



ETH zürich

D MAVT *Chair of Micro- and Nanosystems*

Hallcube - from prototype to product

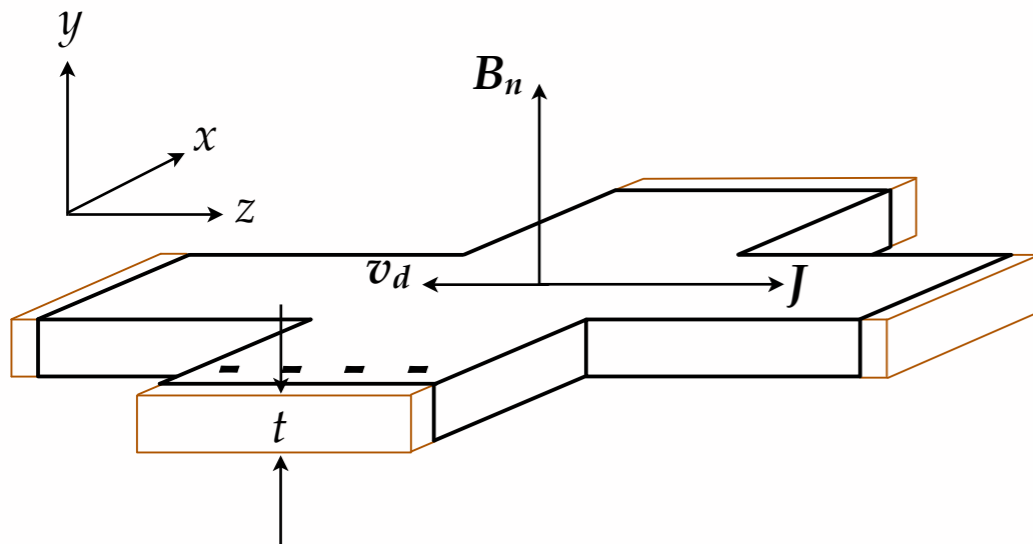
Christina Wouters

IMMW20, Diamond Light Source, 06.06.2017

1D to 3D Hall sensors

- Hall sensor considerations: offset, linearity, sensitivity, temp. coeff., angular alignment, planar Hall effect, induced voltages, noise, magnetoresistance, active area/volume, stability

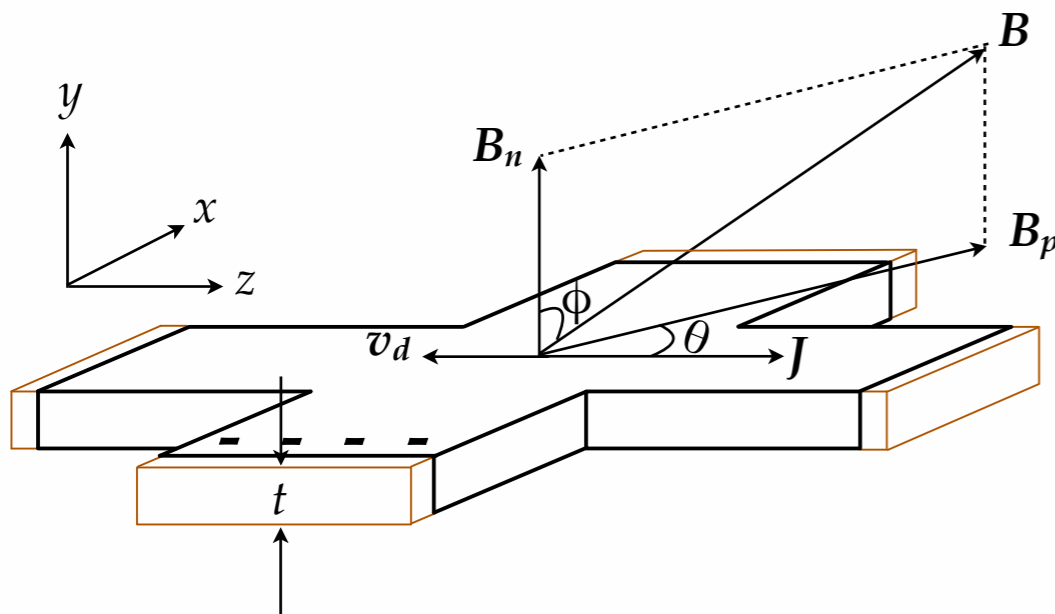
$$V_{out} = V_H + V_{PH} = R_H \frac{I}{t} B_y + R_{PH} \frac{I}{t} B_x B_z = R_H \frac{I}{t} B_n + R_{PH} \frac{I}{2t} B_p^2 \sin 2\theta$$



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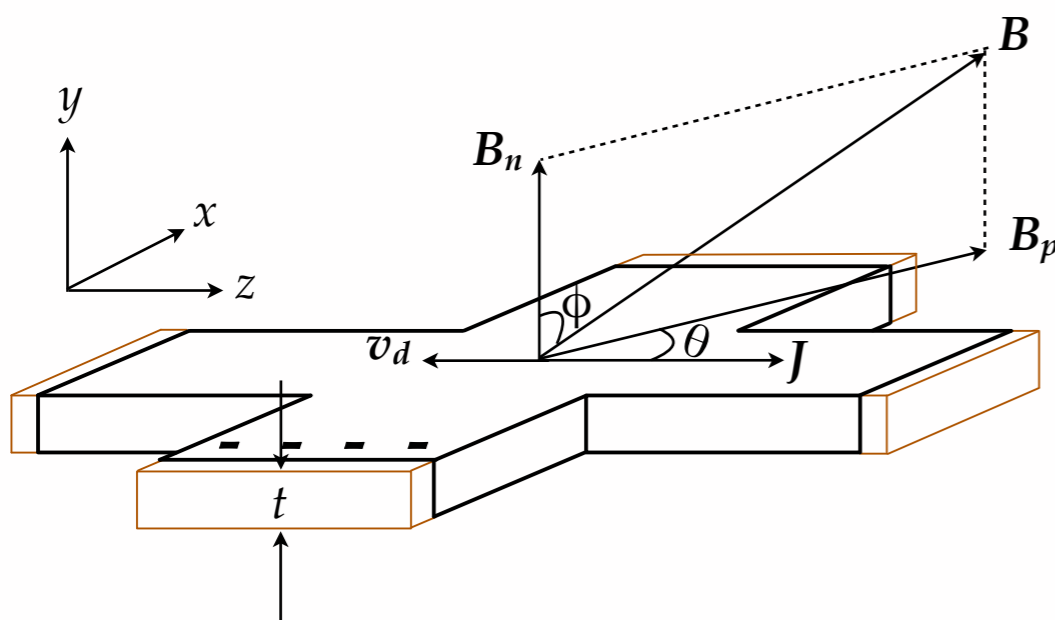
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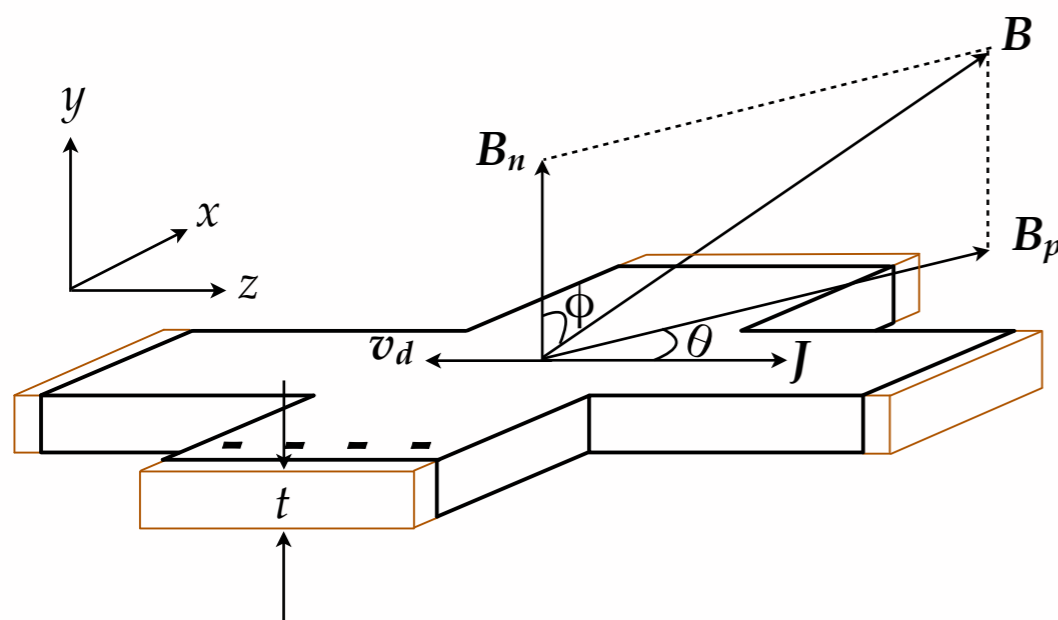
100 ppm accuracy at 1 T (1 Gauss) can be routinely achieved with 1D Hall sensors:

- Precision electronics
- Careful sensor alignment
- Temperature stabilization or control
- Repeated, thorough sensor calibration

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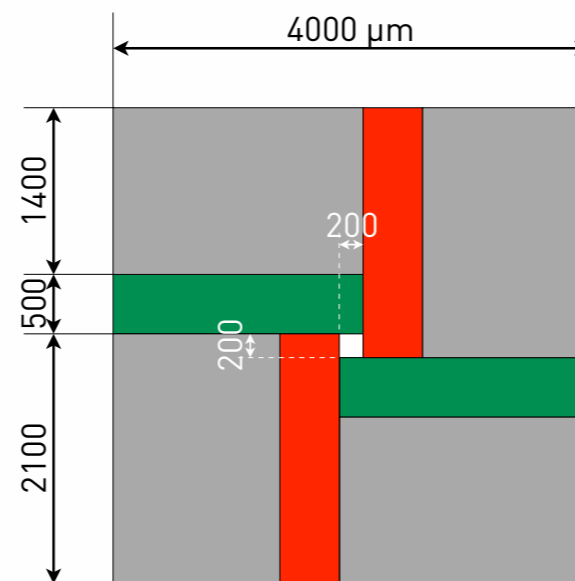
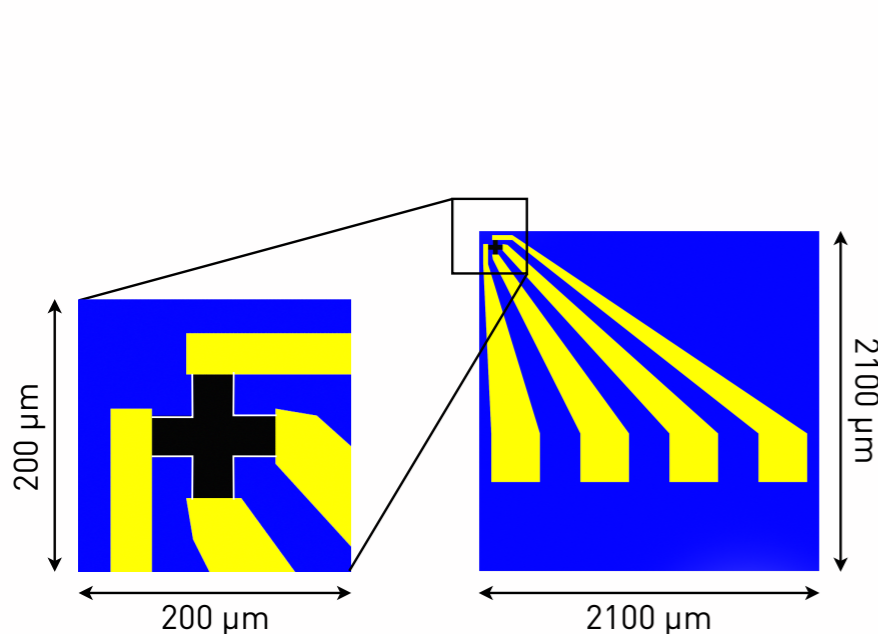
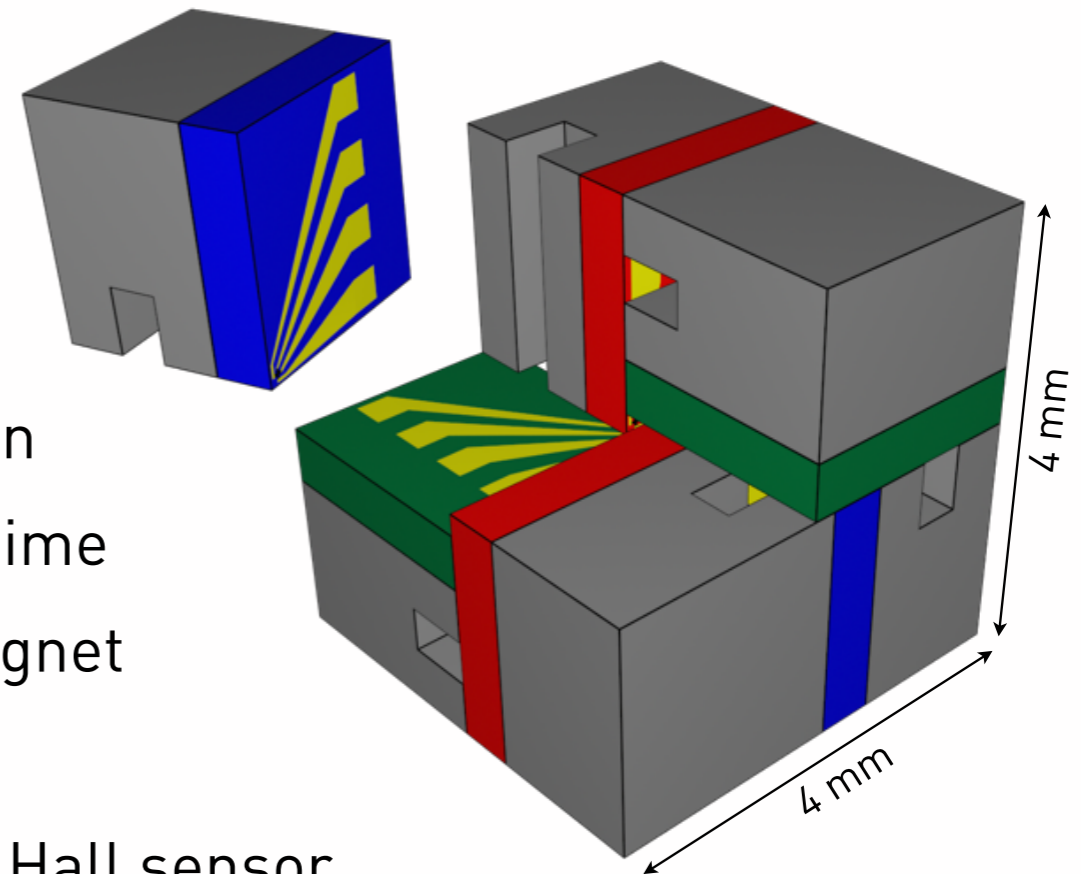


