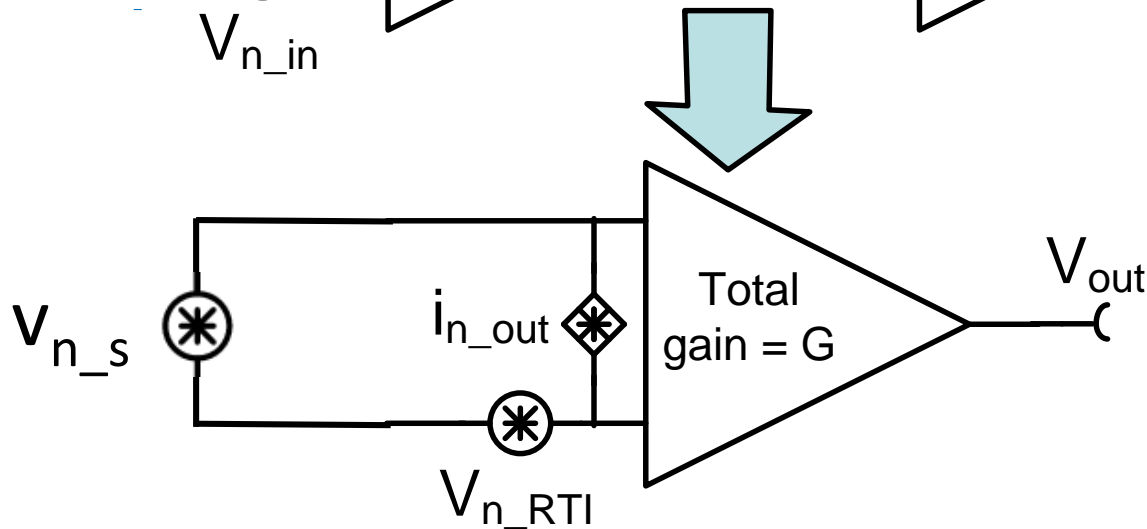
Noise model of a transducer



The Complex Model is Simplified



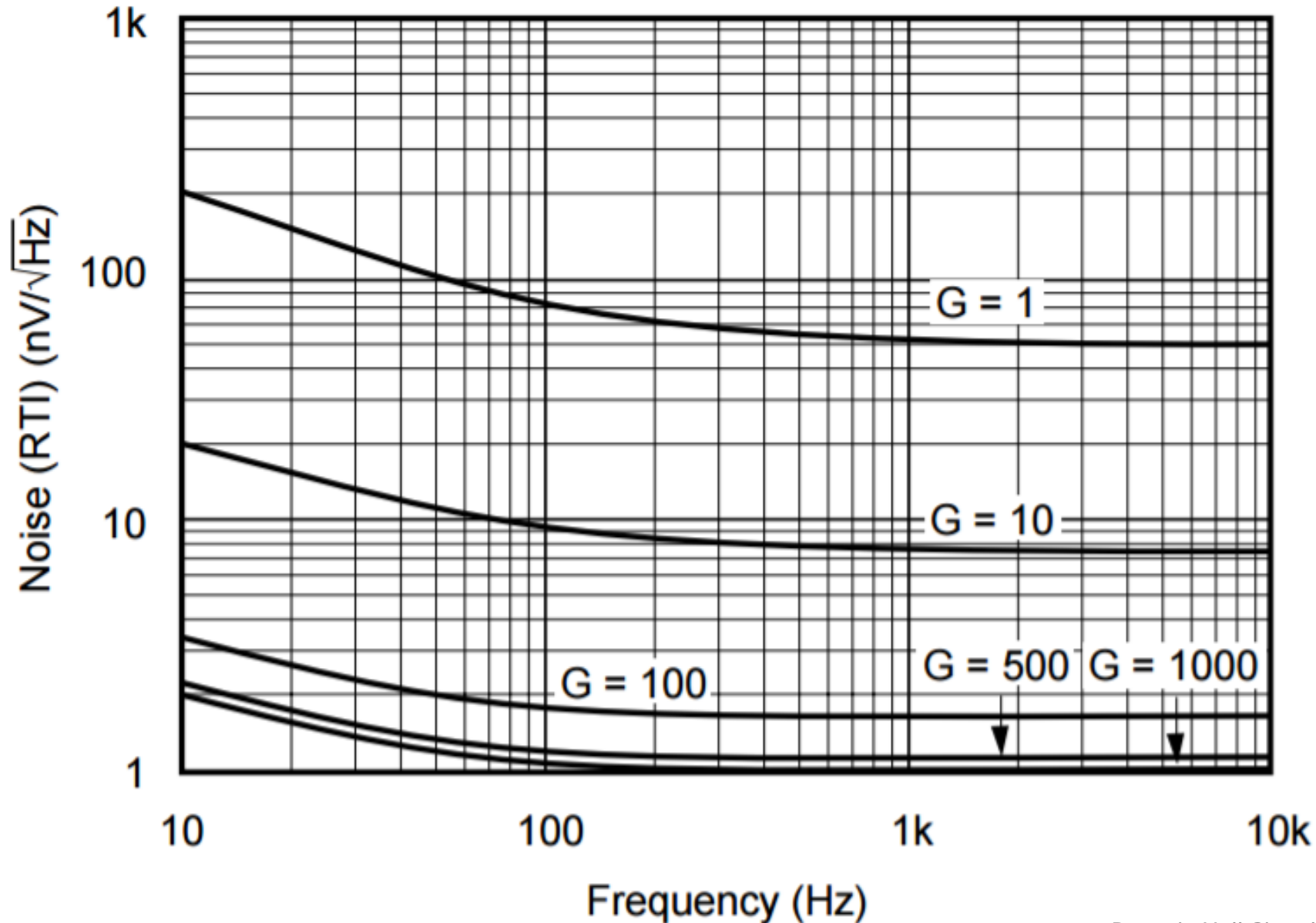
$$(V_{n_in})^2 = (V_{n_s})^2 + (V_{n_ai})^2$$



$$V_{n_out} = \sqrt{(V_{n_out})^2 + (V_{n_in} \cdot G)^2}$$

$$V_{n_RTI} = \sqrt{\left(\frac{V_{n_out}}{G}\right)^2 + (V_{n_in})^2}$$

NOISE VOLTAGE (RTI) vs FREQUENCY



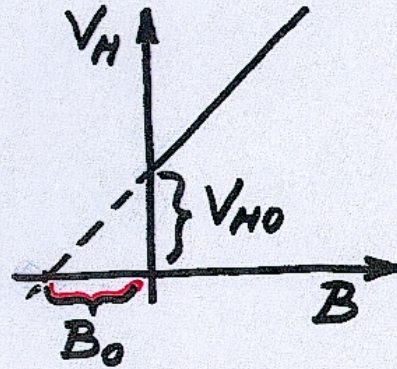
Example:

INA 163

&

$$V_{n_s} \ll V_{n_{ai}}$$

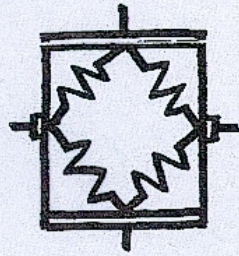
OFFSET IN A HALL DEVICE



$$V_{H0} \equiv V_H \text{ at } B=0$$

$$\underline{B_0} \equiv \text{apparent } B_{\text{meas}} \text{ at } B=0$$

CAUSES: ASYMETRY DUE TO

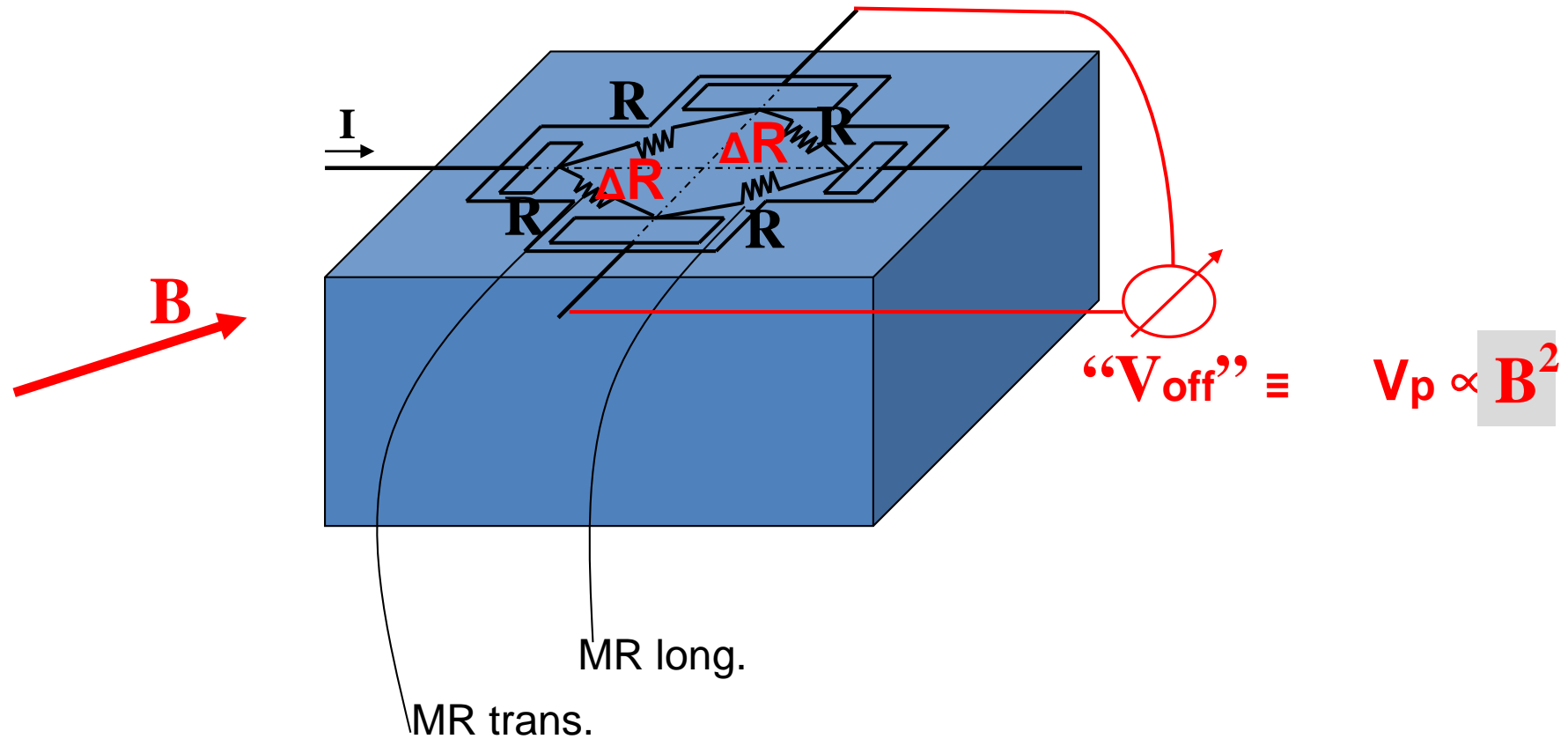


- GEOMETRY
- DOPING
- TEMPERATURE GRAD.
- MECHANICAL STRESS
- SURFACE EFFECTS

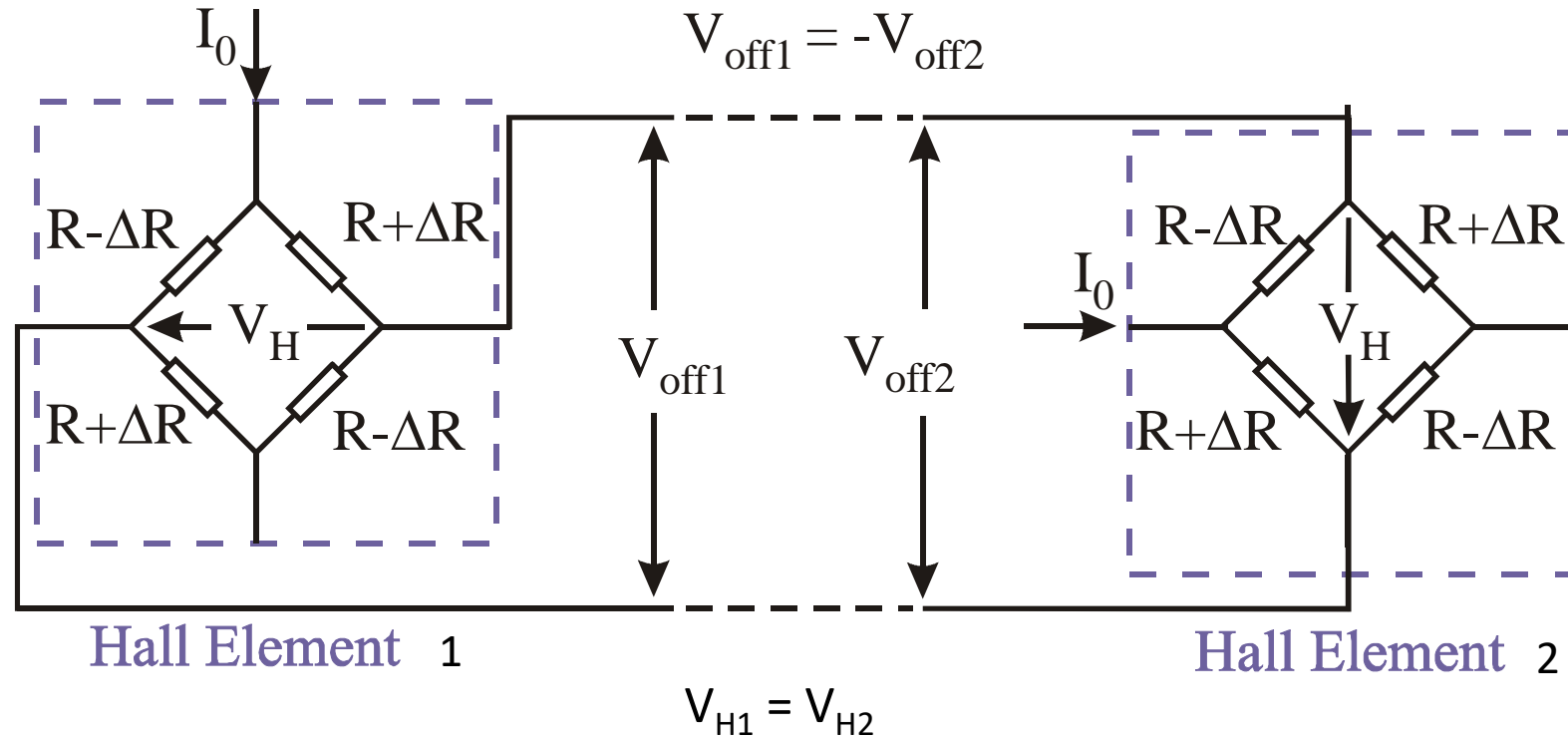
TYPICAL VALUES:

$$B_0 \sim 5 \dots 50 \text{ mT}$$

MR Model of the Planar Hall effect



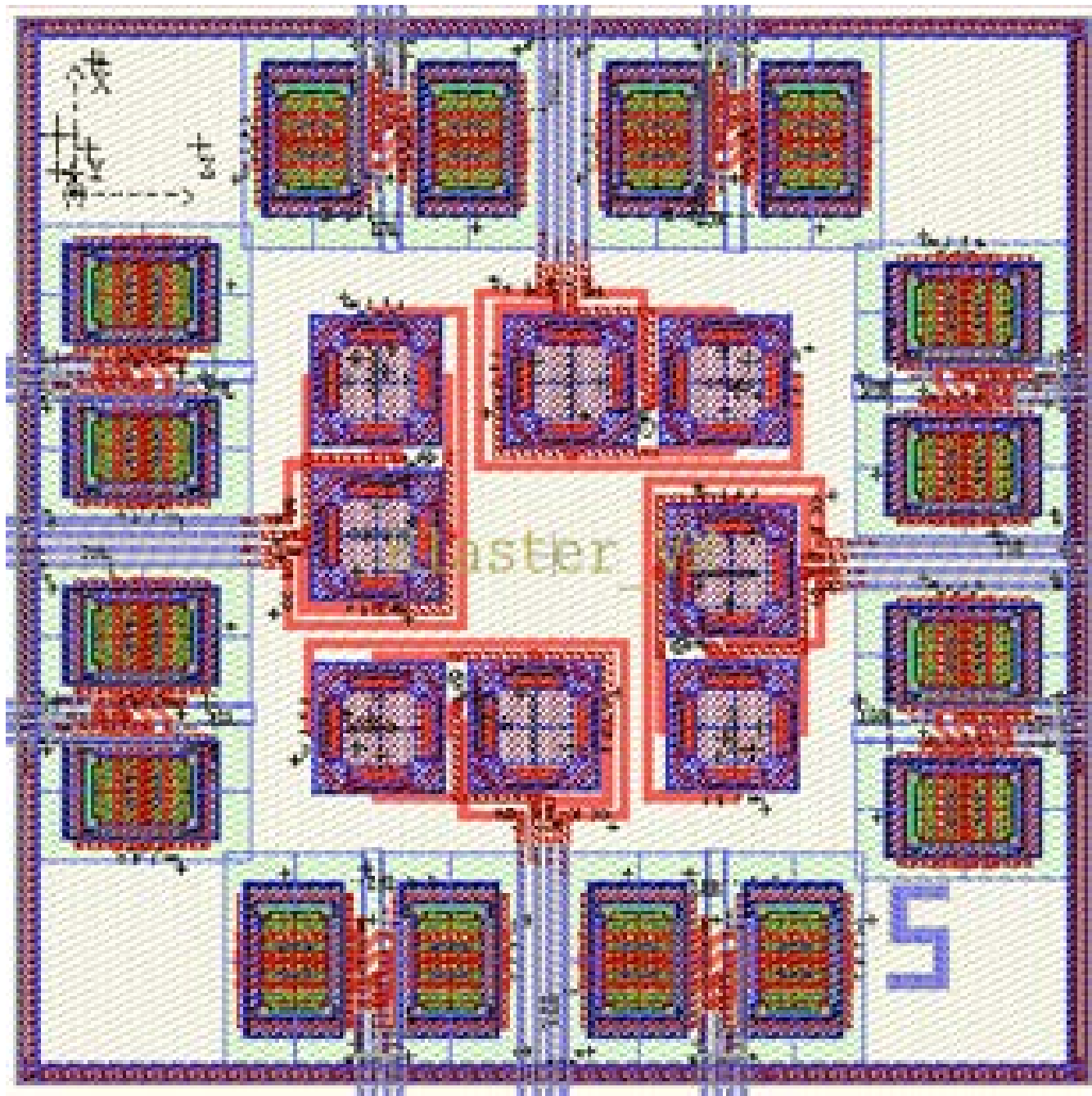
Reducing Offset and Noise: Orthogonal-Parallel Coupling of Hall Elements



1 × Hall: $V_{\text{noise}1} = \sqrt{4kTR\Delta f}$; 2 × Hall: $V_{\text{noise}2} = V_{\text{noise}1} / \sqrt{2}$;

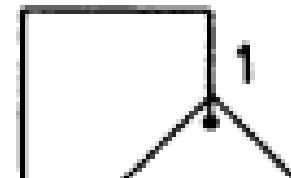
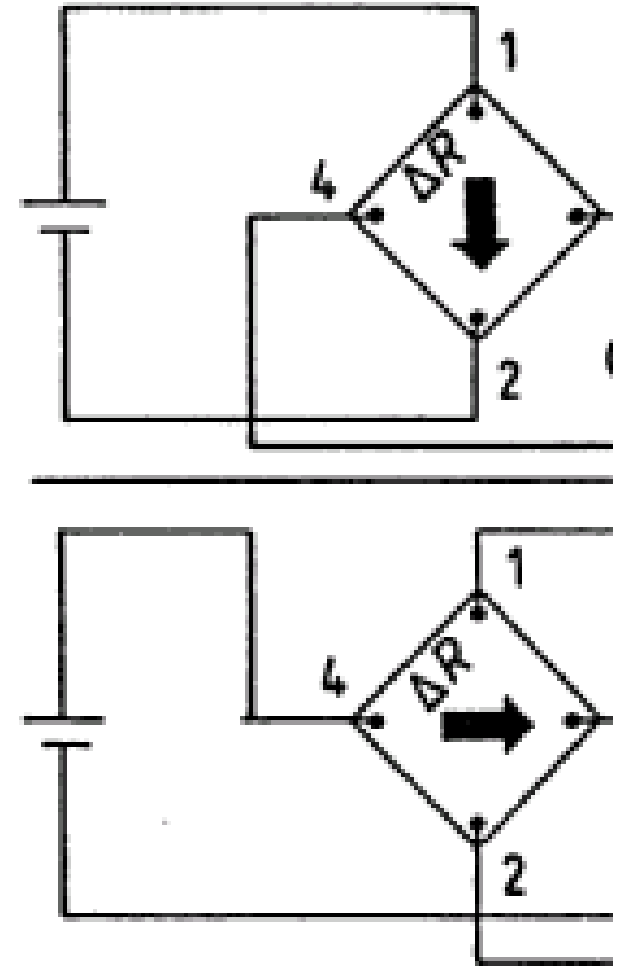
N × Hall: $V_{\text{noise}N} = V_{\text{noise}1} / \sqrt{N}$

SENIS integrated orthogonally coupled Hall elements

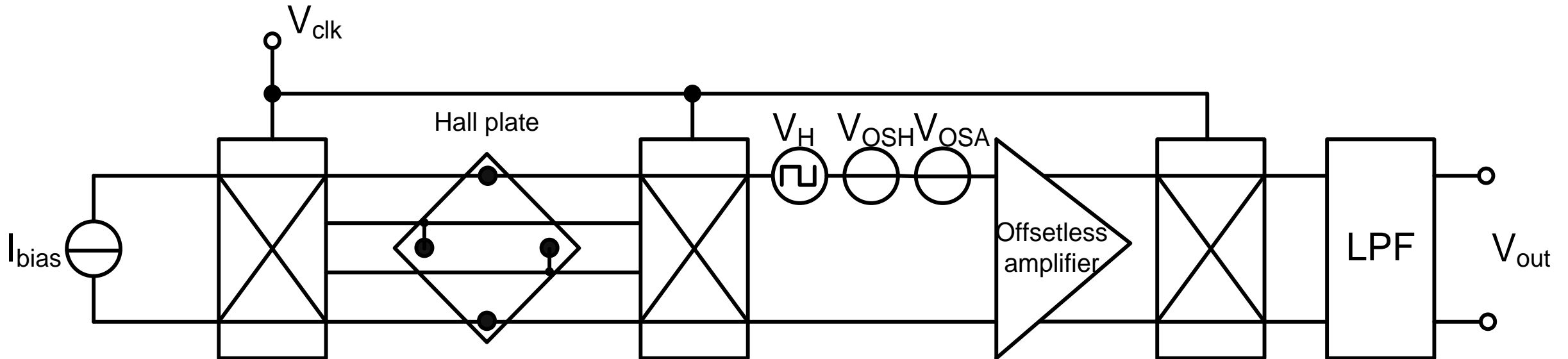


Reducing Offset and 1/f Noise by Current Spinning

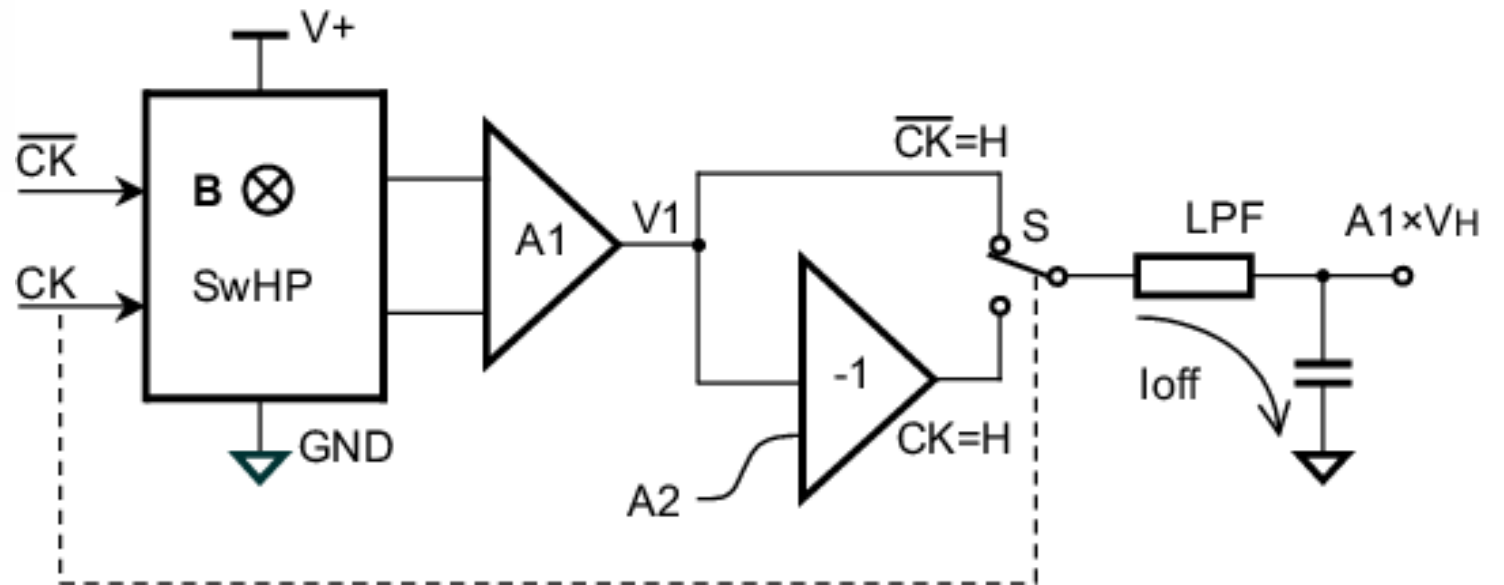
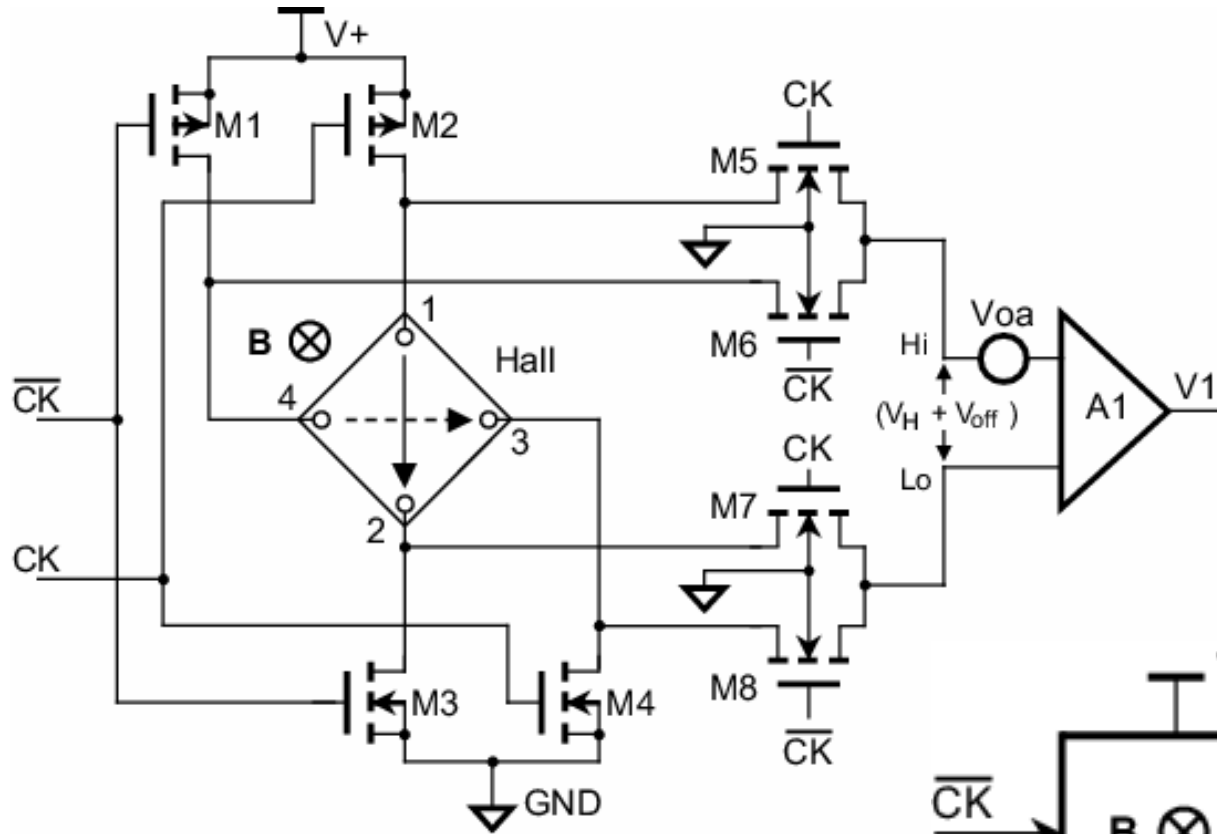
« Switched Hall »
or
« Spinning Current »
Technique