100 ppm accuracy at 1 T (1 Gauss) can be routinely achieved with 1D Hall sensors:

- Precision electronics
 - Careful sensor alignment
 - Temperature stabilization or control
 - Repeated, thorough sensor calibration
- Exploit the good precision of 1D Hall sensors (“Hall plates”) to create from them an equally good **3D Hall sensor**

Hallcube in a nutshell

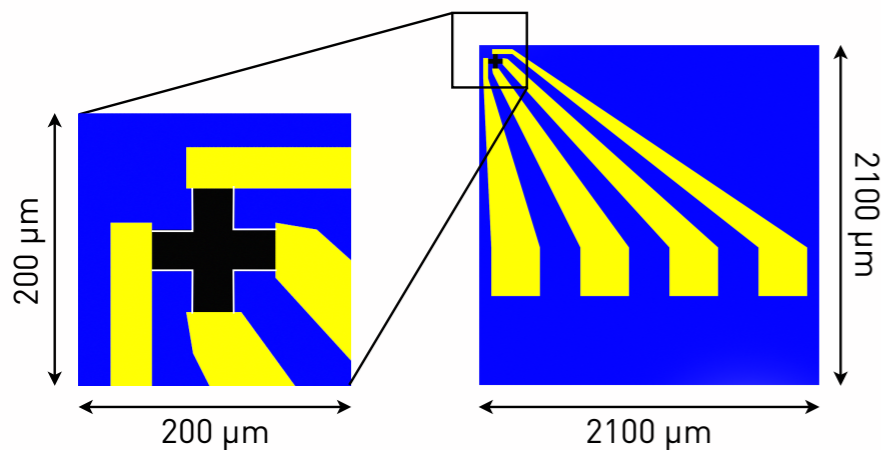
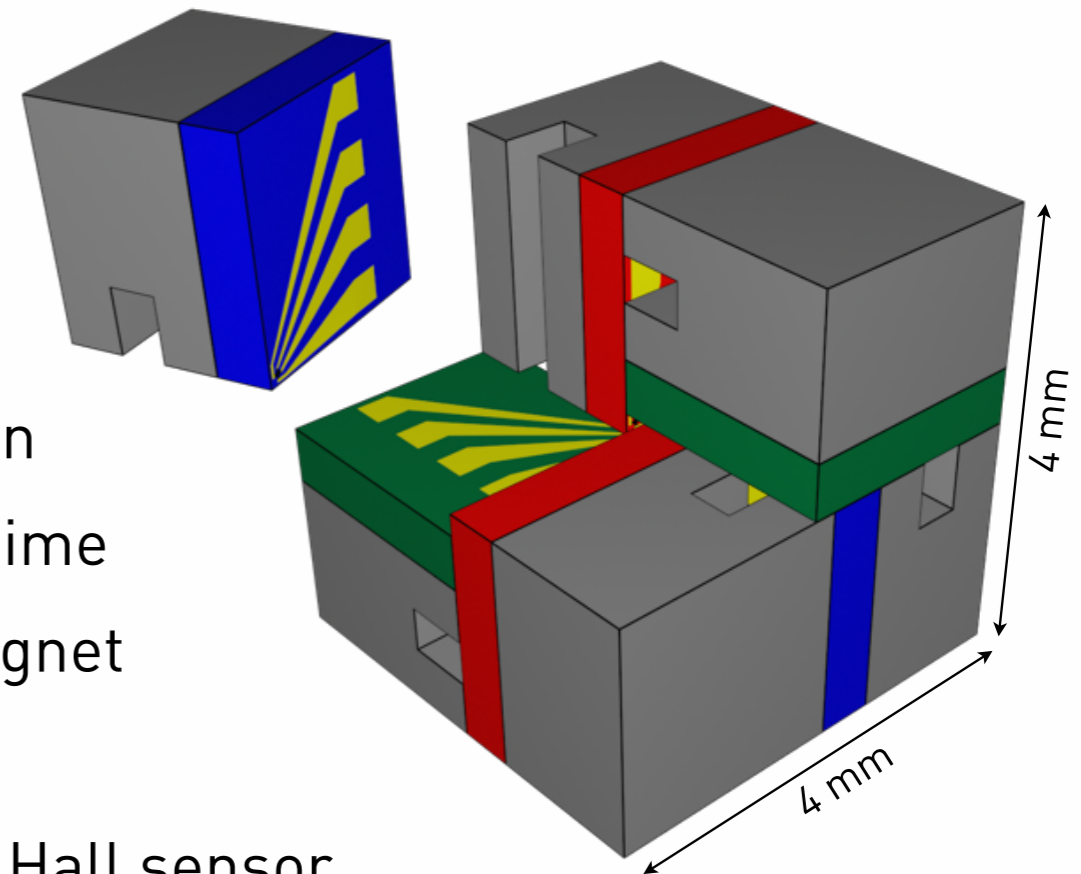
- Active volume $(200\ \mu\text{m})^3$
- One sensor pair (red, green, blue) per field direction
 - Measure \mathbf{B} virtually in single point in space and time
 - Cancel out loop-induced voltages (on-the-fly magnet measurement)
 - Cancel out planar Hall voltage (\mathbf{B}_p in plane to 1D Hall sensor → cross-sensitivity)
- Target accuracy: <100 ppm at the 1 T level for *any* magnetic field direction



- Semi-insulating GaAs
- n-type GaAs
- Au/Ge/Ni Contacts
- MACOR

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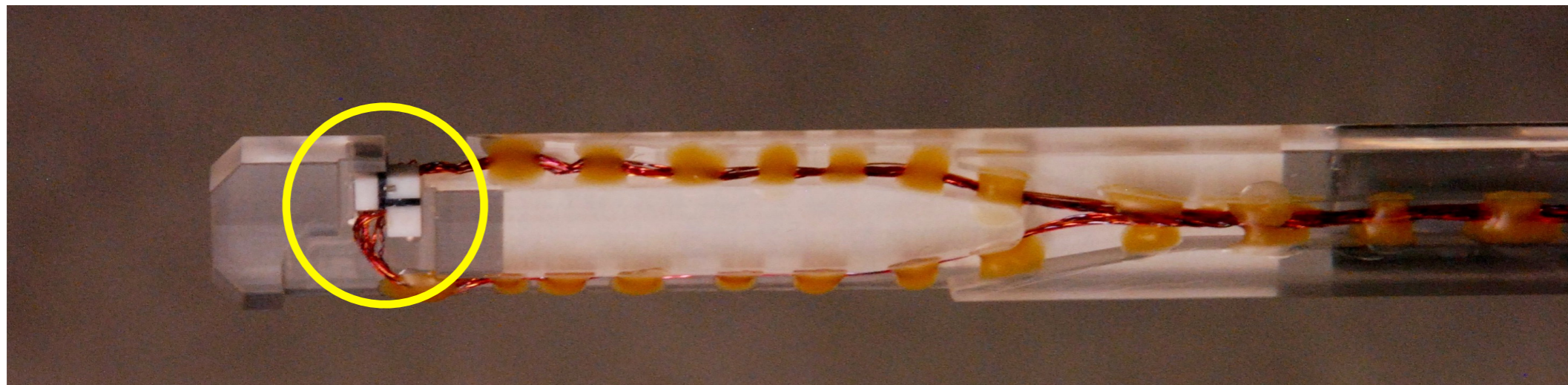
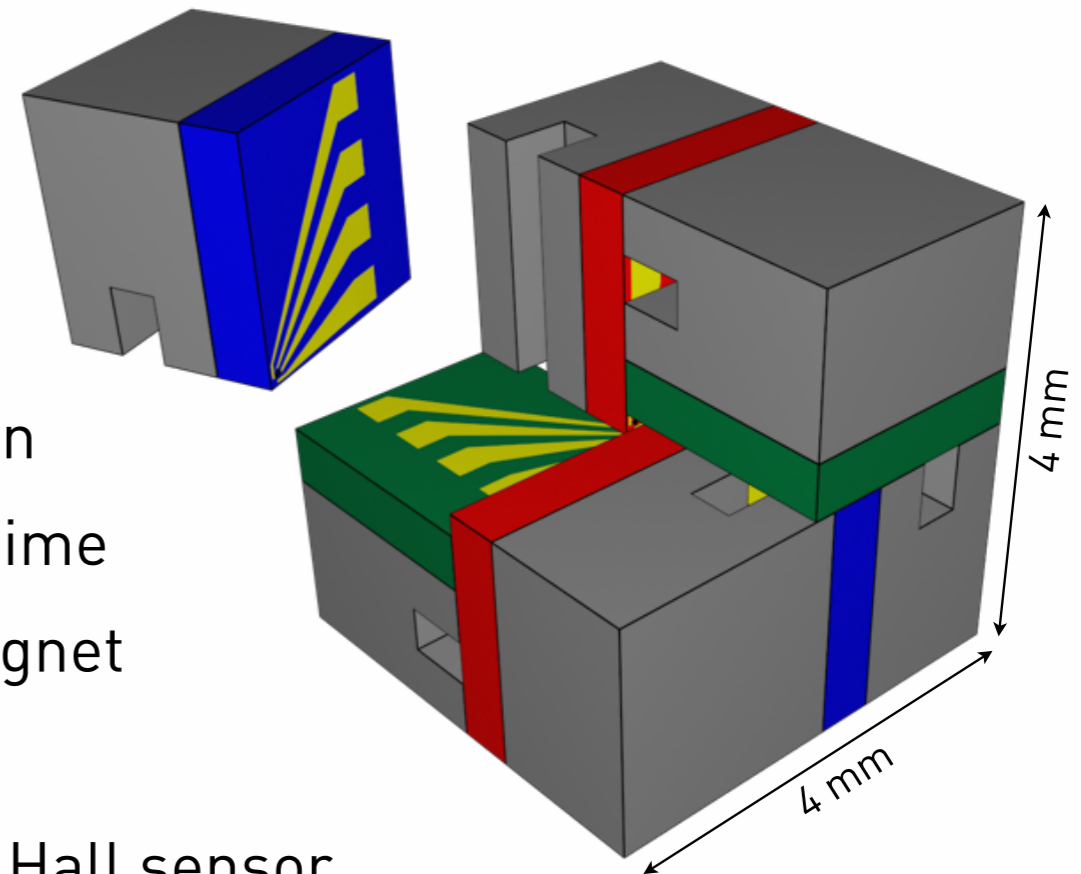


Hall sensor parameters:

- $S = \sim 100\ \text{mV/T}$ ($I = 1\ \text{mA}$)
- Offset < 10 Gauss
- Non-linearity (0 - 2 T) max 10 Gauss
- Temp. coeff. $\sim 200\ \text{ppm}/^\circ\text{C}$
- V_{pp} (short term) $< 2\ \mu\text{V}$ (or 20 ppm)

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Design implications

- Three sensor pairs, Hall voltages assigned practically to a single point. Interpolation error quadratic field distribution:

For $d = 200 \mu\text{m}$ and for a tolerable error of $<100 \text{ ppm}$: fields $B_x(x)$, $B_y(y)$, $B_z(z)$ up to 10.000 Tm^{-2}

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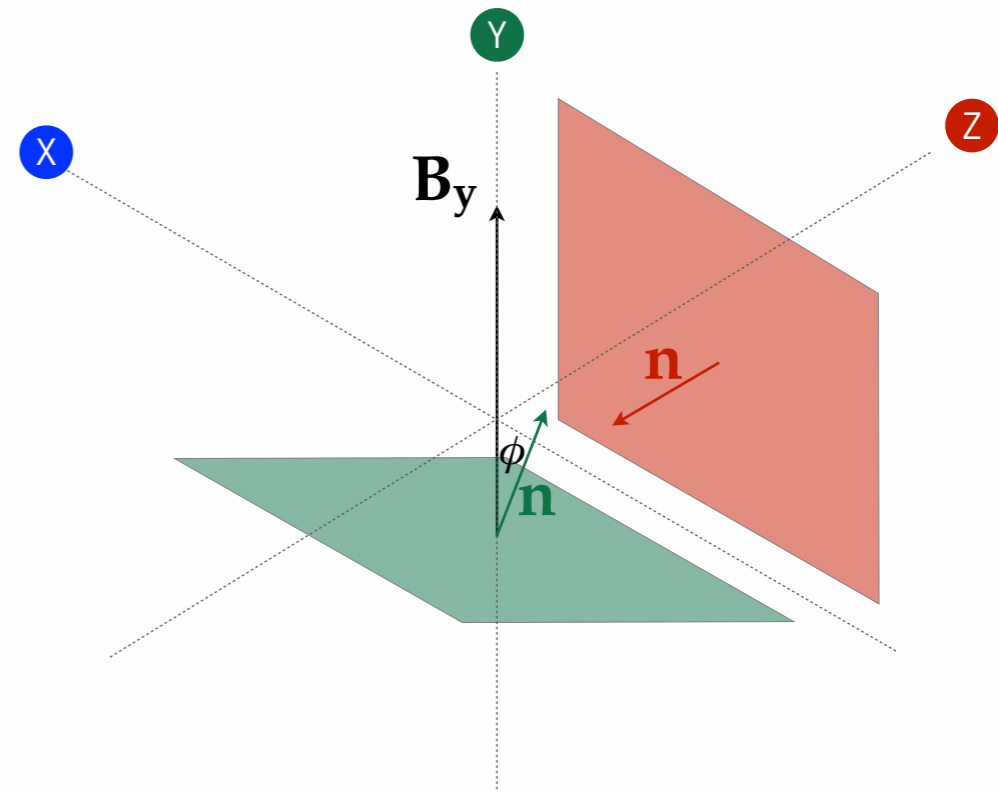
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- Orthogonality errors

$$\mathbf{B} \cdot \mathbf{n} = |\mathbf{B}_y| \cos \phi \approx B_y \text{ for small } \phi$$

$$\mathbf{B} \cdot \mathbf{n} = 0$$



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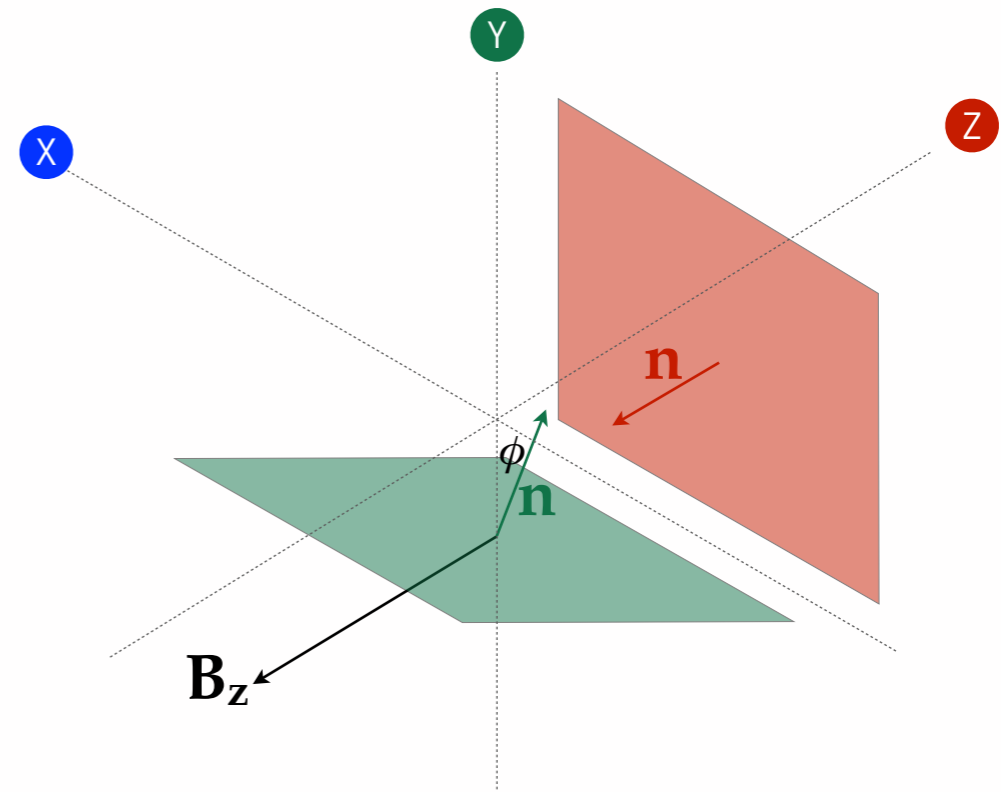
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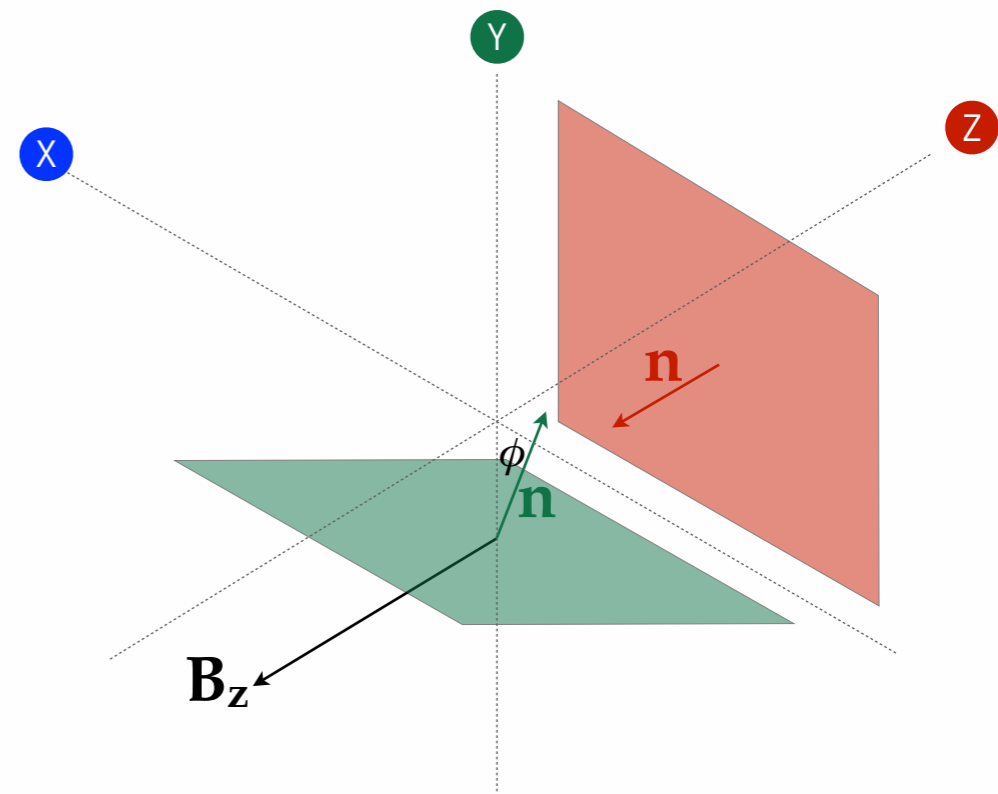
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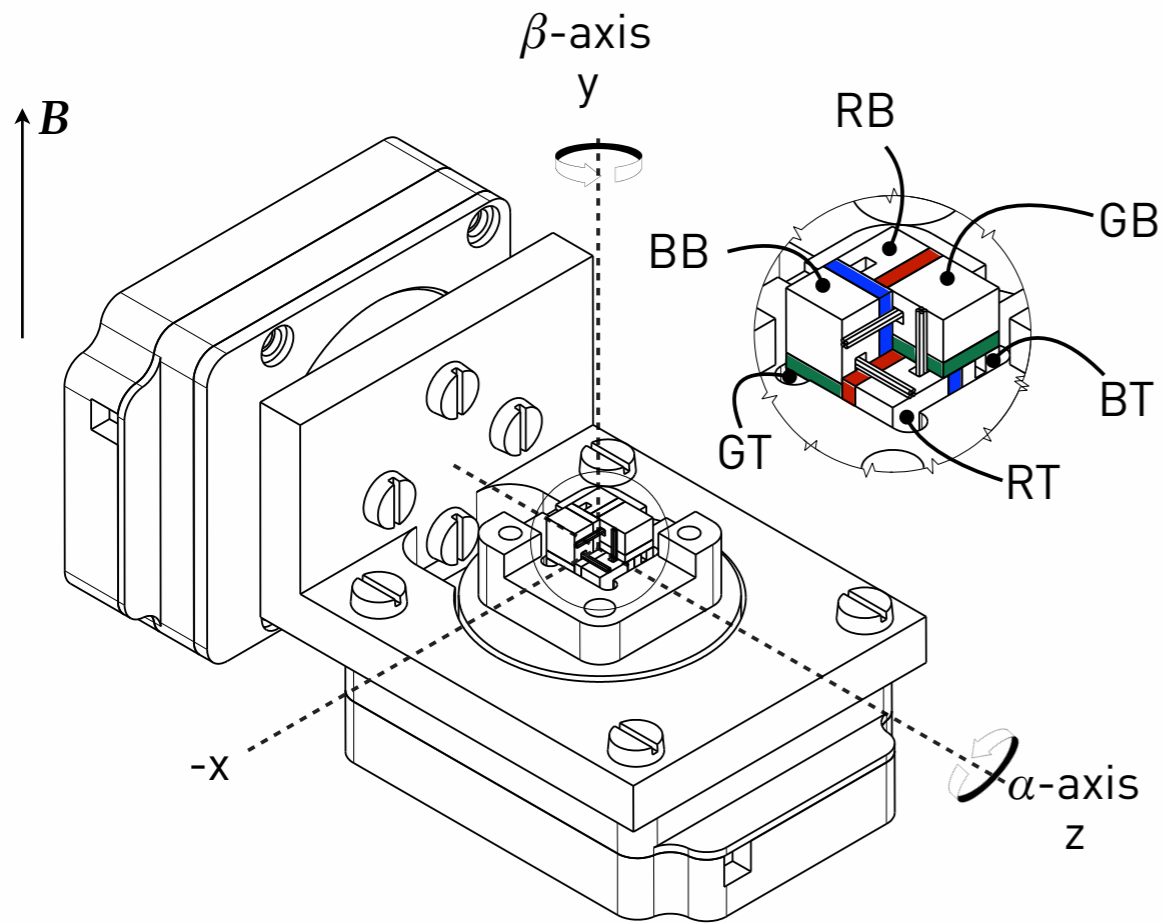
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$<100 \text{ ppm}$ cross sensitivity $\rightarrow <0.1 \text{ mrad}$ or 0.006° orthogonality error

Orthogonality errors



Harmonic Analysis

$B \approx 1 \text{ T}$

360° rotation around one axis (α or β)

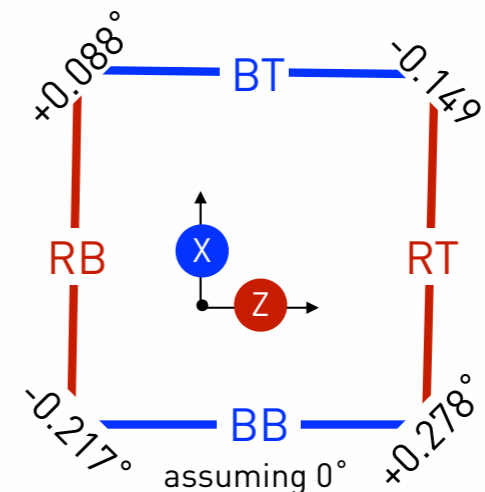
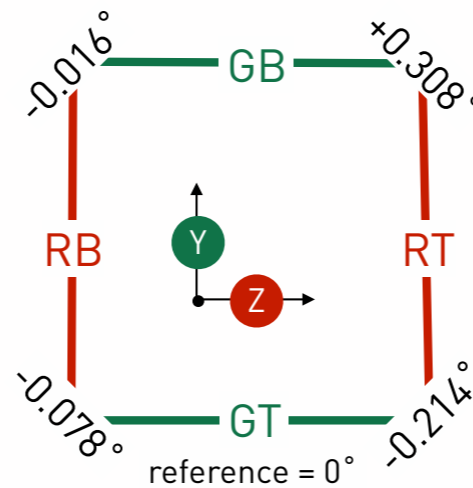
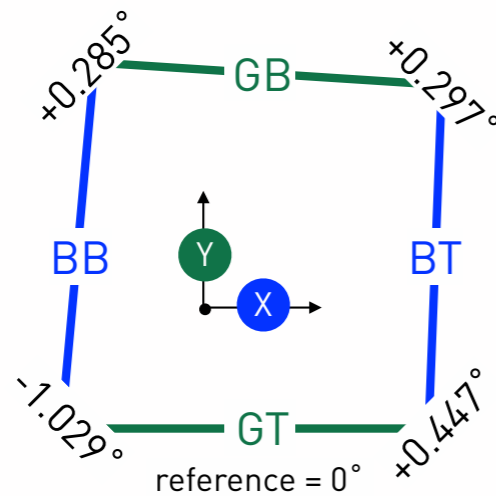
E.g. around α at given β :