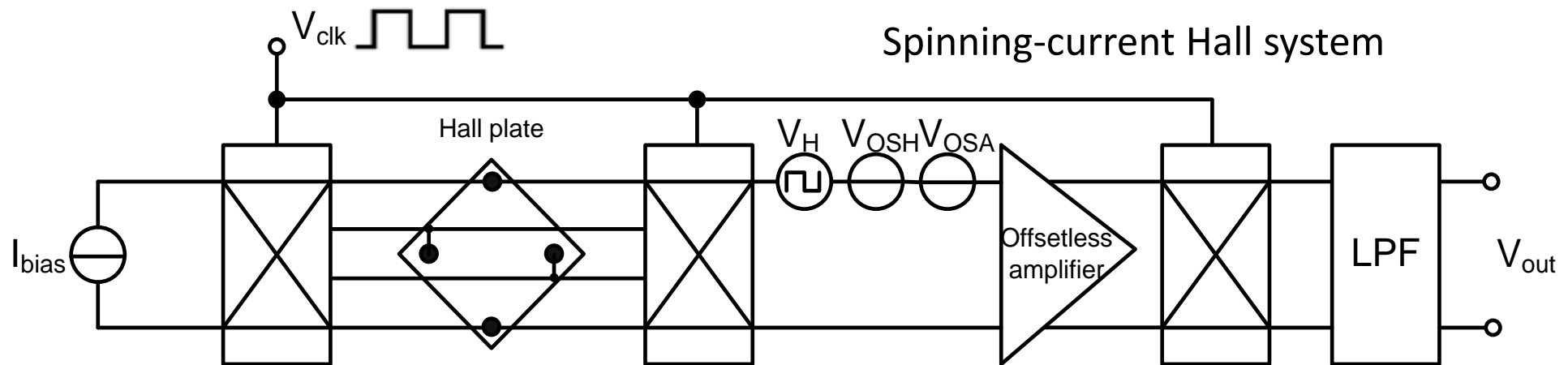
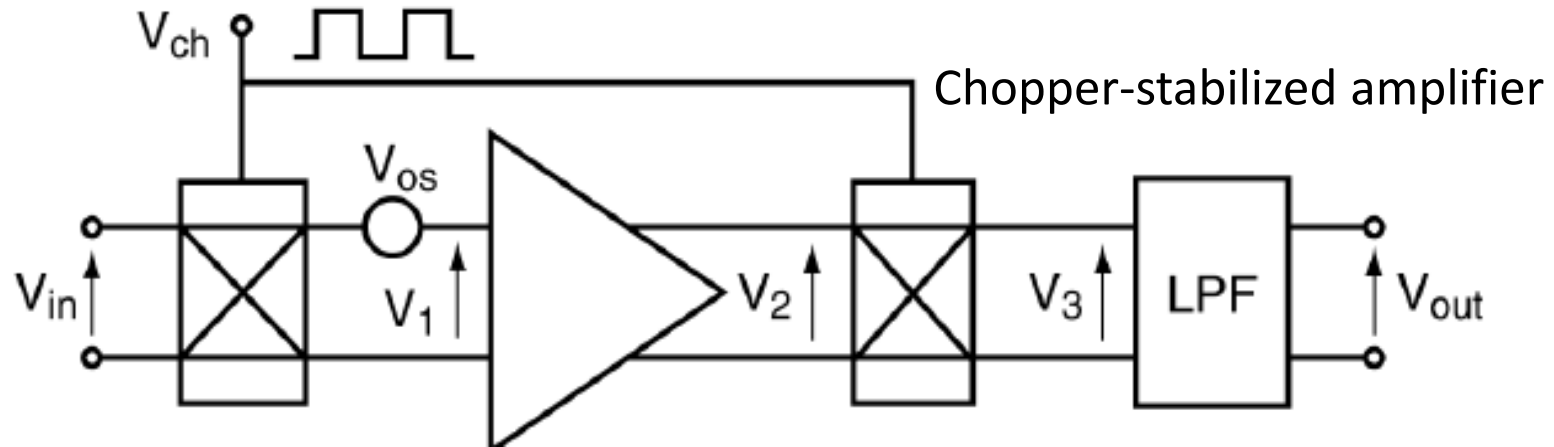
Spinning-Current Hall Sensor System



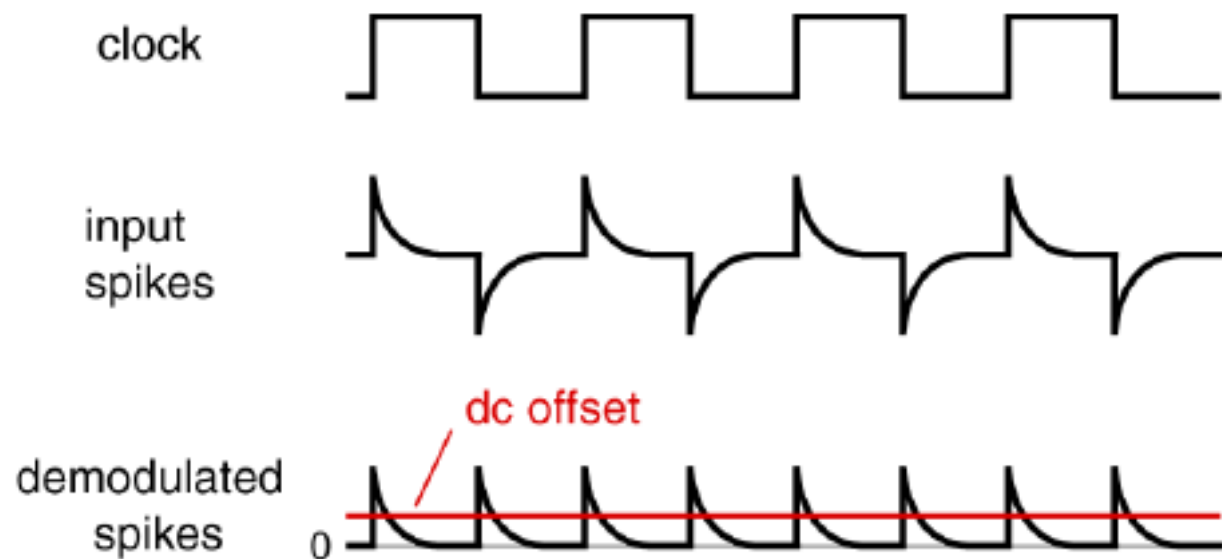
Spinning Current Hall System



Comparing Chopping with Spinning Current Technique

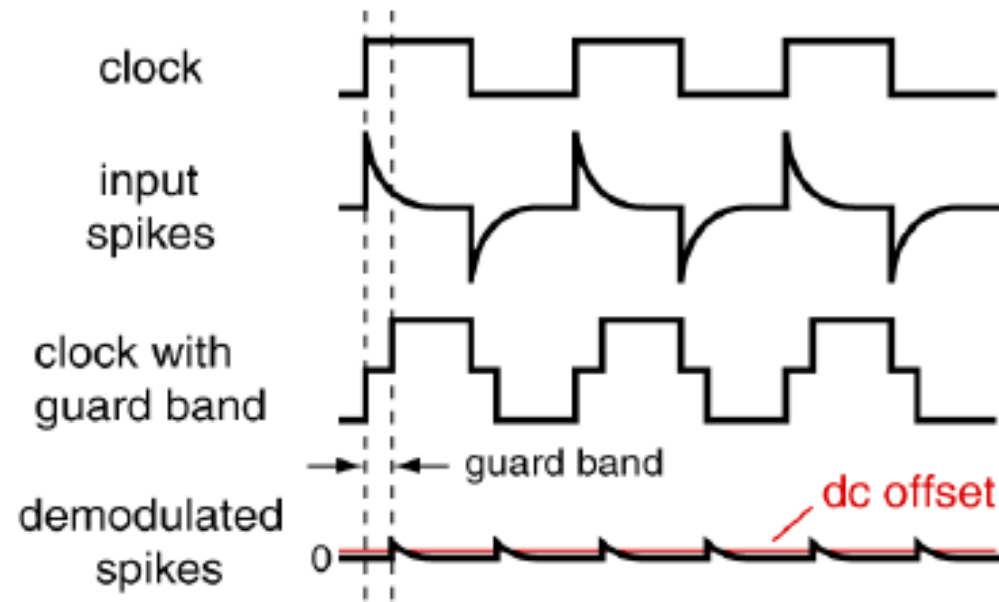


Residual Offset of Chopping (1)



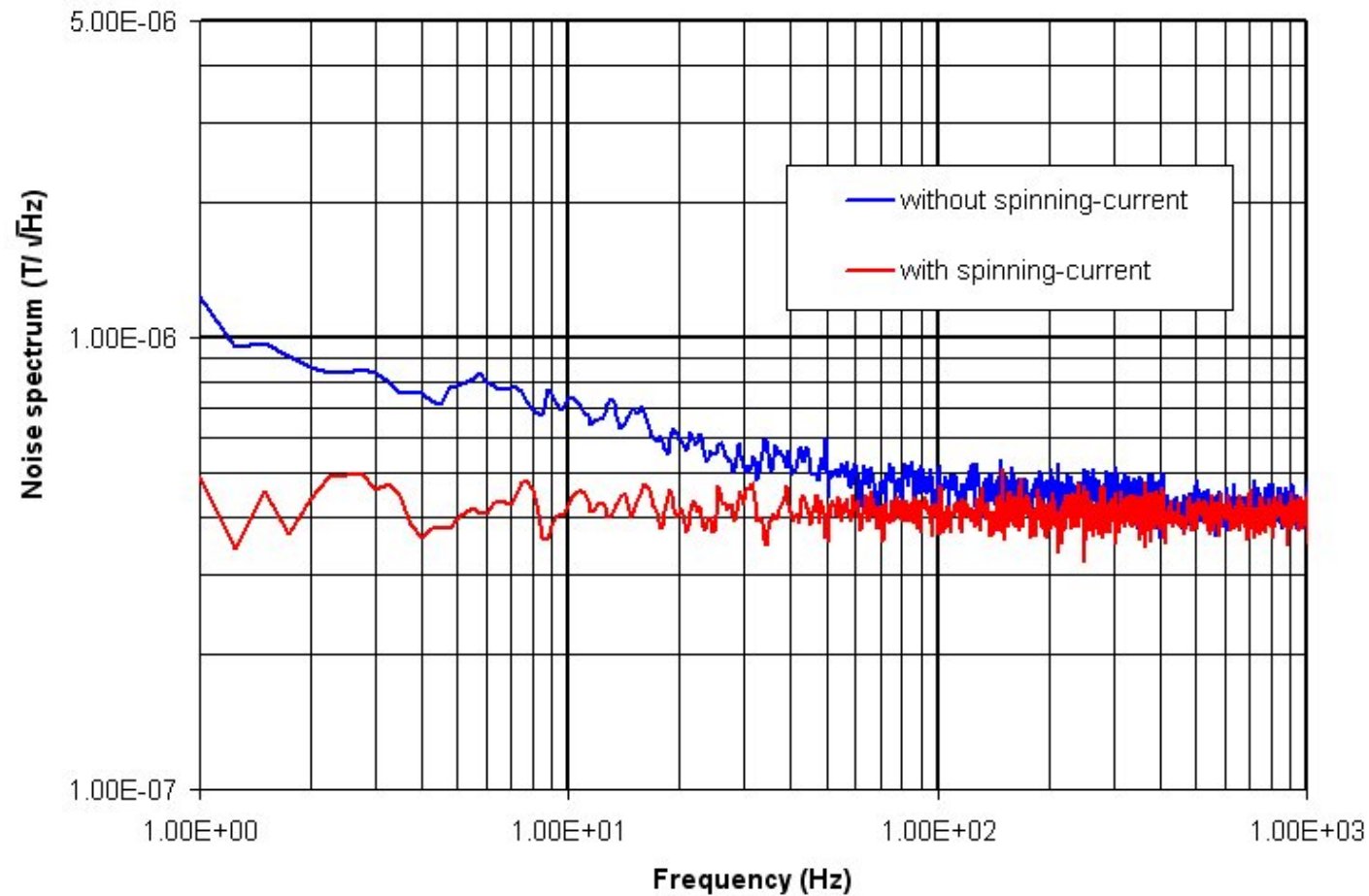
- Due to charge injection at the input chopper
- Causes a typical offset of a few μV
- Input spikes \Rightarrow bias current (a few tens of pA)