$$A_0 + A_1 \cos(1\alpha - p_1) + A_2 \cos(2\alpha - p_2)$$

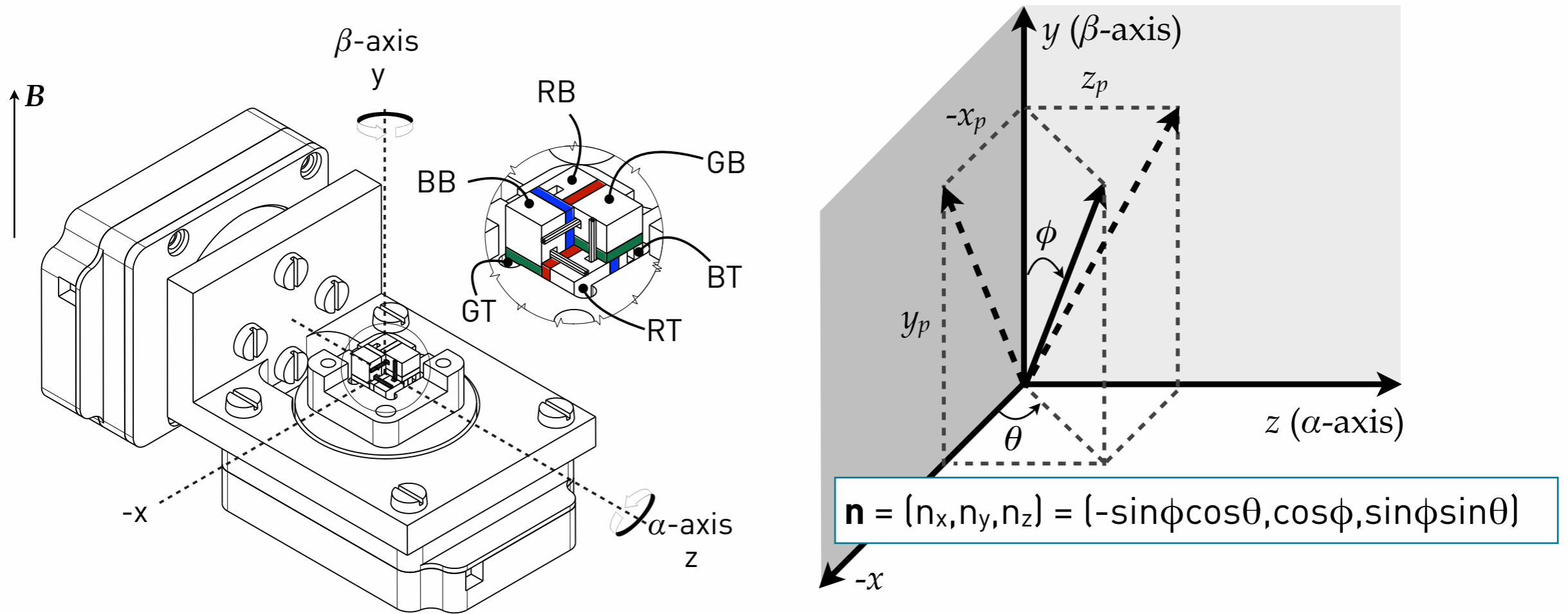
0th harm: offset, $B \cdot z \neq 0$

1st harm: Hall effect

2nd harm: planar Hall effect



Field reconstruction

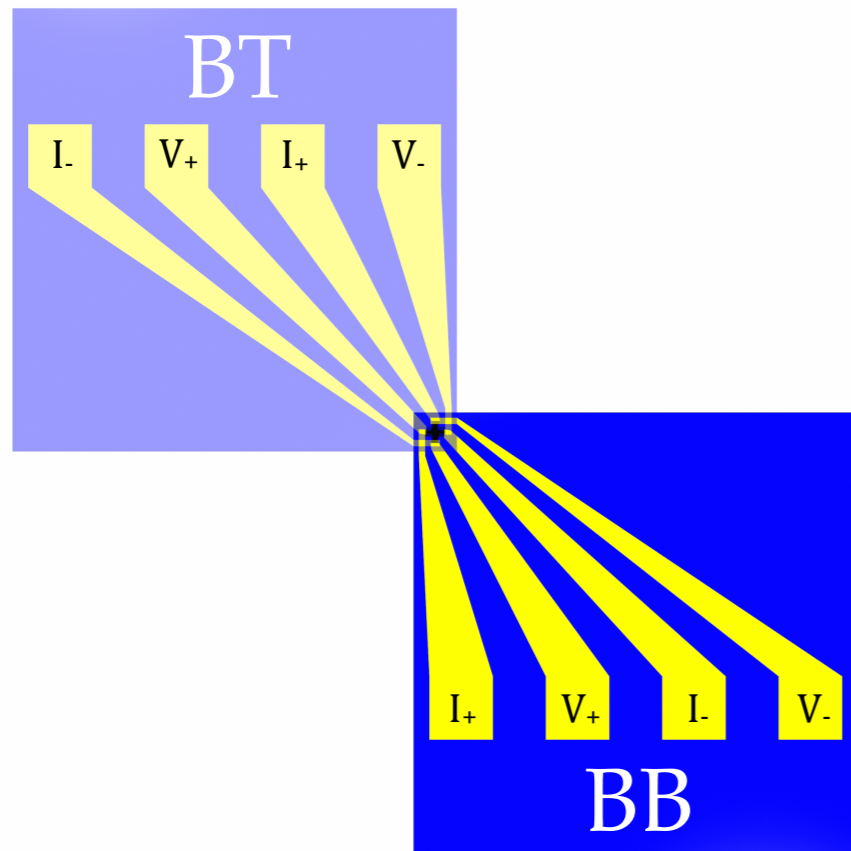


$$\begin{aligned}
 \mathbf{B} \cdot (\mathbf{n}_{GB} + \mathbf{n}_{GT}) &= B_n^{GB} (V_{GB}) + B_n^{GT} (V_{GT}) \\
 \mathbf{B} \cdot (\mathbf{n}_{BB} + \mathbf{n}_{BT}) &= B_n^{BB} (V_{BB}) + B_n^{BT} (V_{BT}) \\
 \mathbf{B} \cdot (\mathbf{n}_{RB} + \mathbf{n}_{RT}) &= B_n^{RB} (V_{RB}) + B_n^{RT} (V_{RT})
 \end{aligned}$$

$$\begin{pmatrix}
 n_{x,GB} + n_{x,GT} & n_{y,GB} + n_{y,GT} & n_{z,GB} + n_{z,GT} \\
 n_{x,BB} + n_{x,BT} & n_{y,BB} + n_{y,BT} & n_{z,BB} + n_{z,BT} \\
 n_{x,RB} + n_{x,RT} & n_{y,RB} + n_{y,RT} & n_{z,RB} + n_{z,RT}
 \end{pmatrix}
 \begin{pmatrix}
 B_x \\
 B_y \\
 B_z
 \end{pmatrix}
 =
 \begin{pmatrix}
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 \end{pmatrix}$$

Design implications

- Planar Hall effect and loop-induced voltage compensation



$$V_{PH} = \frac{R_{PH}}{2t} I B_p^2 \sin 2\theta$$

if $R_{PH1} = R_{PH2}, B_{p1} = B_{p2}, |\theta_2 - \theta_1| = 90^\circ$:

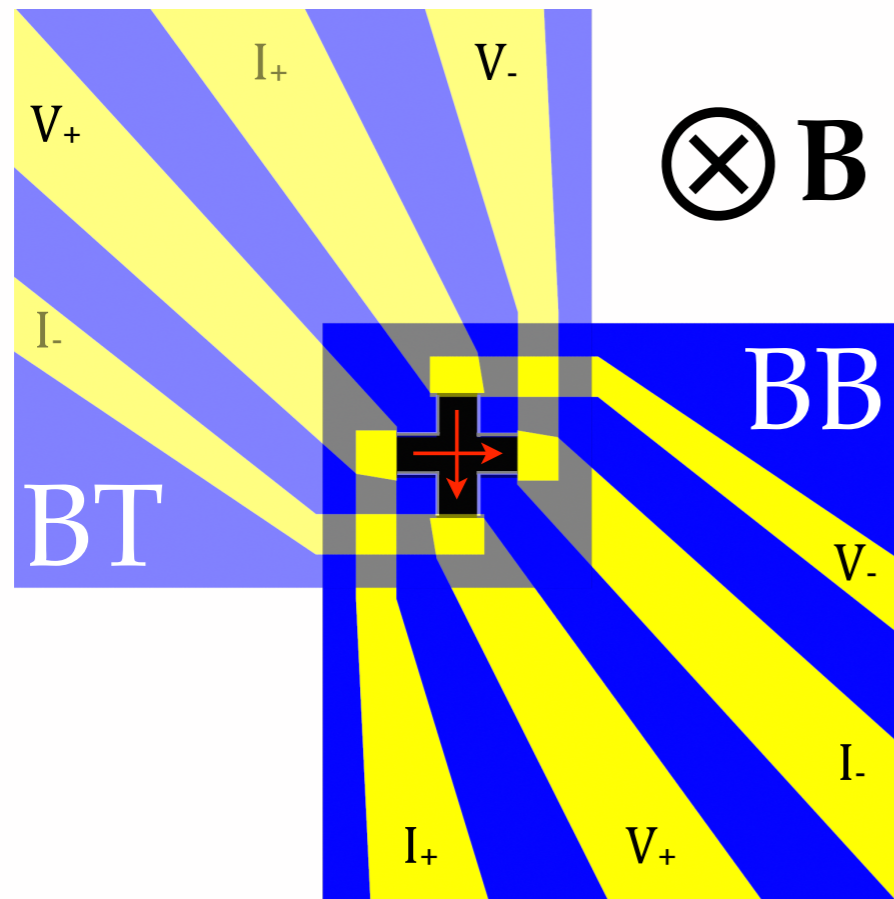
$$\frac{1}{2}(V_{PH1} + V_{PH2}) = 0$$

I direction (orthogonal): PHE compensation

I direction (+ or -): induced voltage compensation

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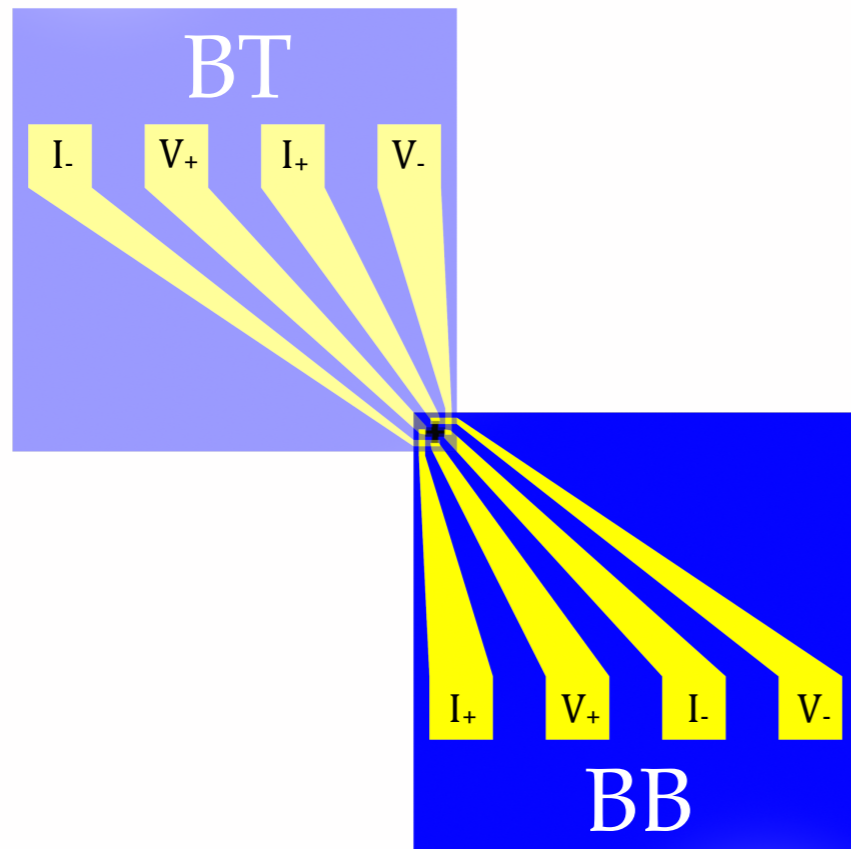
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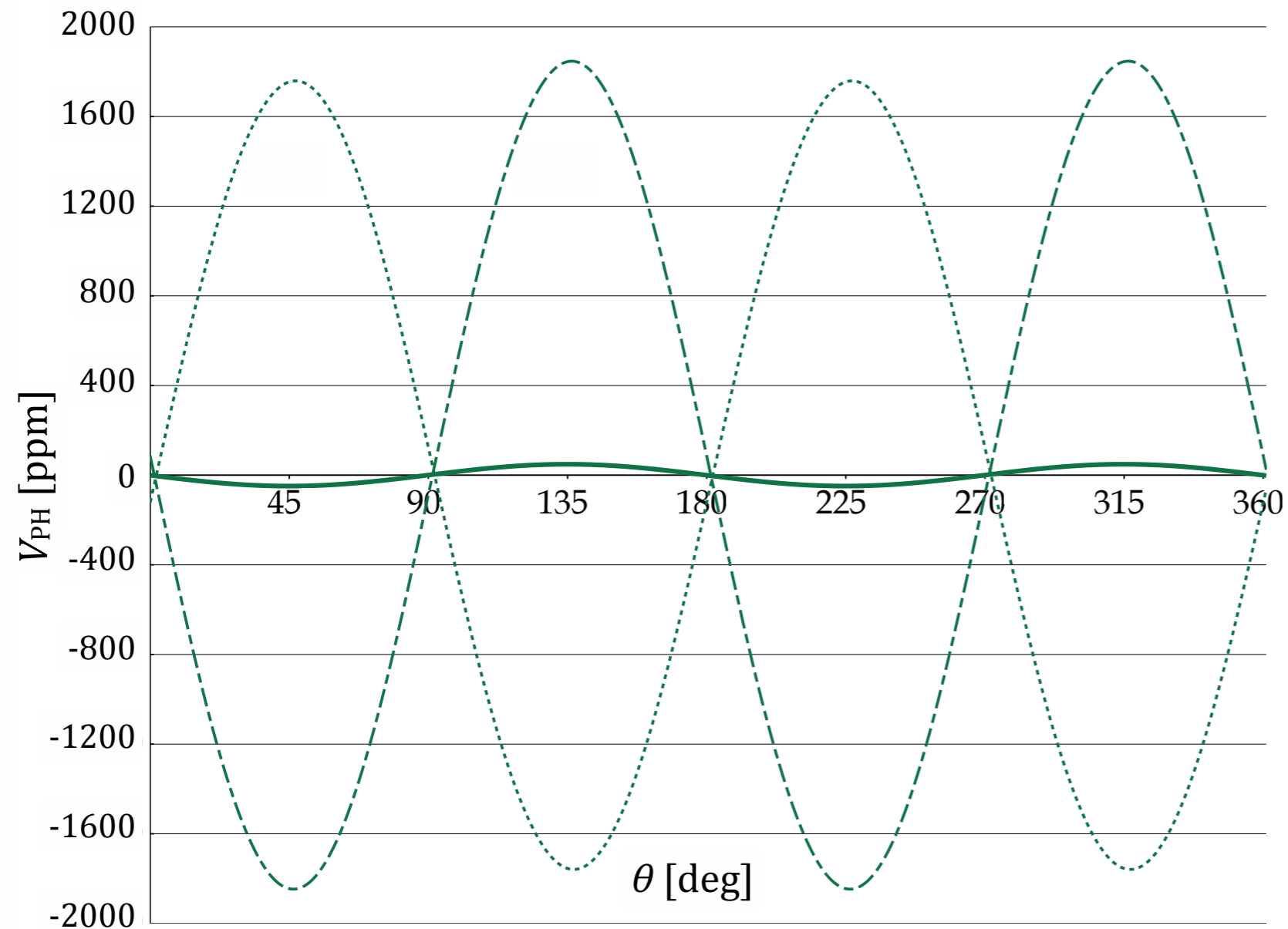
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if $|\theta_2 - \theta_1| \neq 90^\circ$: per degree angular error, 1.7% of the PH voltage is not cancelled out

if $R_{PH1} \neq R_{PH2}$: for 1% difference, 0.5% of the PH voltage is not cancelled out

if $B_{p1} \neq B_{p2}$: for 1% difference, also 1% of the PH voltage is not cancelled out

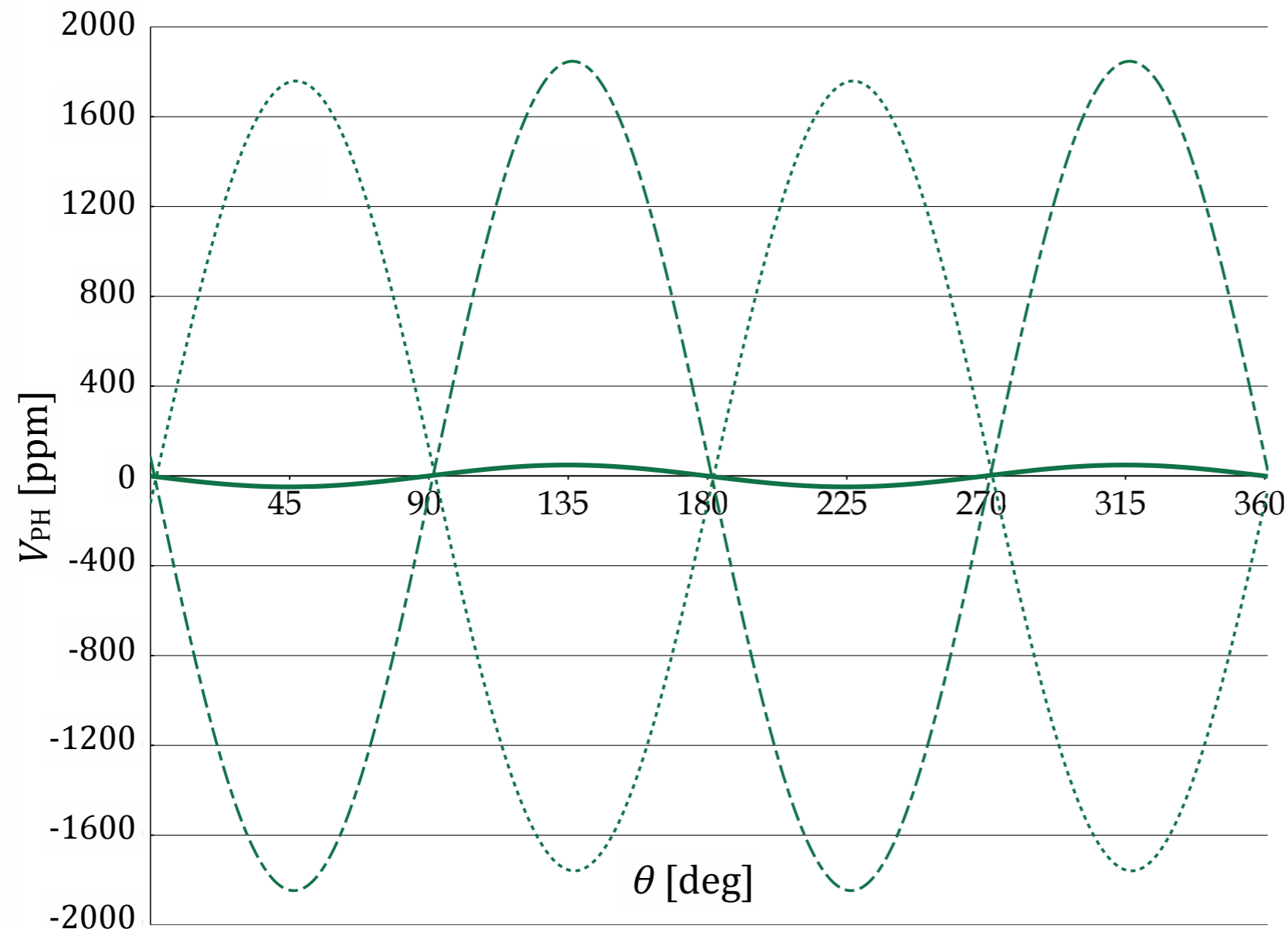
Planar Hall effect voltage compensation



$$V_{PH} = \frac{R_{PH}}{2t} I B_p^2 \sin 2\theta$$

$$B_p = 1 \text{ T}$$

Planar Hall effect voltage compensation



$$V_{PH} = \frac{R_{PH}}{2t} IB_p^2 \sin 2\theta$$

$$B_p = 1\text{T}$$

- Planar Hall effect 500-600 times weaker than Hall effect
- Reduced >35 times by compensation using pairs
- Remnant maximum V_{PH} at 1 T is <5 μV (or 50 ppm) for worst pair \rightarrow 0.5 Gauss max err.

Total field reconstruction

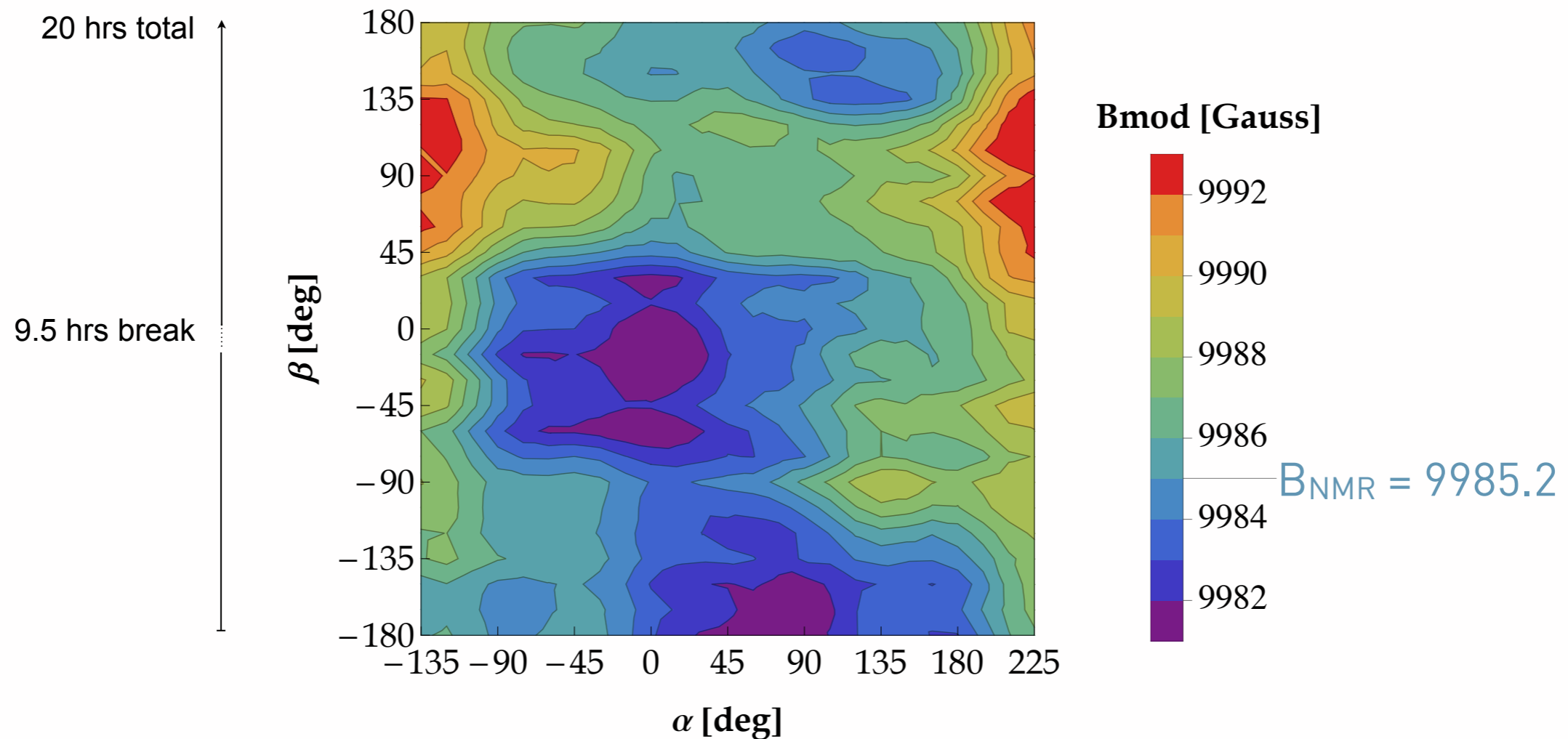
- Goal: target accuracy: <100 ppm at the 1 T level for *any* magnetic field direction

Homogeneous magnetic field volume

- Known field (NMR probe)
- Total measured field, $B_{\text{mod}} = \sqrt{B_x^2 + B_y^2 + B_z^2}$, should be constant
- Even if not $\alpha \perp \beta$ and not $\mathbf{B} \perp \alpha$
- Calibration magnet at 1 T: At every β position perform 360° rotation around α

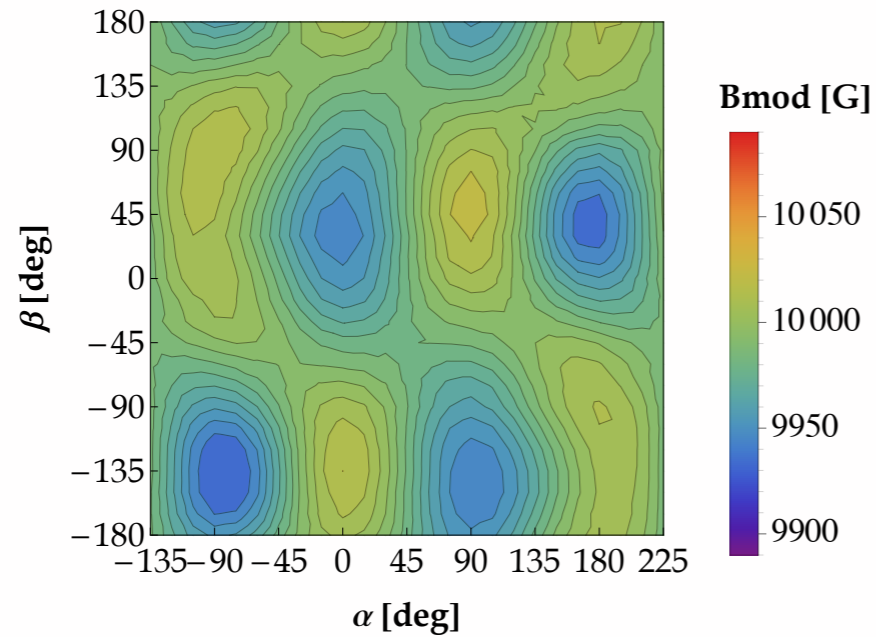
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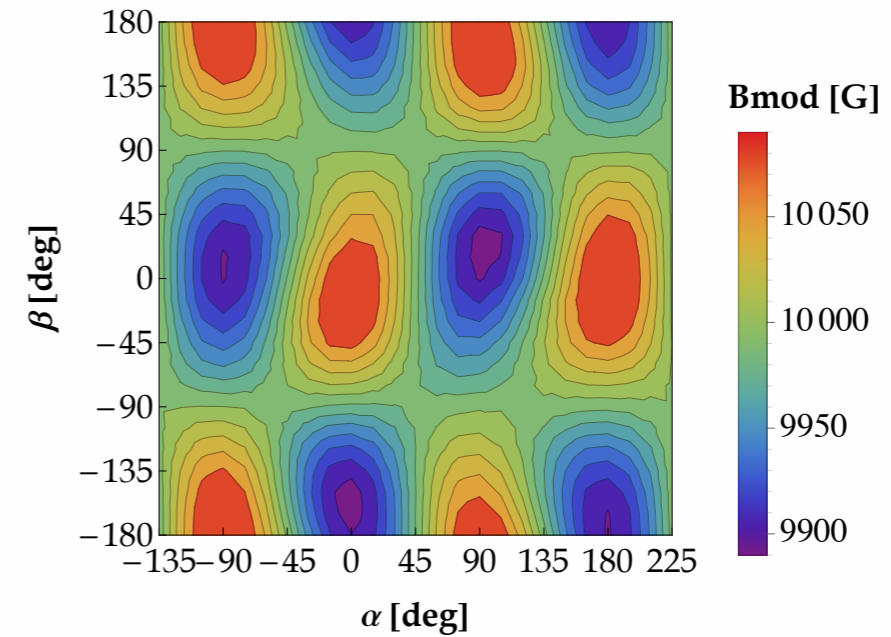


Total field reconstruction for full α and β rotation in a homogeneous field of 1 T, $pp = 12$ Gauss

Total field reconstruction

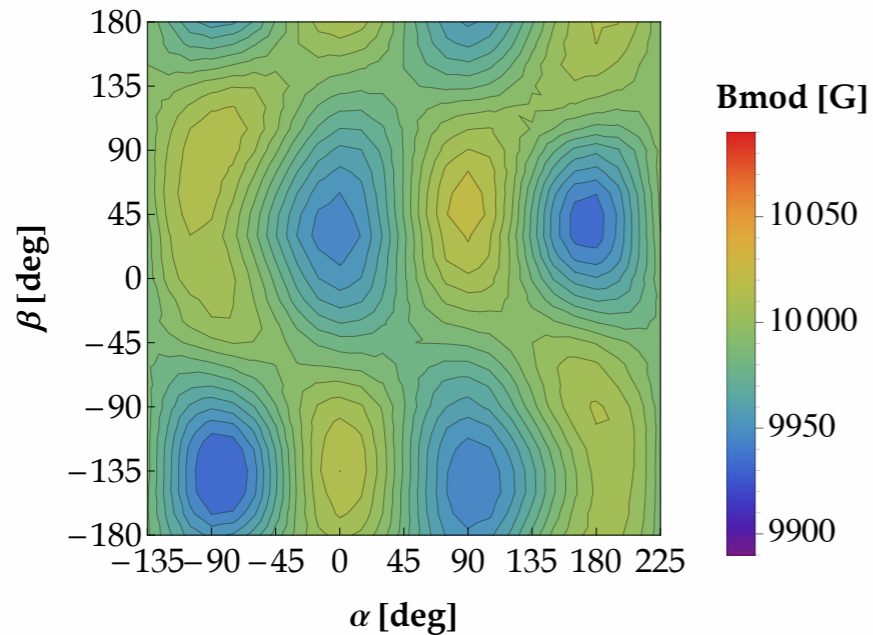


Total field reconstruction from BT, GB, and RT Hall sensors without angular error correction, $pp = 88$ G