Chopper With Guard Band



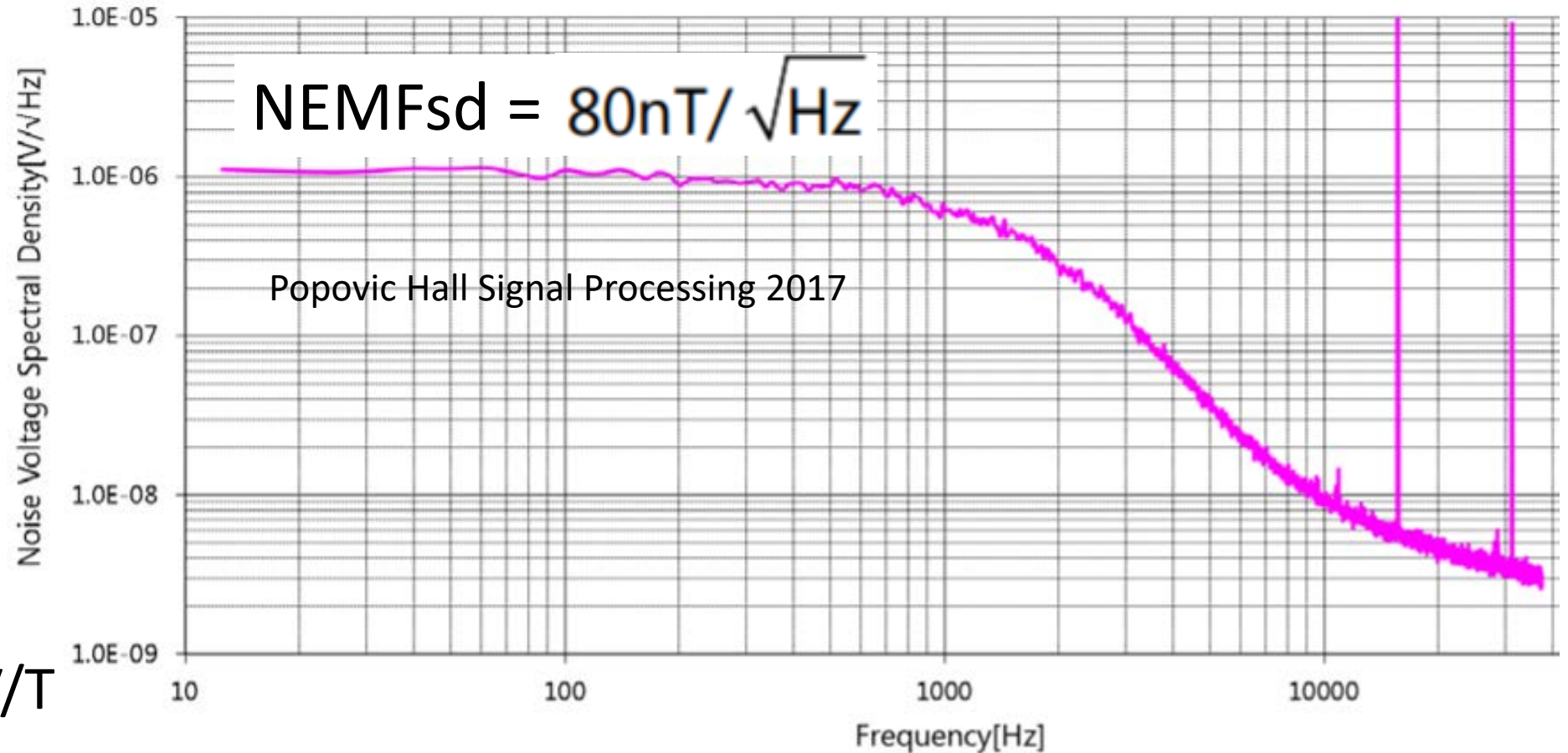
- During guard-band, output is shorted [15,16] or tri-stated [17]
- Residual offset $\sim 200\text{nV}$!
- Slightly worse noise performance

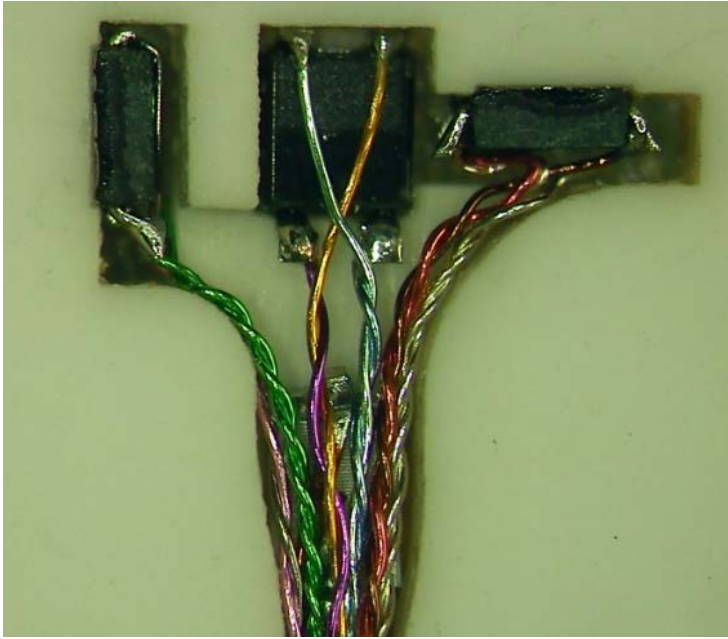
1/f noise reduction in a Hall device by the spinning-current



SENIS integrated vertical Hall device: Noise voltage spectral density with spinning current

Gain: 200
 $F_{\text{spin}} = 16\text{kHz}$
Sensitivity: 12.6V/T
BW = 1kHz

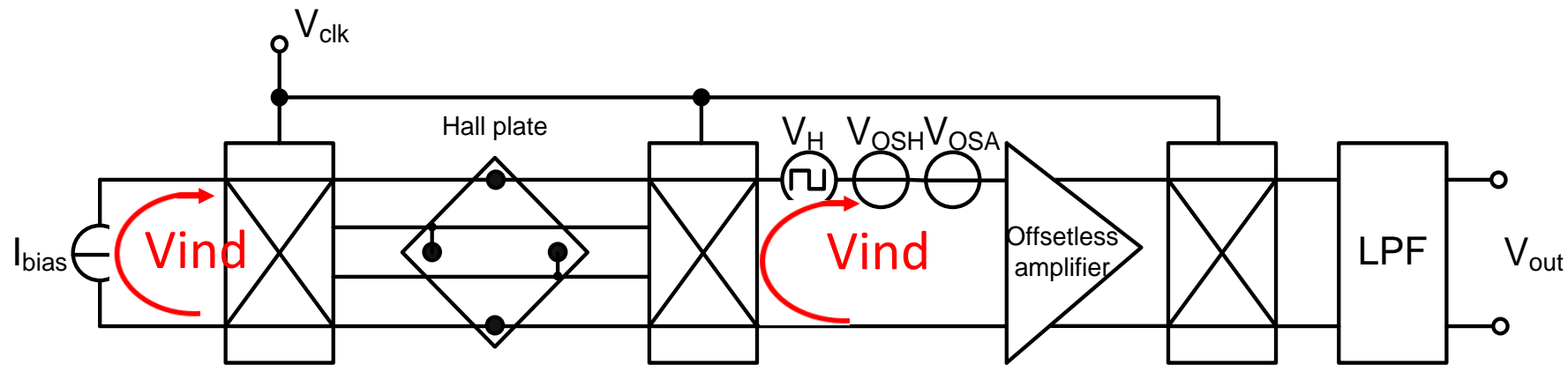




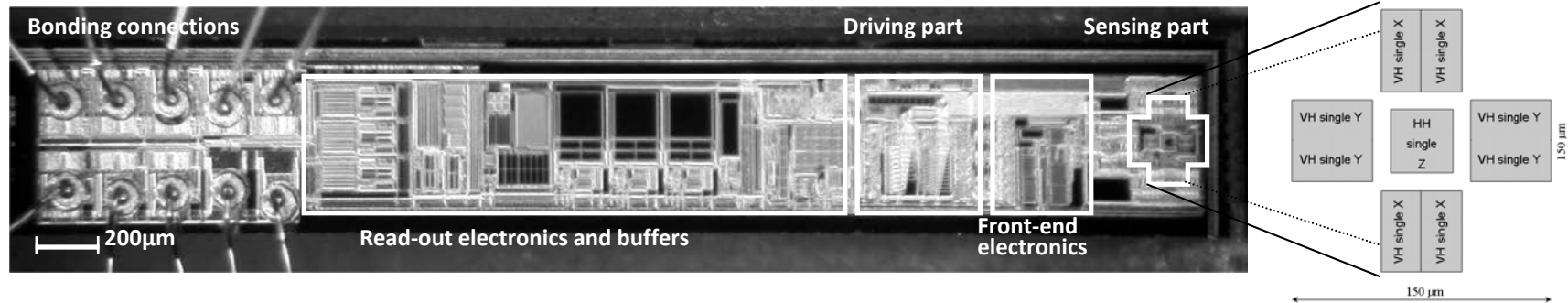
Reducing inductive effects

- Minimizing inductive loops
- Compensating inductive loops

- Biasing by a constant current
- Spinning current



Fully integrated 3D Hall probe



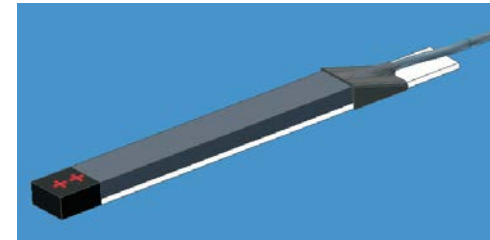
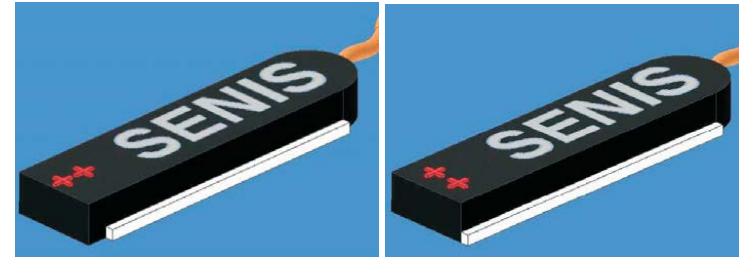
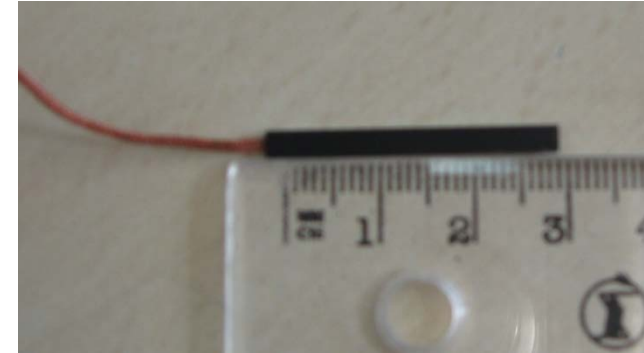
Precise 3D magnetic field measurements

- from militeslas up to tens of tesla
- in the frequency range from DC to 30 kHz
- spatial resolution of about 150 μm
- die dimensions: 4300 μm x 640 μm x 550 μm

Sensing part composed of two types of micro-Hall sensors

- a planar Hall sensor – the perpendicular B-component
- 8 vertical Hall sensors – the in-plane B-components

1ppm 2T Two-Axis Hall Transducer

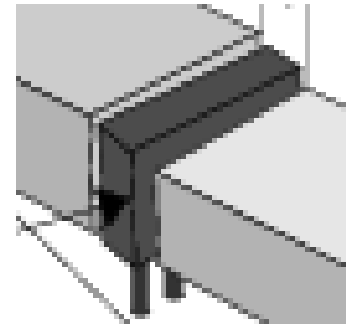
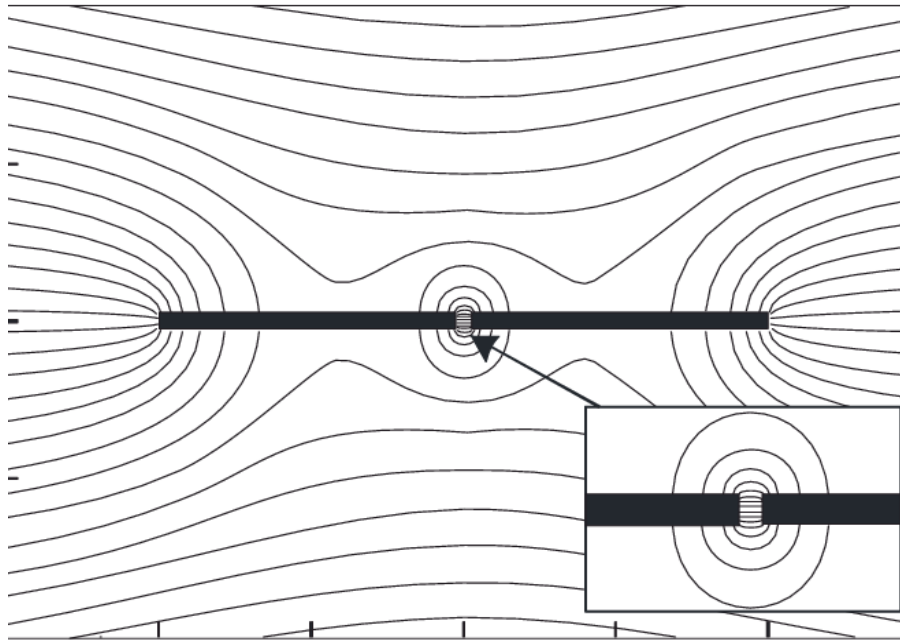


Key Features

▪ Measurement range	$\pm 2\text{T}$
▪ Frequency response	DC to 100Hz
▪ Broad-band Noise	$B_{\text{RMS}} < 0.5\mu\text{T}$
▪ Offset Drift	$B_{\text{OF,RMS}} < 0.4\mu\text{T}$
▪ Calibration Accuracy	10ppm
▪ Probe dimensions	$1.5 \times 3 \times 30 \text{ mm}^3$

Resolution: NEMF < 0.25 10^{-6} B-range

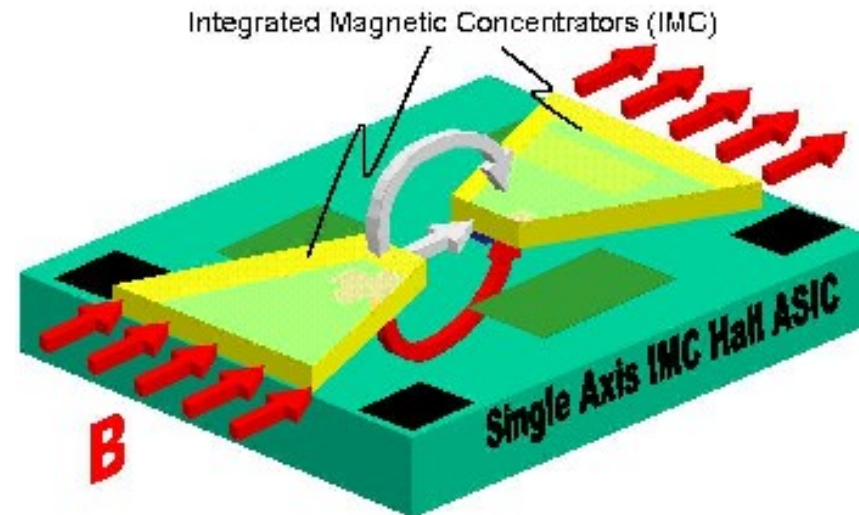
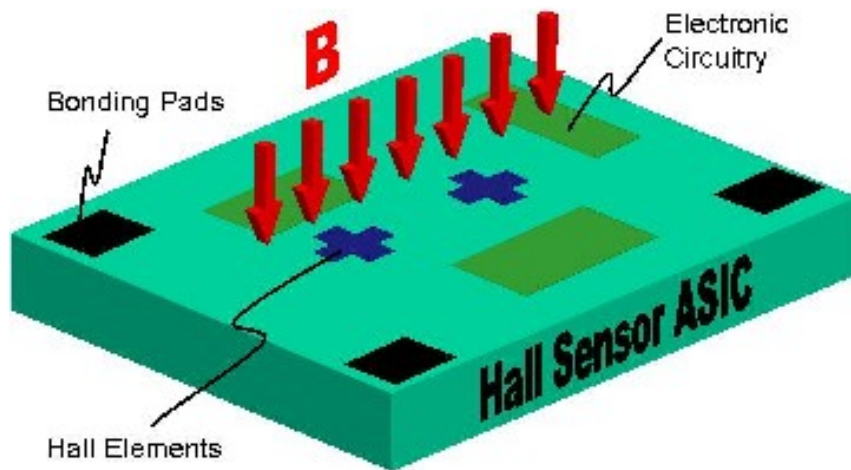
Amplifying the magnetic signal: the concept of 2 IMC - Hall



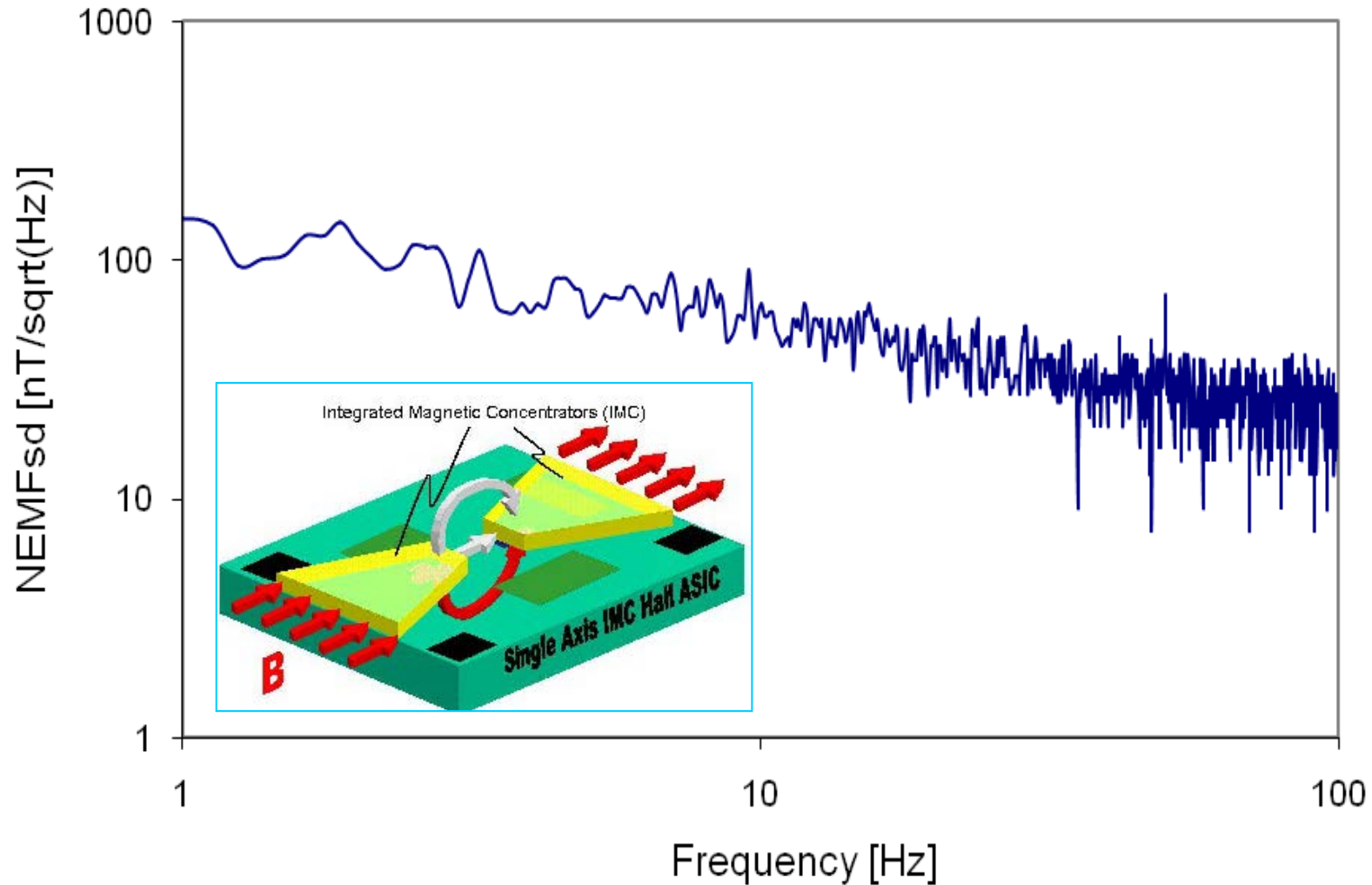
Magnetic Flux
Concentration
Gain:

$$G_{MC} = B_{Hall} / B_{ext}$$

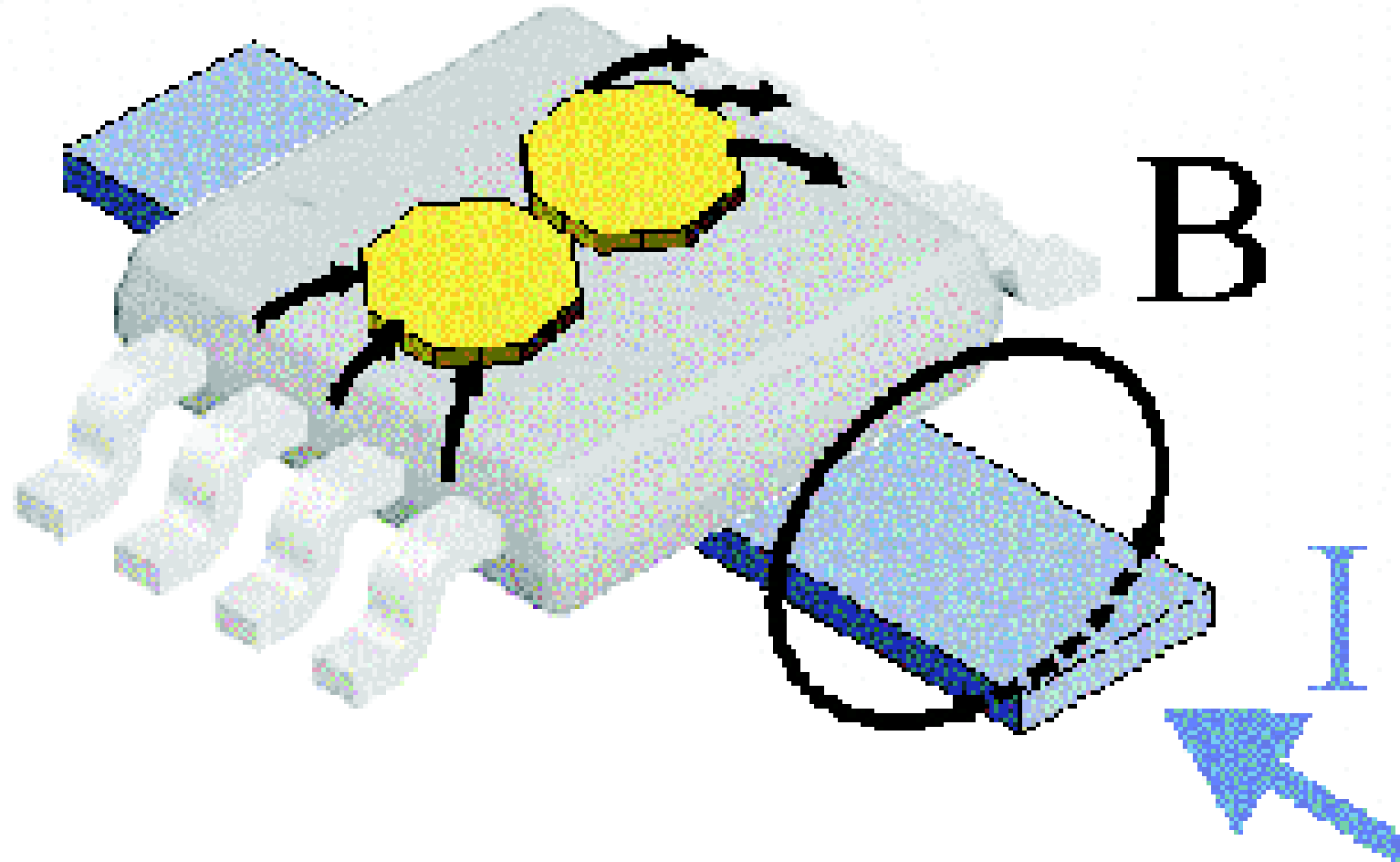
$$G_{MC} = 1 \dots 10$$



Measured NEMFsd CSA-1V (Sentron)



Application: Low Cost Current Sensor



PHYSICAL LIMIT OF RESOLUTION

(Thermal) Noise-Equivalent Magnetic Field spectral density:

$$\text{NEMFsd, min} \geq \sqrt{4 k T R_H} / (G_{MC} S_V V_b)$$

k – Boltz. constant; T – abs. temp.; R_H – resistance of Hall;
 G_{MC} – magn. gain of IMC; S_V - volt-rel. sensitivity; V_b - bias volt.

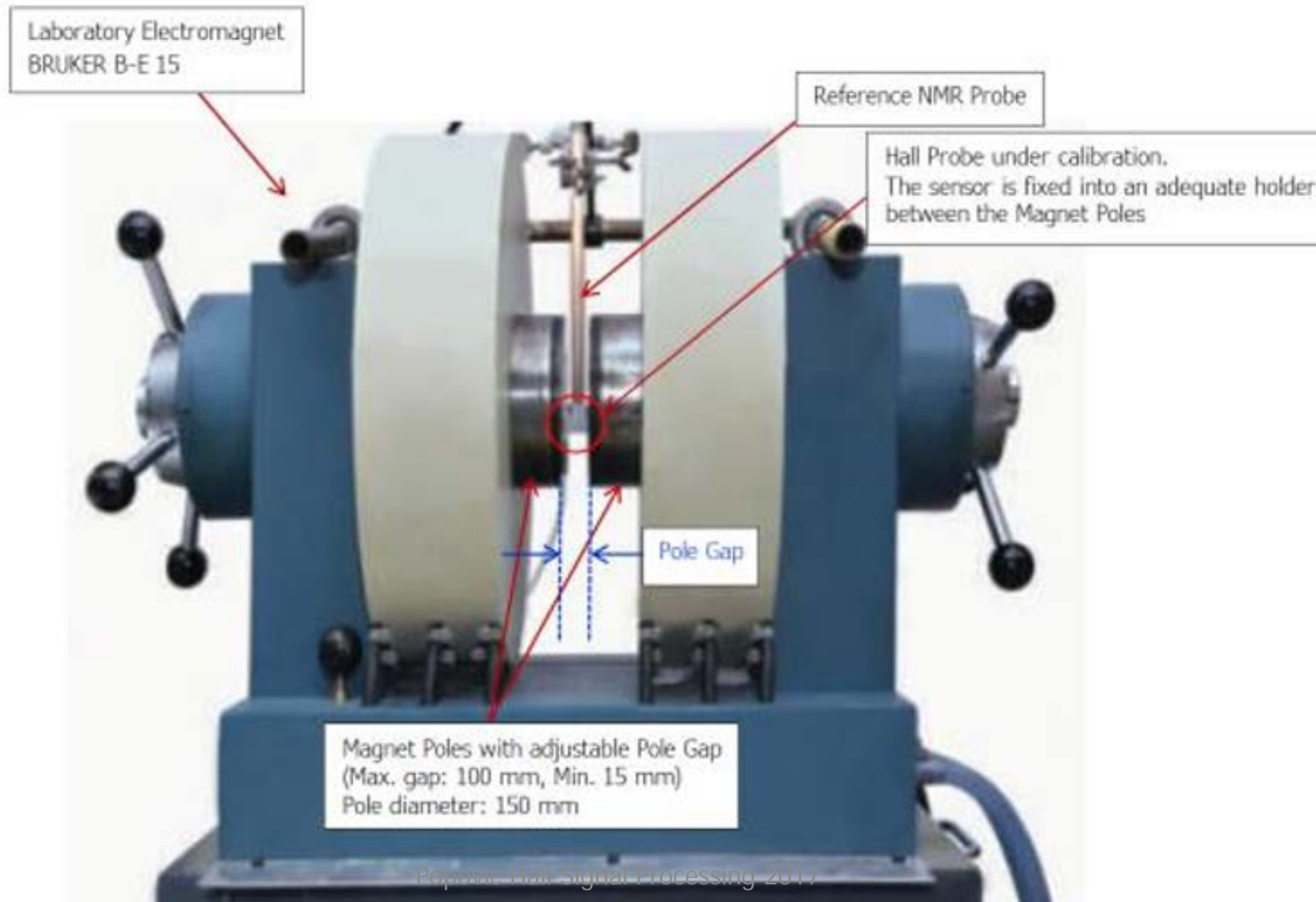
$$\text{NEMFsd, min} \geq \sqrt{4 k T} / (G_{MC} S_V \sqrt{P_b})$$