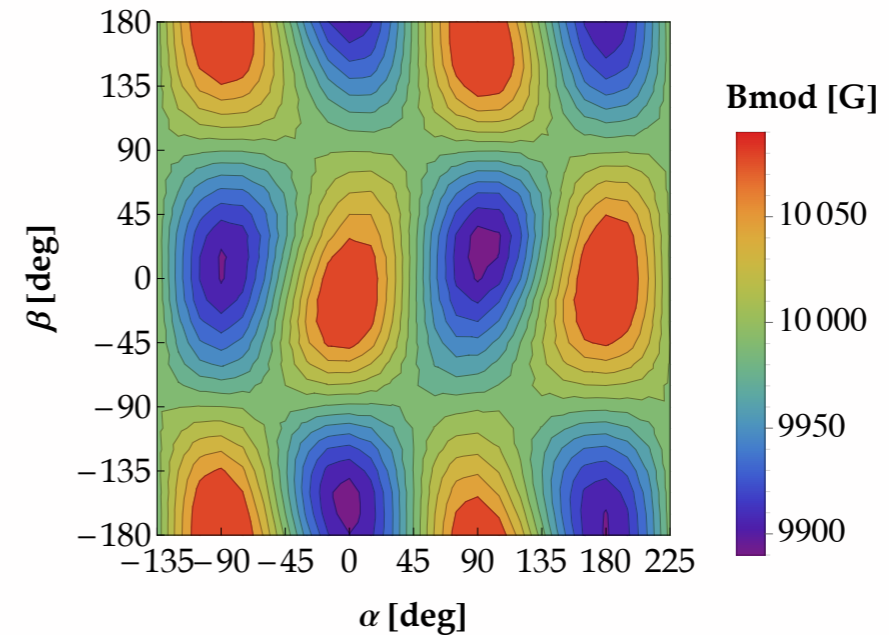


Total field reconstruction from BB, GT, and RB Hall sensors without angular error correction, $pp = 189$ G

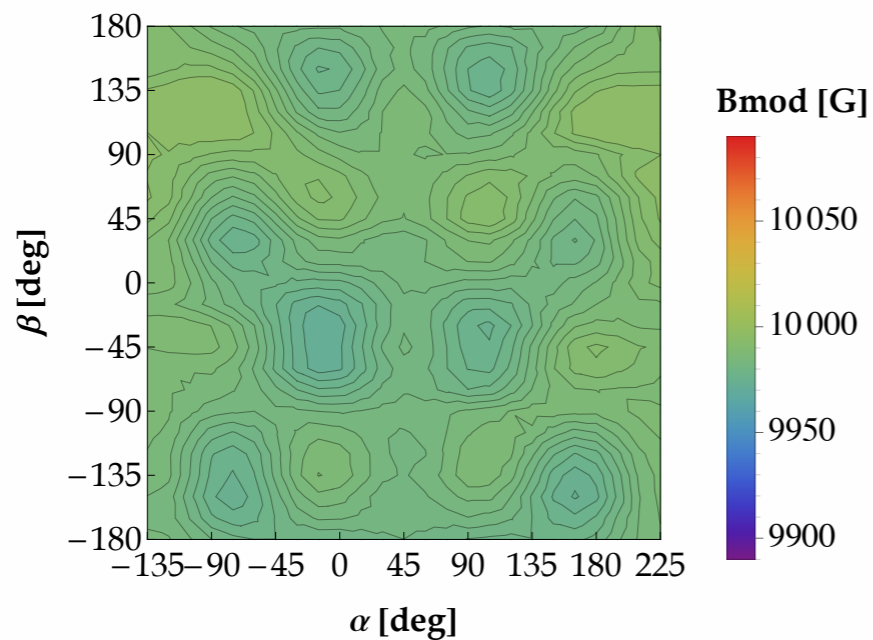
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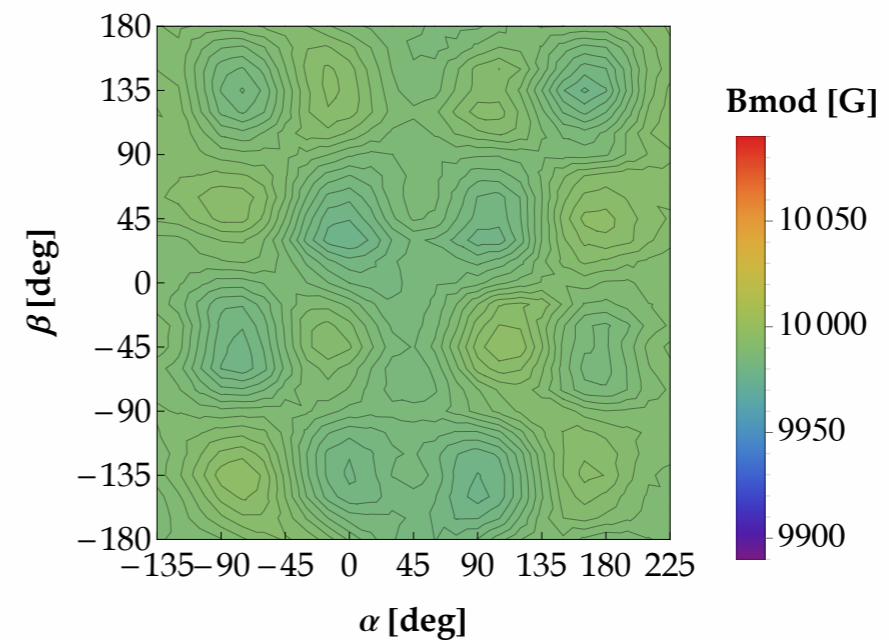
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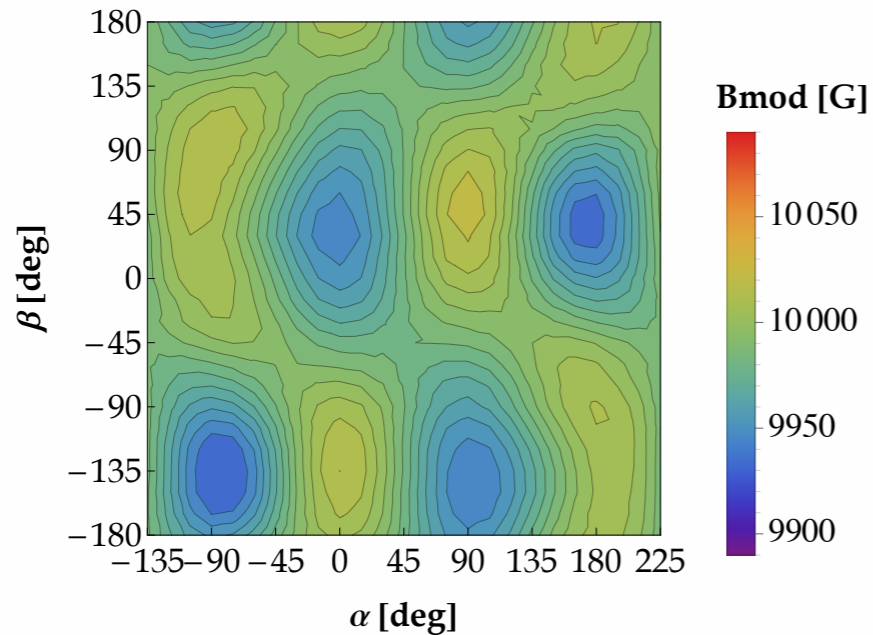


Total field reconstruction from BT, GB, and RT Hall sensors with angular error correction, $pp = 23$ G

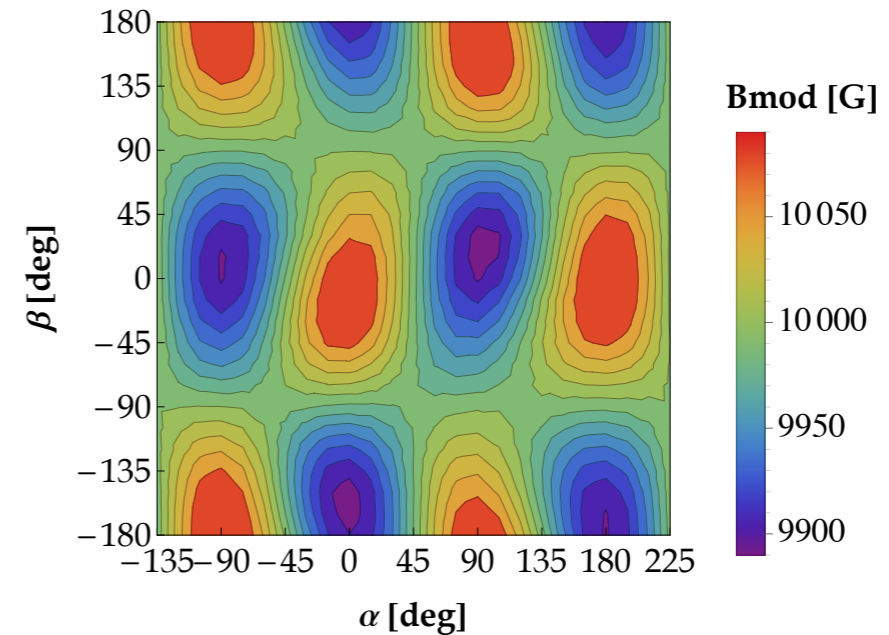


Total field reconstruction from BB, GT, and RB Hall sensors with angular error correction, $pp = 21$ G