P_b : bias power of Hall, $P_b = V_b I_b$

For $S_V = 0.05$ (contemporary max for Si Hall) and $T = 300\text{K}$:

$$\text{NEMFsd, min} \geq 82 \text{ nT}/\sqrt{\text{Hz mW}} / G_{MC}$$

Electromagnet for calibrating Hall probes



Hall Voltage & Magnetic Sensitivity

Hall Voltage: $V_H = \int_{S1}^{S2} \mathbf{E}_H \, dw$

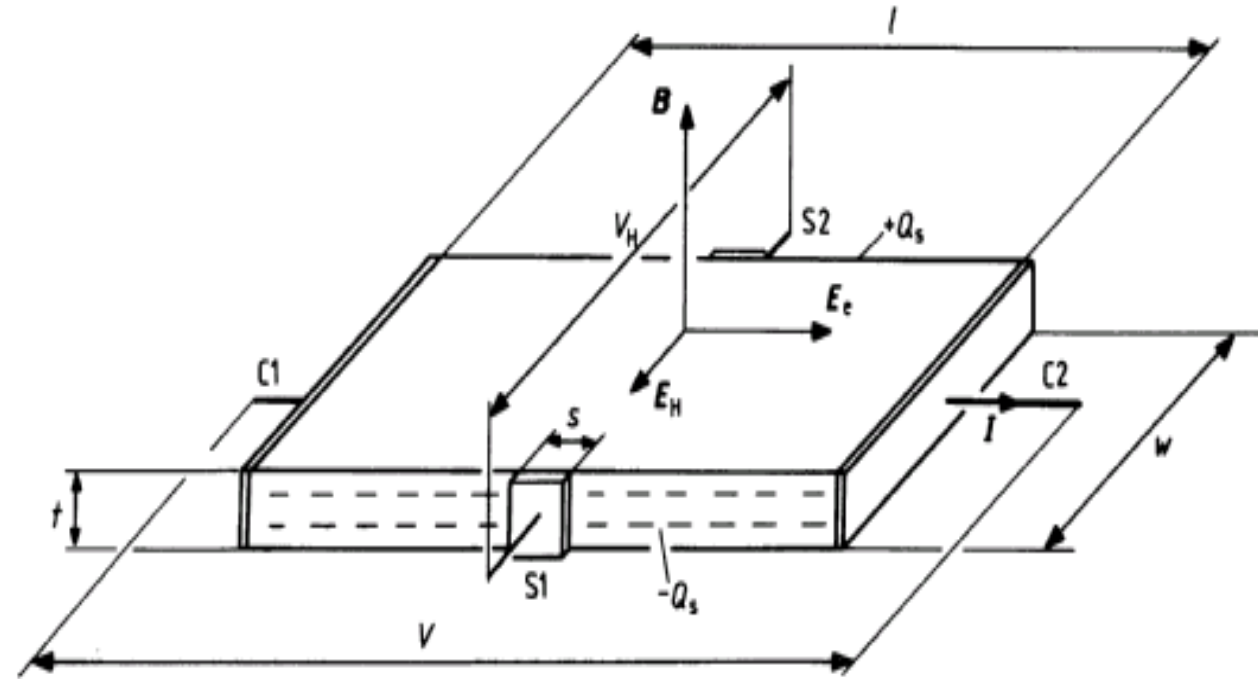
$$V_H = E_H w$$

$$\mathbf{E}_{Hn} = \mu_n [\mathbf{E} \times \mathbf{B}] \quad \Rightarrow \quad V_H = \mu_n \frac{V}{l} w B_{\perp} \quad \Rightarrow \quad V = RI = \frac{1}{q\mu_n n} \frac{l}{wt} I$$

$$V_H = S_V V B_{\perp}$$

Voltage-Related Sensitivity:

$$S_V \approx \mu_n \frac{w}{l}$$



$$V_H = S_I I B_{\perp}$$

Current-Related Sensitivity:

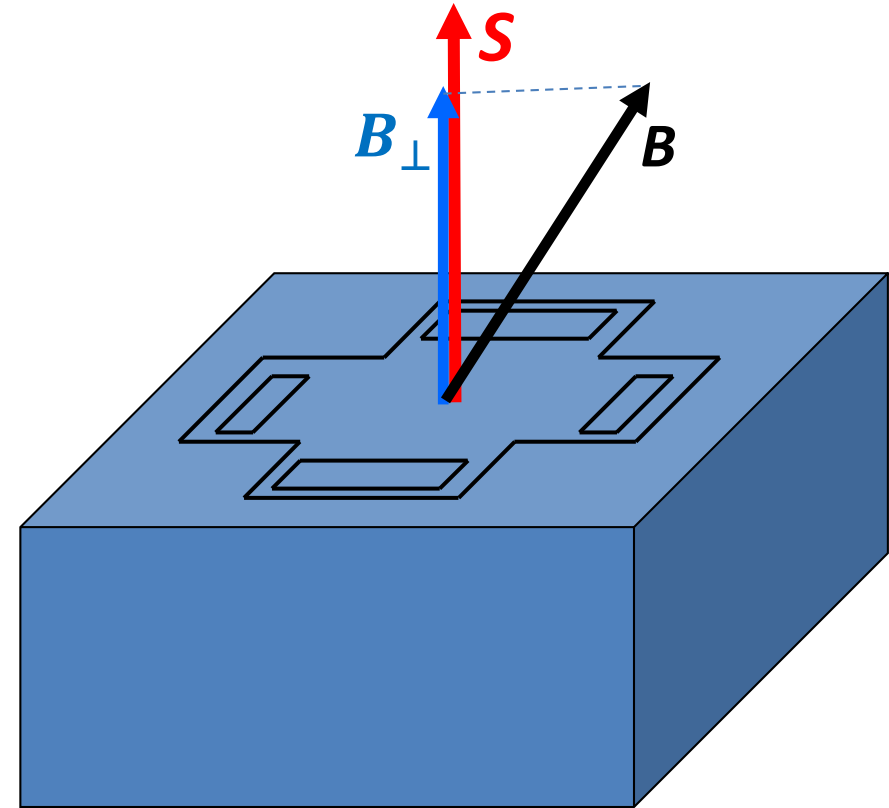
$$S_I \approx \frac{1}{q n t} \approx \frac{R_H}{t}$$

Magnetic Sensitivity Vector

Since

$$V_H = S_V V B_{\perp} \quad \text{and}$$

$$V_H = S_I I B_{\perp}$$



➔ $V_H = \mathbf{S} \cdot \mathbf{B}$ (the scalar product of \mathbf{S} and \mathbf{B})

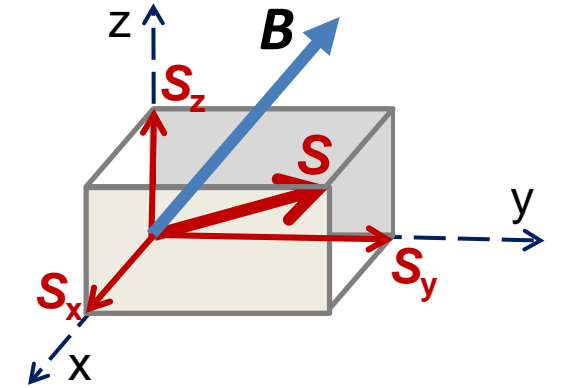
\mathbf{S} : Magnetic Sensitivity Vector of a Hall device

$$U_{out} = S_X \cdot B_X + S_Y \cdot B_Y + S_Z \cdot B_Z$$

Magnetic Sensitivity Tensor

1 - axis Hall magnetic sensor:

$$V_1 = \mathbf{S}_1 \cdot \mathbf{B} \quad \Rightarrow \quad V_1 = (S_{1X} \quad S_{1Y} \quad S_{1Z}) \begin{pmatrix} B_X \\ B_Y \\ B_Z \end{pmatrix}$$

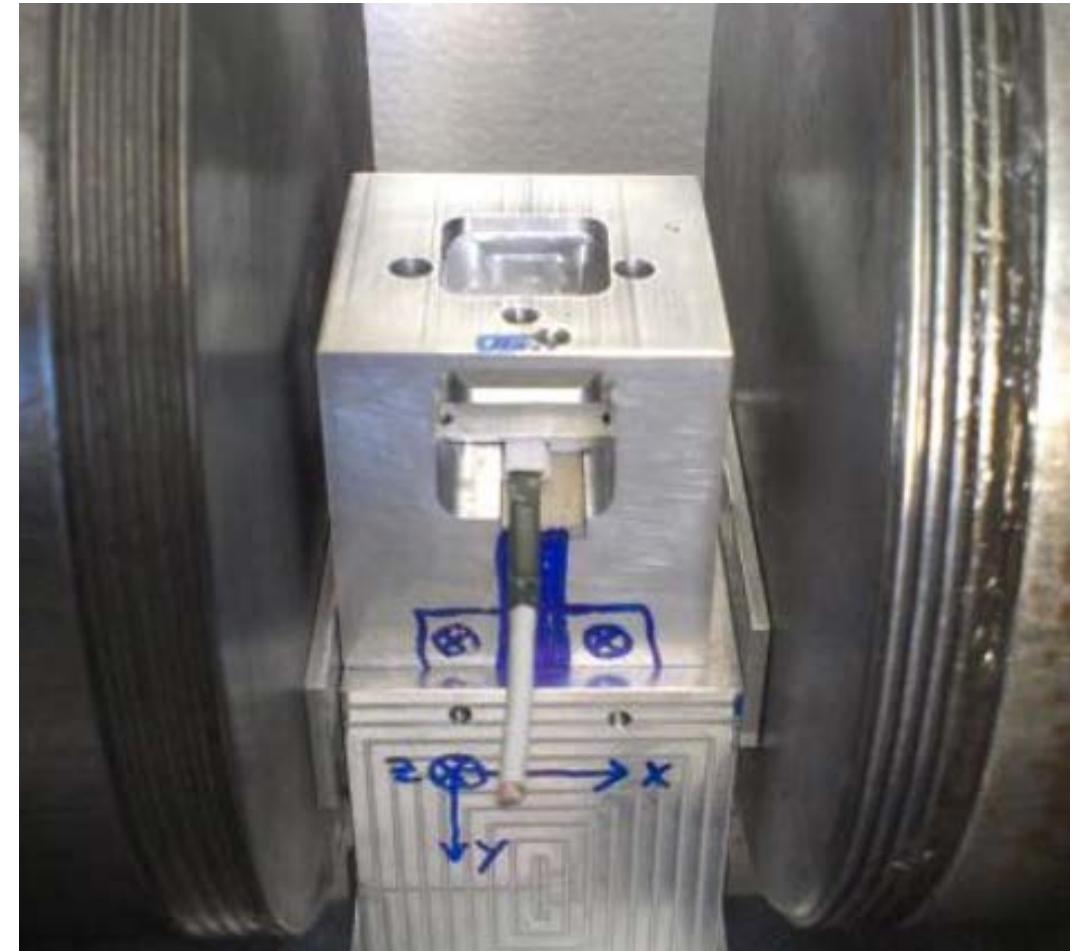
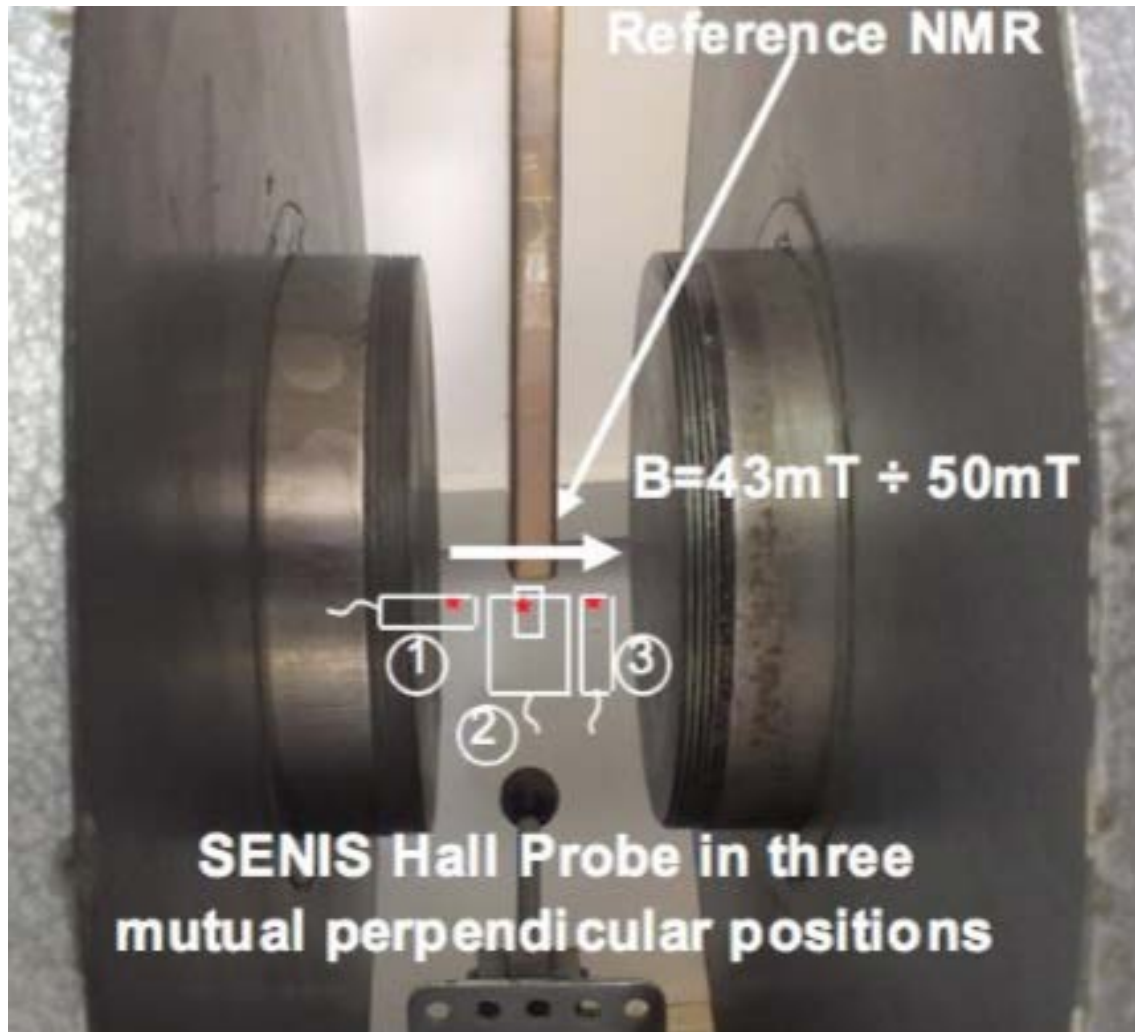


3 - axis Hall magnetic sensor:

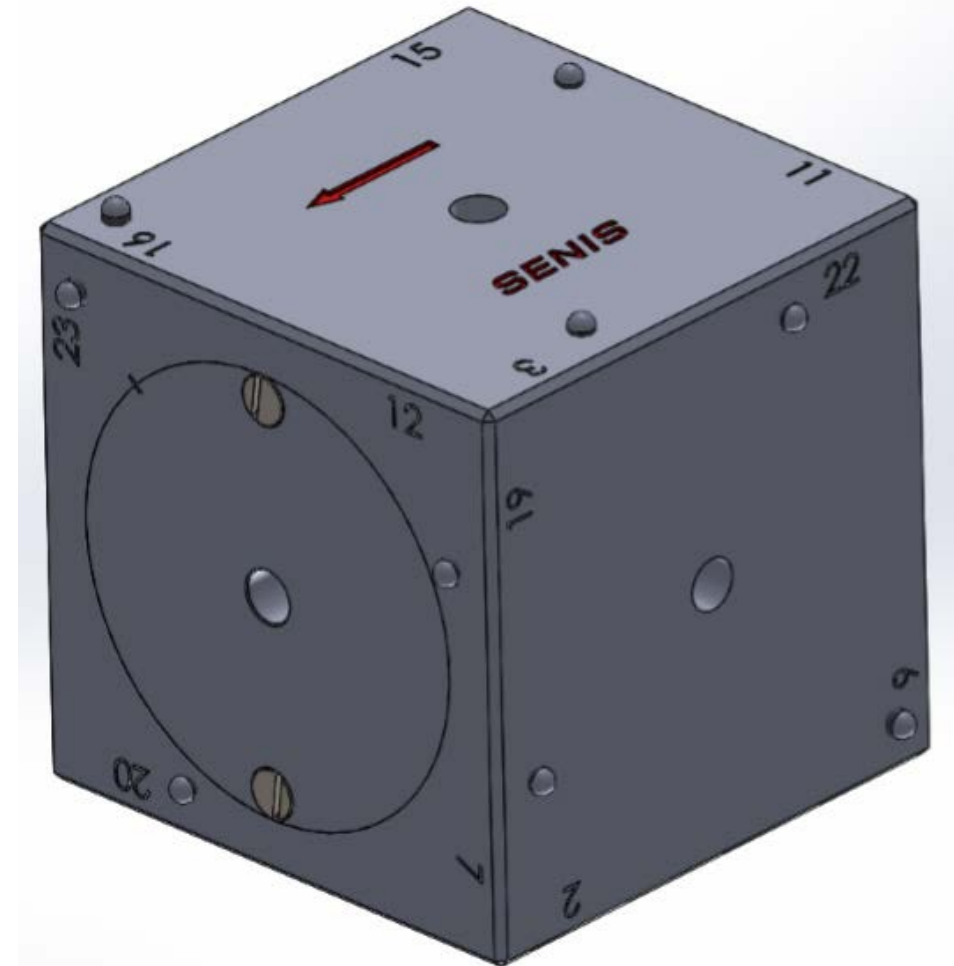
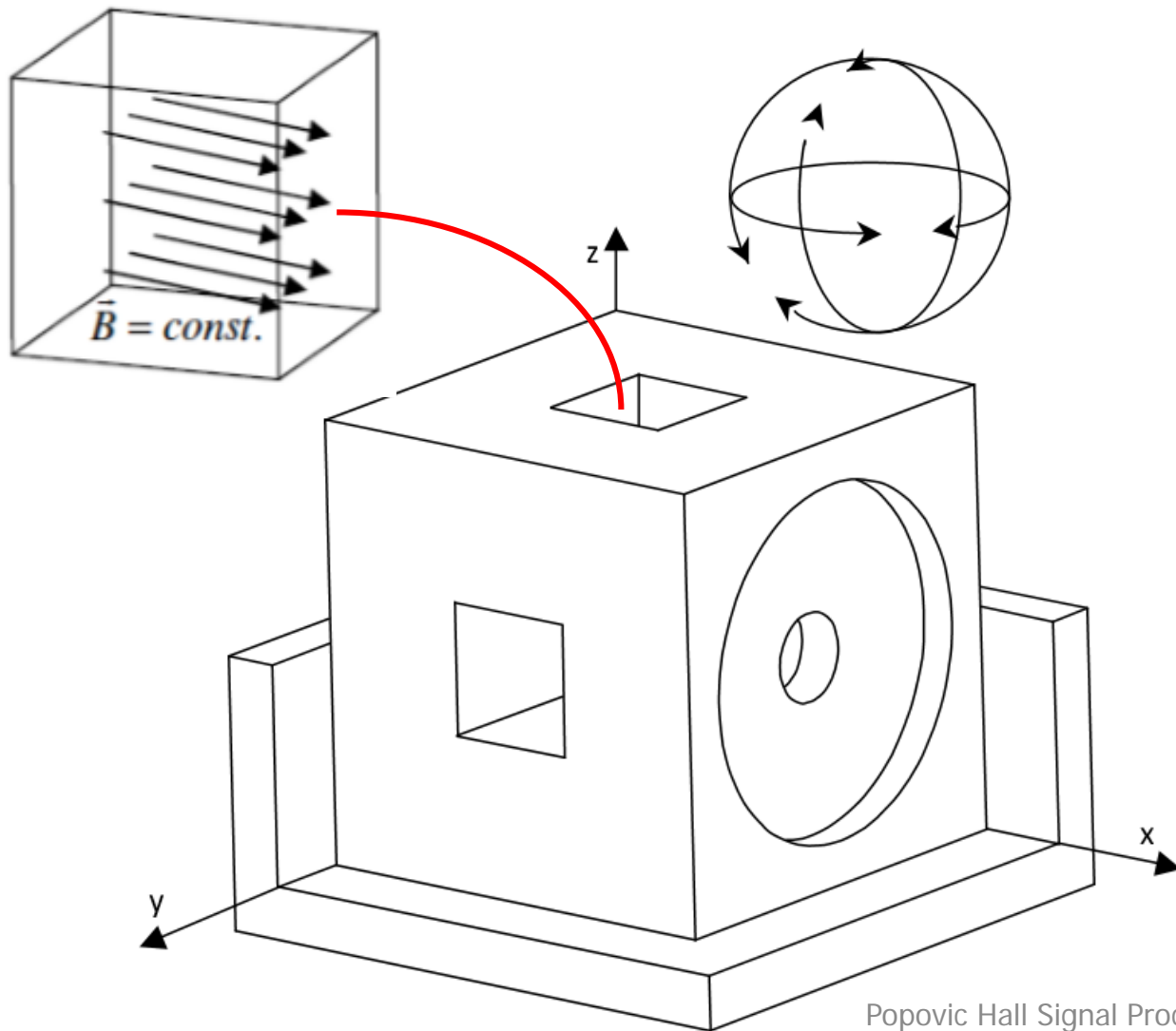
$$\begin{pmatrix} V_1 \\ V_2 \\ V_3 \end{pmatrix} = \begin{pmatrix} S_{1X} & S_{1Y} & S_{1Z} \\ S_{2X} & S_{2Y} & S_{2Z} \\ S_{3X} & S_{3Y} & S_{3Z} \end{pmatrix} \begin{pmatrix} B_X \\ B_Y \\ B_Z \end{pmatrix} \quad \Rightarrow \quad \mathbf{V}_3 = (\mathbf{S}_3) \mathbf{B} \quad \Rightarrow \quad \mathbf{B} = (\mathbf{S}_3)^{-1} \mathbf{V}_3$$

(\mathbf{S}_3) : Magnetic Sensitivity Tensor of a 3-Axis Hall Probe

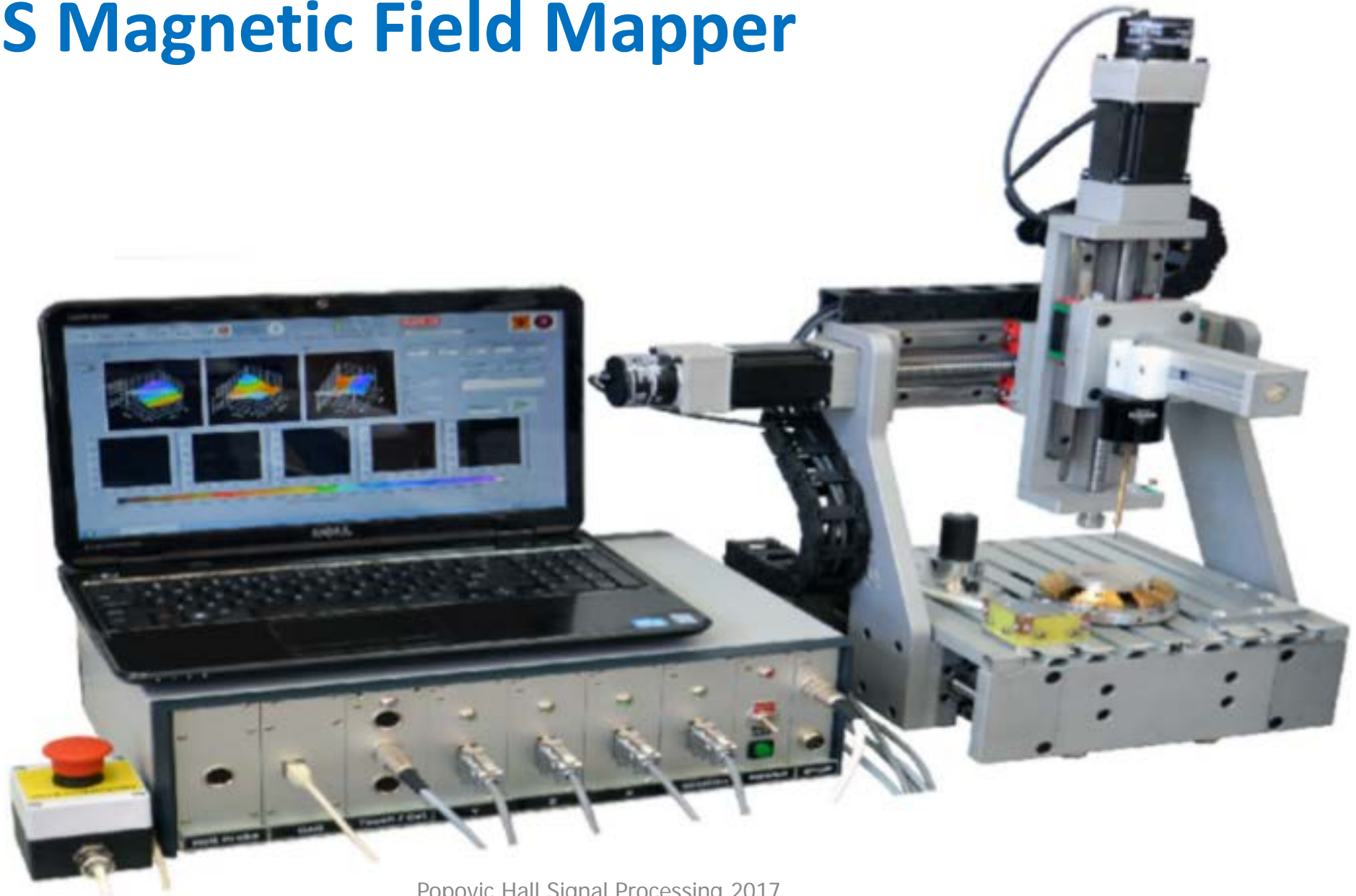
Calibrating the magnetic sensitivity tensor in an electromagnet