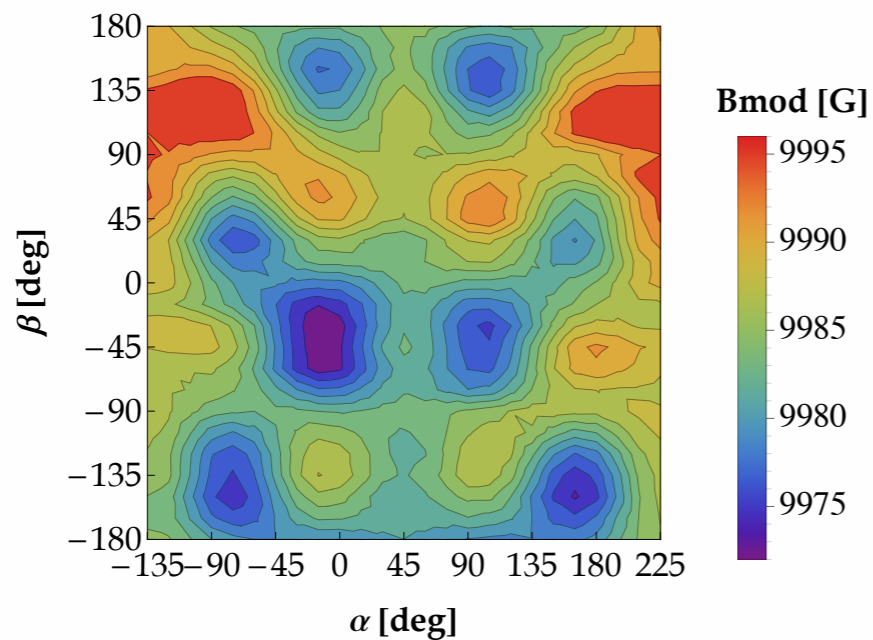
Total field reconstruction



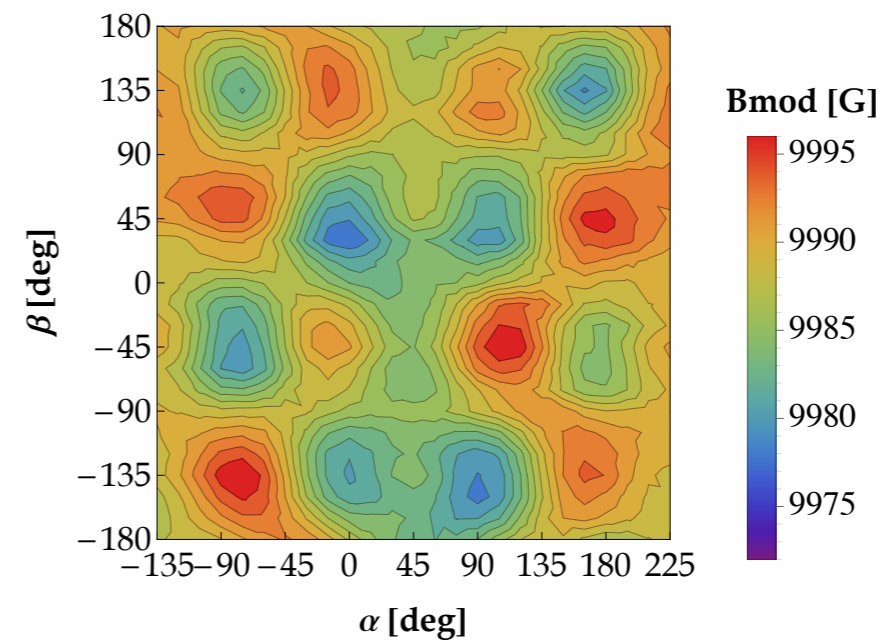
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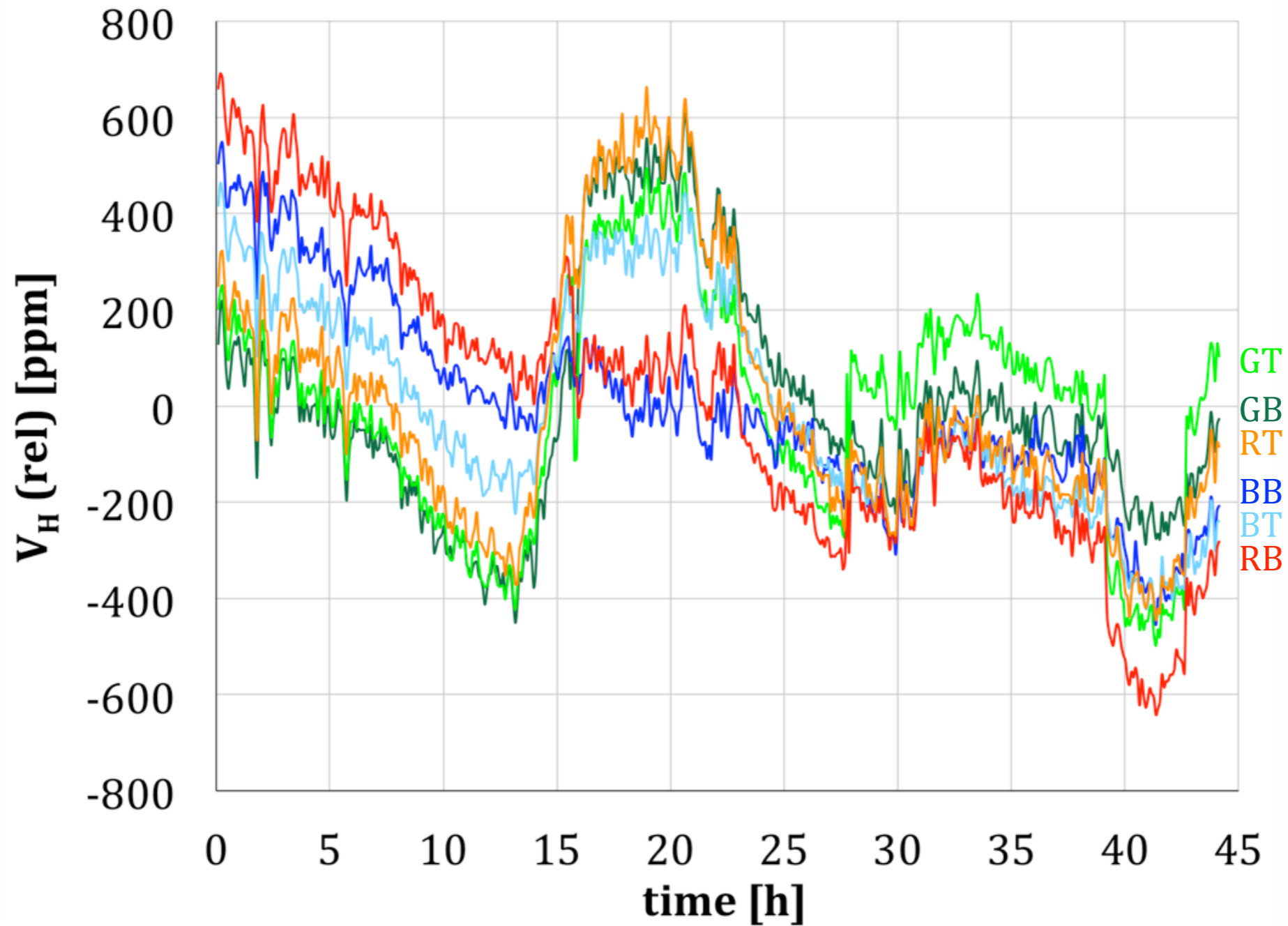


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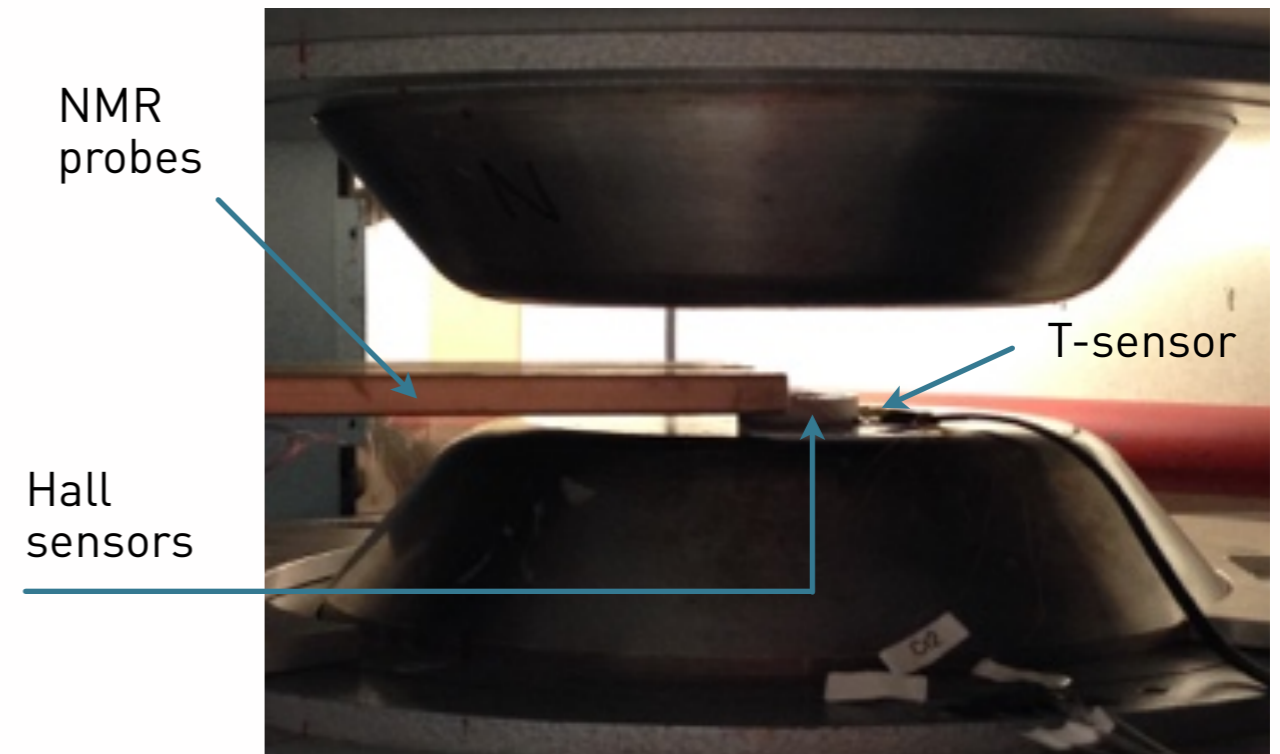
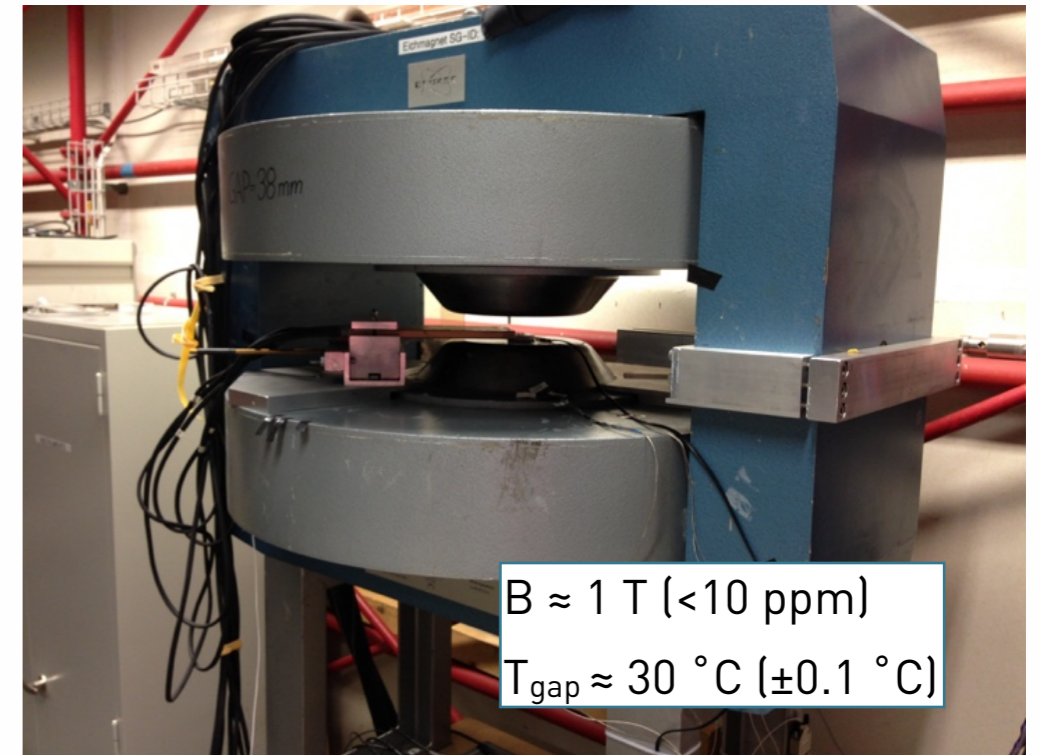
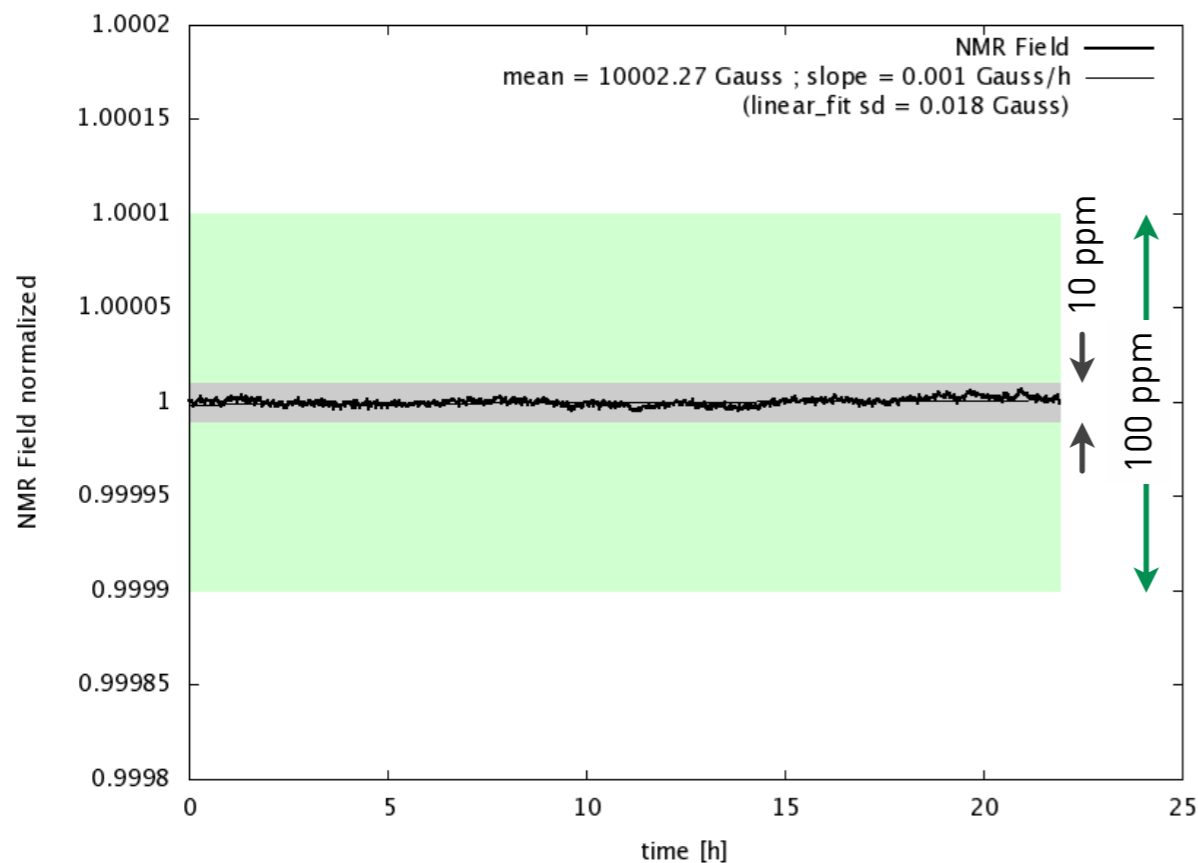
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Long-term stability



Measurement setup

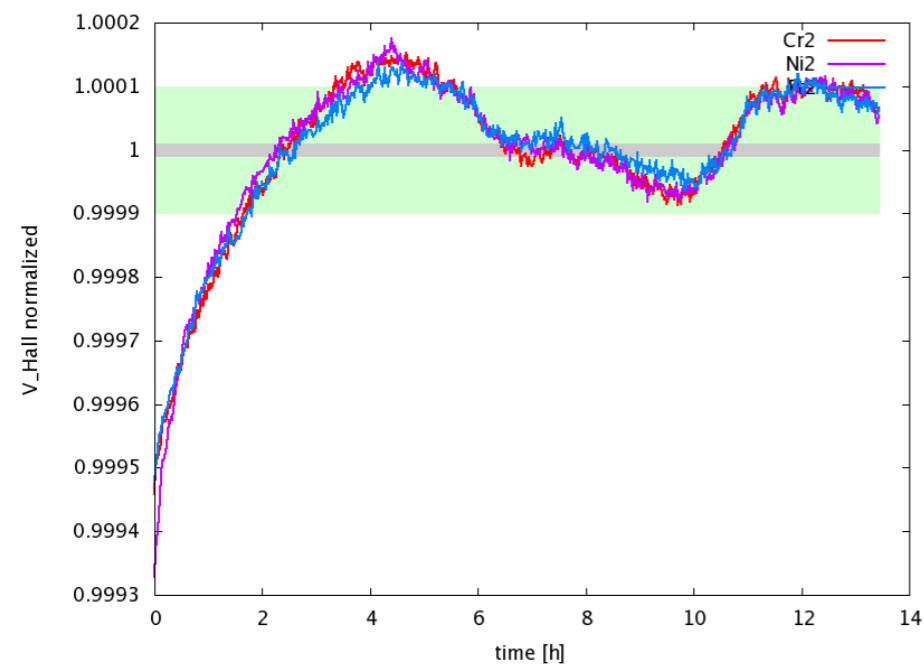
- Long-term measurements: every 60 s one data point (avg of 100 samples)
- V_H : HP/Agilent/Keysight 3458A
- I_H : 1.0 mA DC, series, Keithley 6221
- NMR probes: Metrolab, PT2025
- Devices controlled over EPICS via Python script