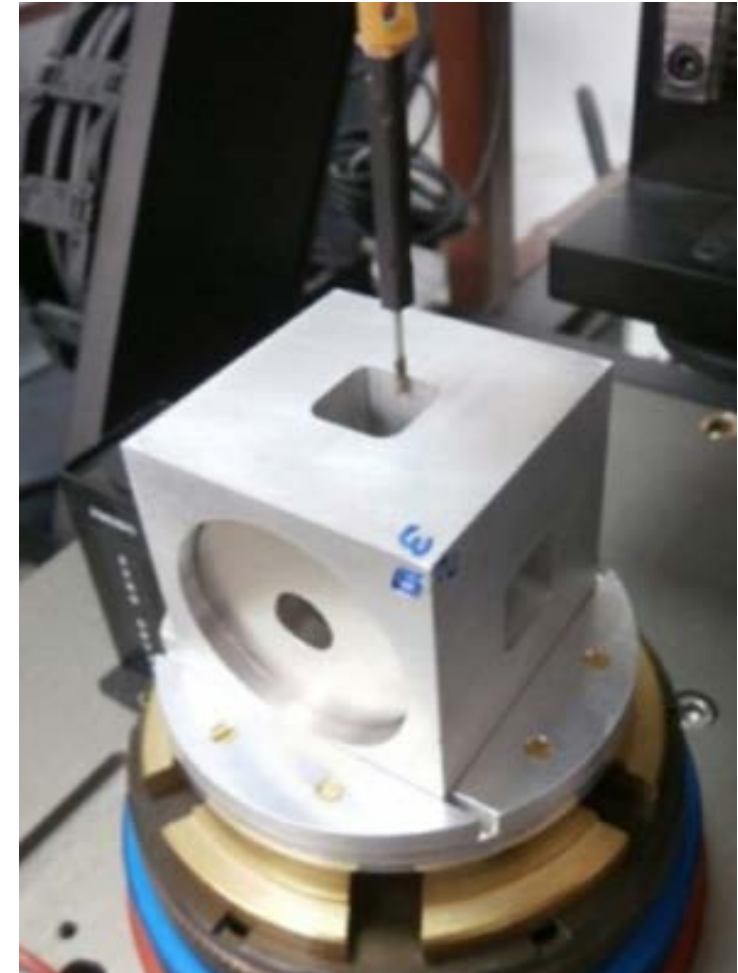
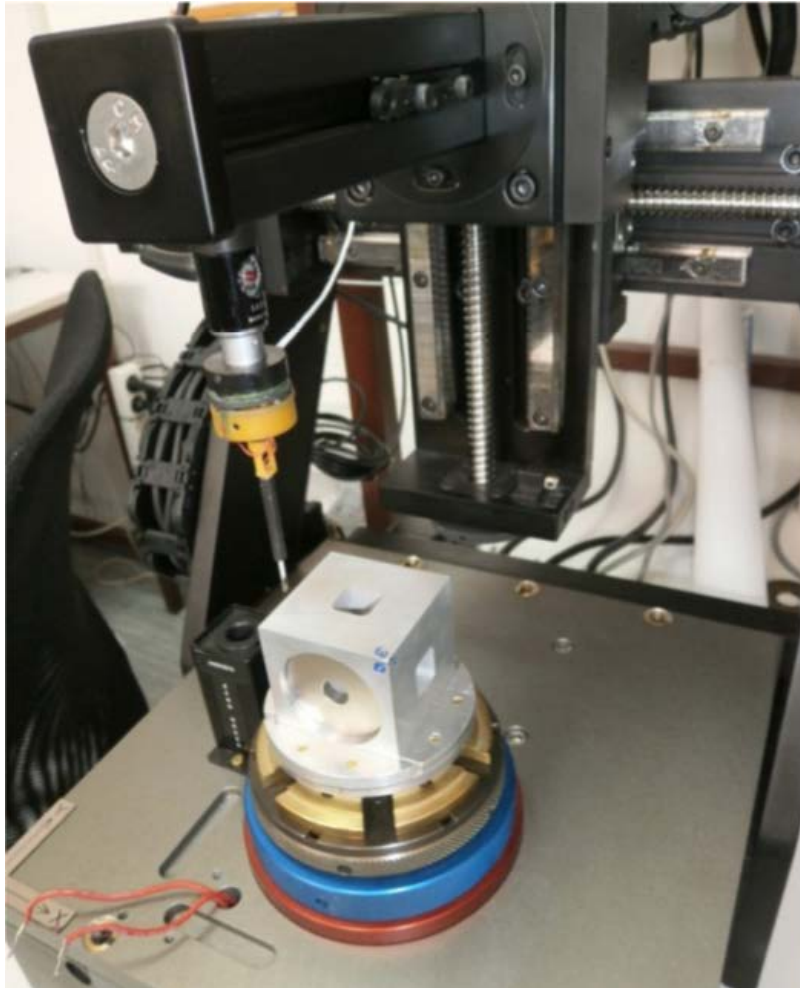
A tool for calibrating the magnetic sensitivity tensor



SENIS Magnetic Field Mapper



Calibration of the magnetic sensitivity tensor of a 3D Hall probe in the mapper



Calibration of the Magnetic Sensitivity Tensor - an example

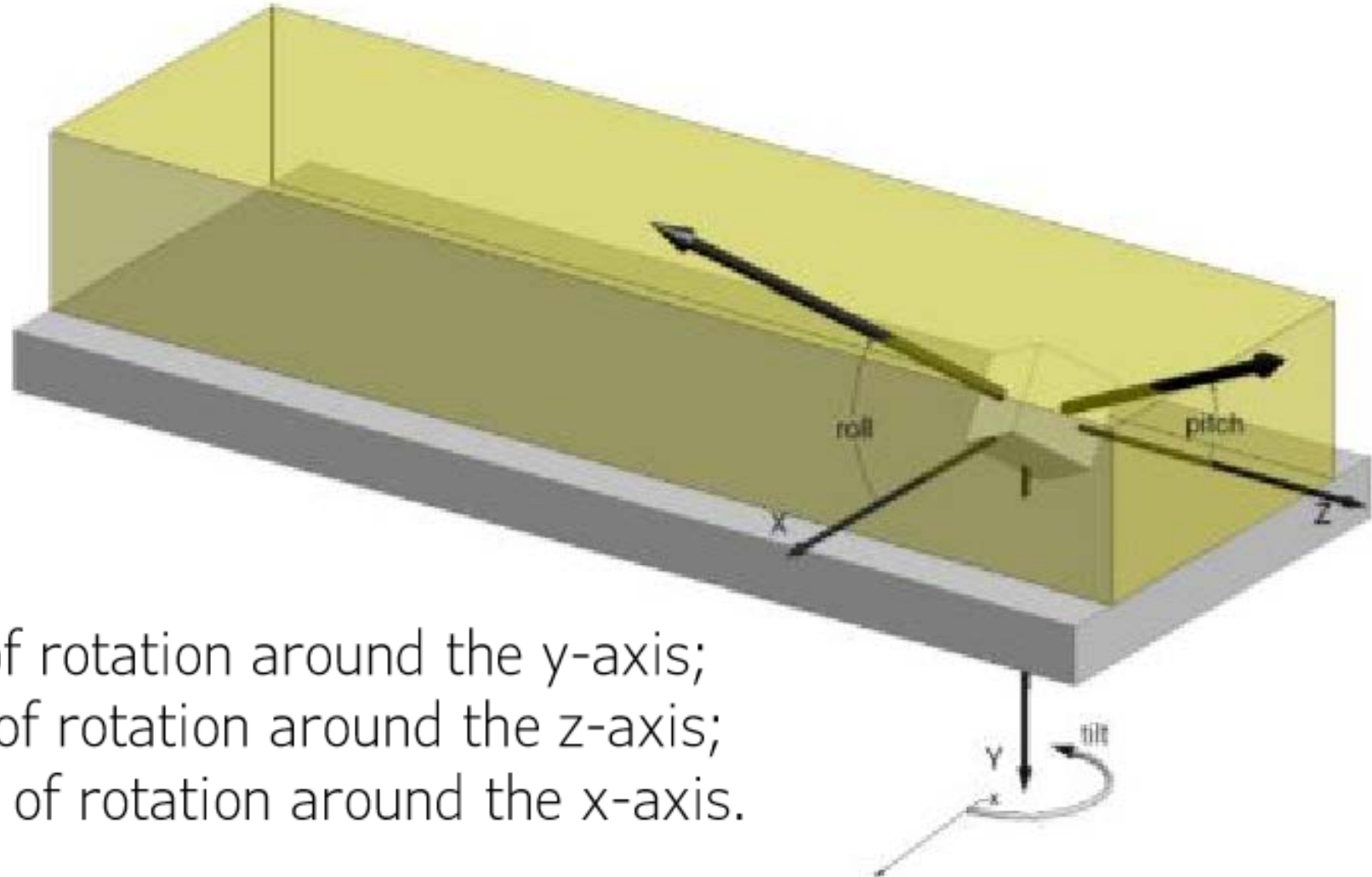
$$[S] = \begin{bmatrix} S_{xx} & S_{xy} & S_{xz} \\ S_{yx} & S_{yy} & S_{yz} \\ S_{zx} & S_{zy} & S_{zz} \end{bmatrix} = \begin{bmatrix} 96.6577 & 25.6285 & 2.44729 \\ -25.5293 & 96.6622 & 1.95327 \\ -2.4162 & -2.69085 & 99.9925 \end{bmatrix} \quad \text{Before...}$$

**... and after
Calibration**

$$[S] = \begin{bmatrix} 100.002 & 0.0298746 & -0.00891582 \\ -0.103873 & 100.038 & 0.0110116 \\ 0.0138412 & -0.0328856 & 100.041 \end{bmatrix}$$

$$[S] \approx S_s \bullet [I] \quad S_s = 100\text{V/T}$$

Definition of the angular errors of a probe



TILT is the angle of rotation around the y-axis;
ROLL is the angle of rotation around the z-axis;
PITCH is the angle of rotation around the x-axis.

Measurement of the angular errors of a 3D probe - an example

$$\begin{vmatrix} S_{XX} & S_{XY} & S_{XZ} \\ S_{YX} & S_{YY} & S_{YZ} \\ S_{ZX} & S_{ZY} & S_{ZZ} \end{vmatrix} = \begin{vmatrix} 100.009 & -6.758 & -1.095 \\ 5.517 & 100.000 & 0.055 \\ 0.304 & -1.695 & 100.052 \end{vmatrix}$$

...

$$B_c \cdot S_x = \sqrt{\frac{U_{xx}^2 + U_{xy}^2 + U_{xz}^2 + \sqrt{(U_{xx}^2 + U_{xy}^2 + U_{xz}^2)^2 - 4 \cdot U_{xy}^2 \cdot U_{xz}^2}}{2}}$$

$$x_r = \arcsin\left(\frac{U_{xy}}{B_c \cdot S_x}\right)$$

$$x_t = \arcsin\left(\frac{U_{xz}}{B_c \cdot S_x}\right)$$

...

$$X_{\text{roll}} (^{\circ}) = -3.87$$

$$X_{\text{tilt}} (^{\circ}) = -0.63$$

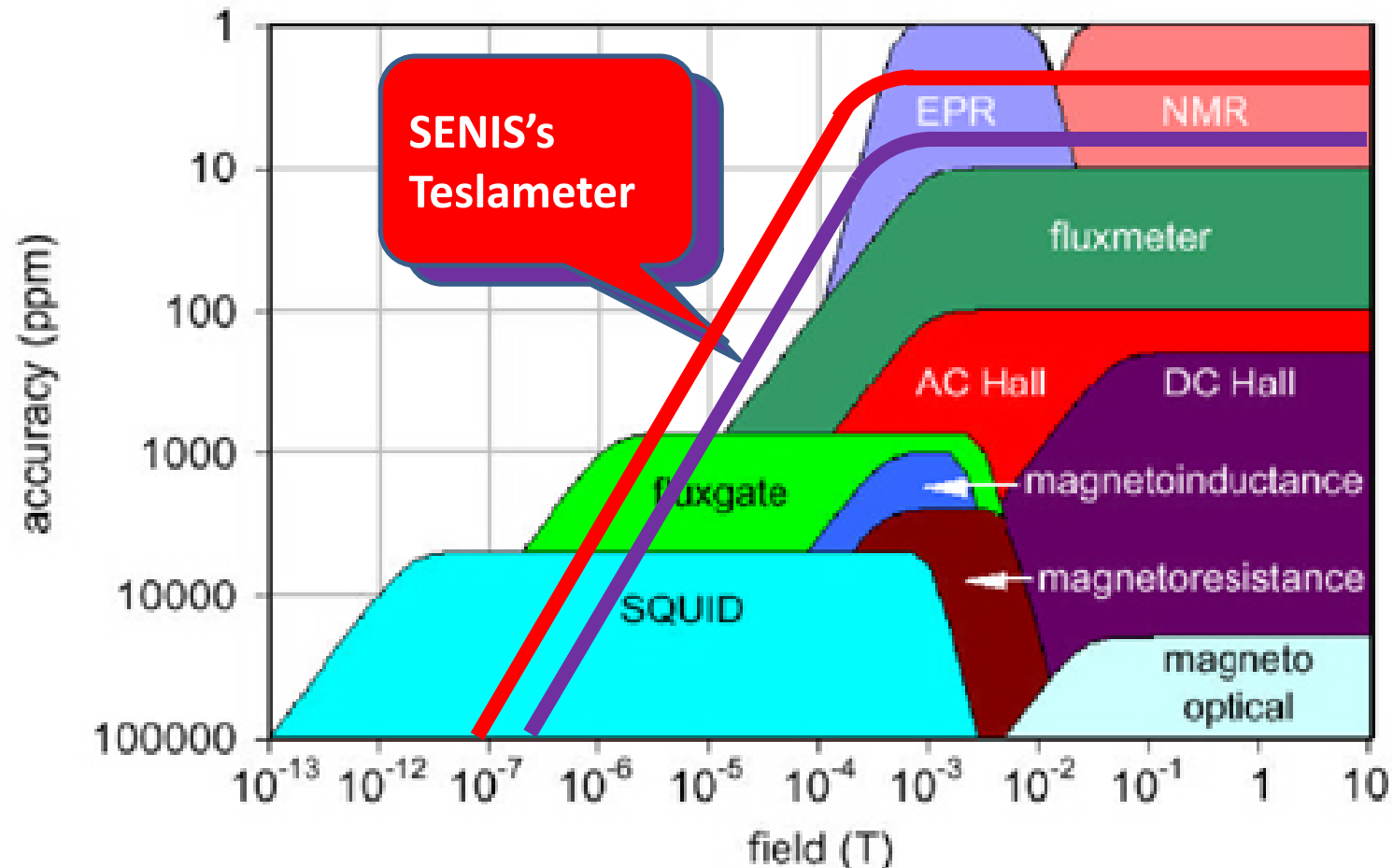
$$Y_{\text{roll}} (^{\circ}) = 3.16$$

$$Y_{\text{pitch}} (^{\circ}) = 0.03$$

$$Z_{\text{pitch}} (^{\circ}) = -0.97$$

$$Z_{\text{tilt}} (^{\circ}) = 0.17$$

Up-dated classification of magnetic measurement technologies*



*Luca Bottura of CERN; Revised by SENIS 2011