First results

Learned:

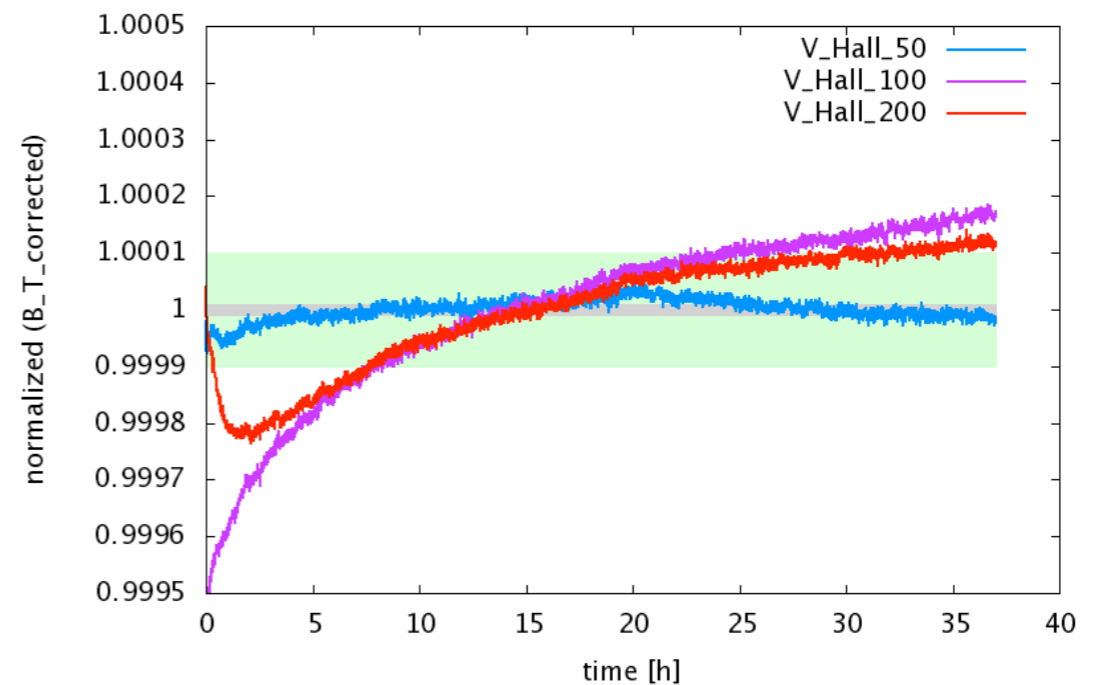
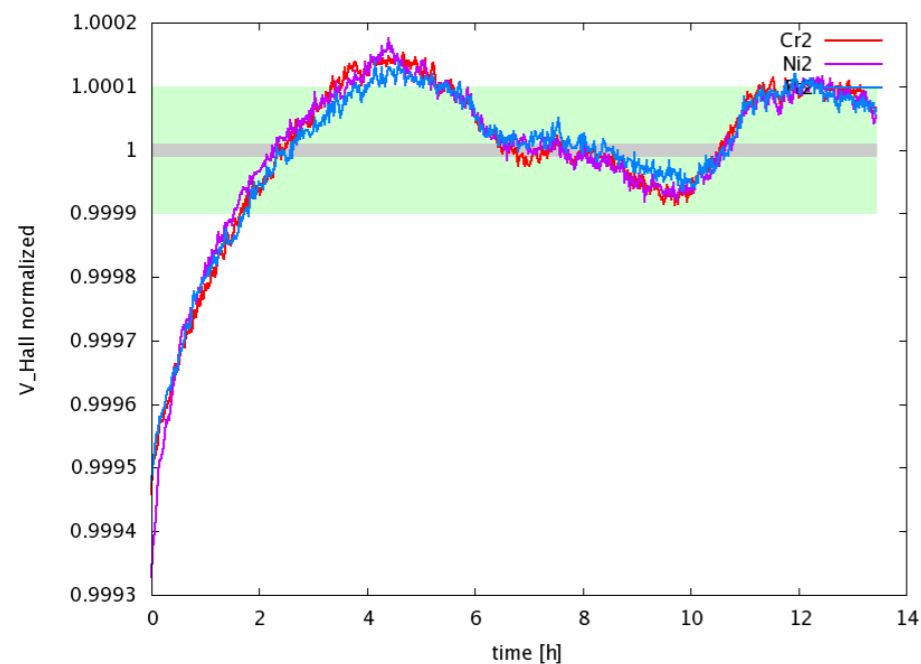
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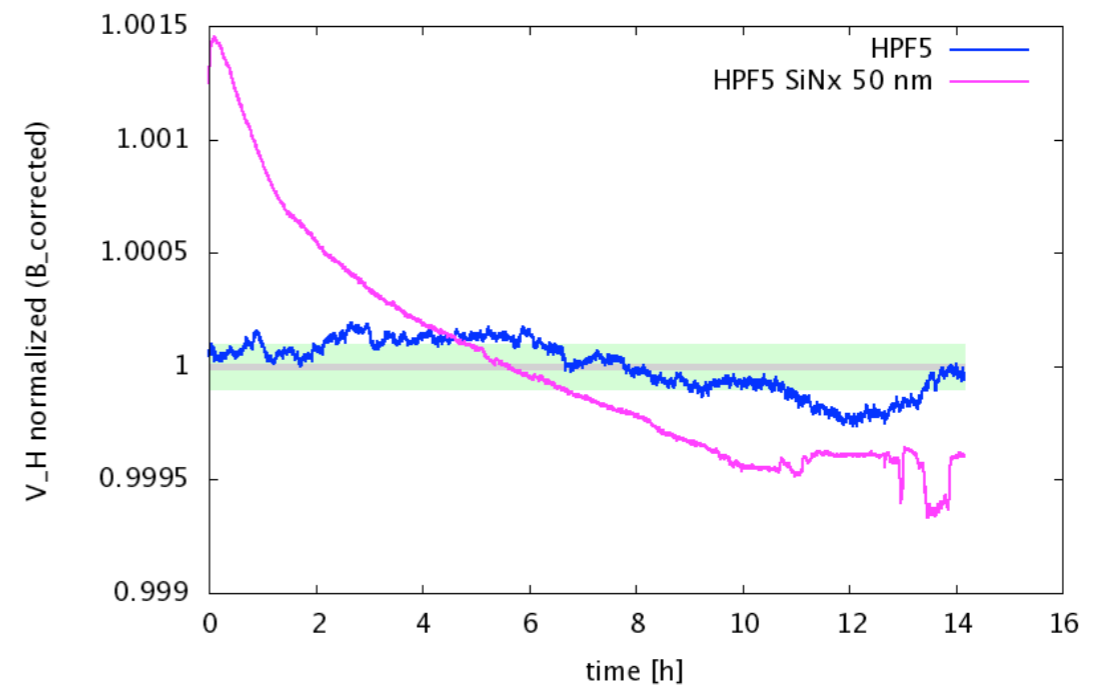
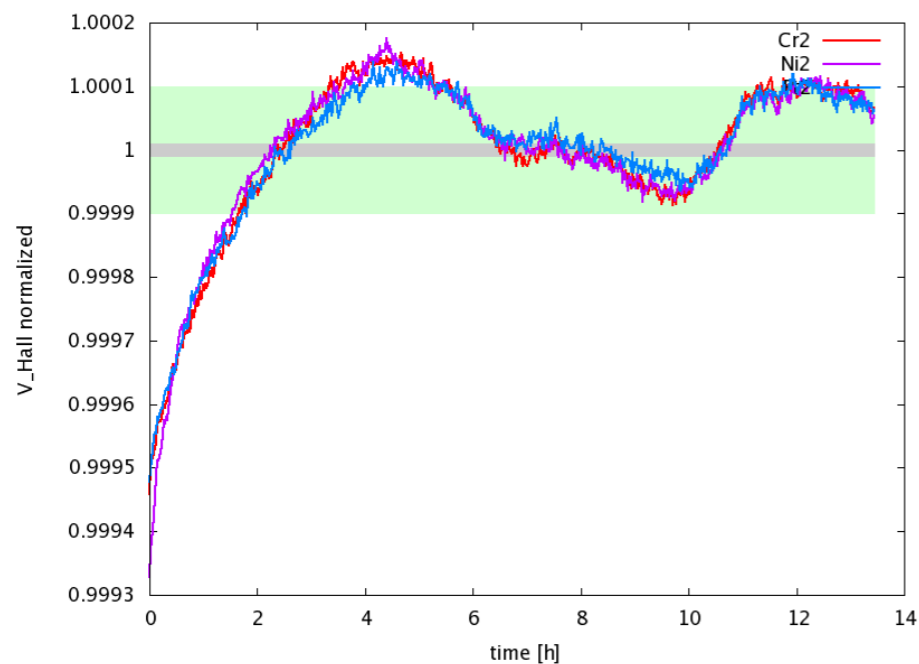
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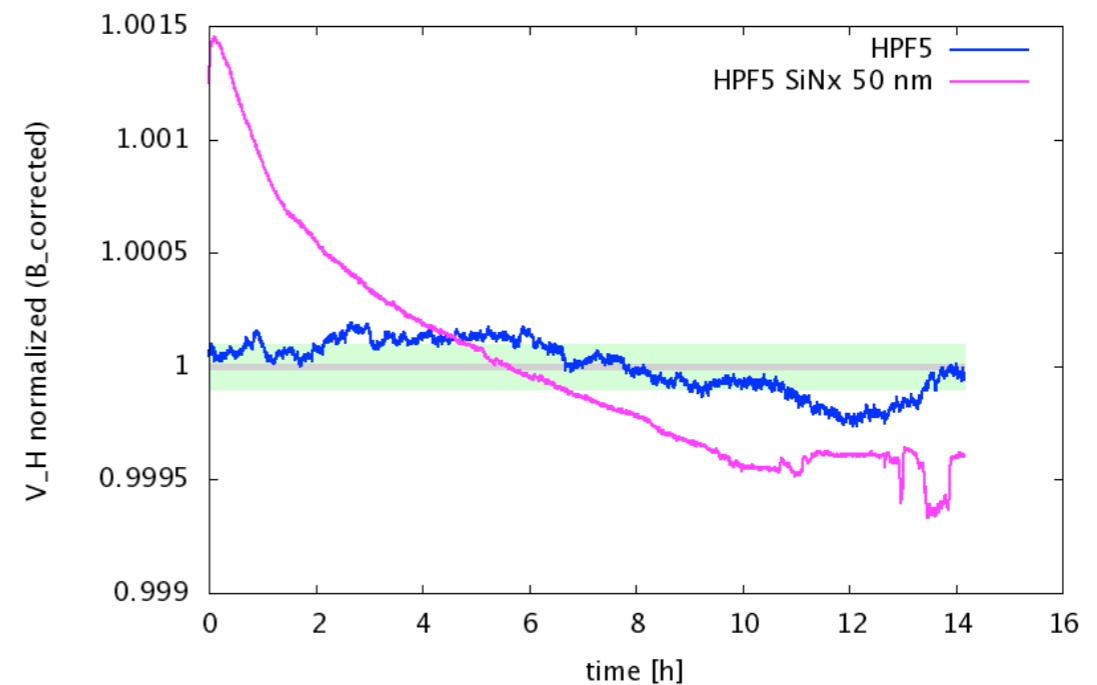
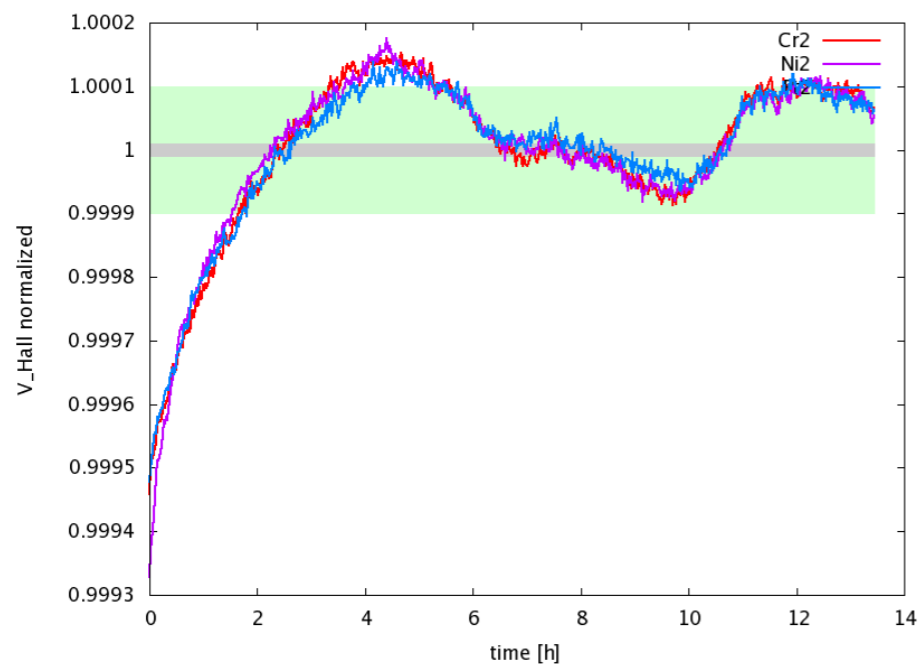
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Material, fabrication process, measurement-setup



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To do:

- Confirm necessity for SiN_x, optically inspect SiN_x quality, check repeatability

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 - <100 nm SiN_x surface passivation
- Mixed results, due to quality of SiN_x?

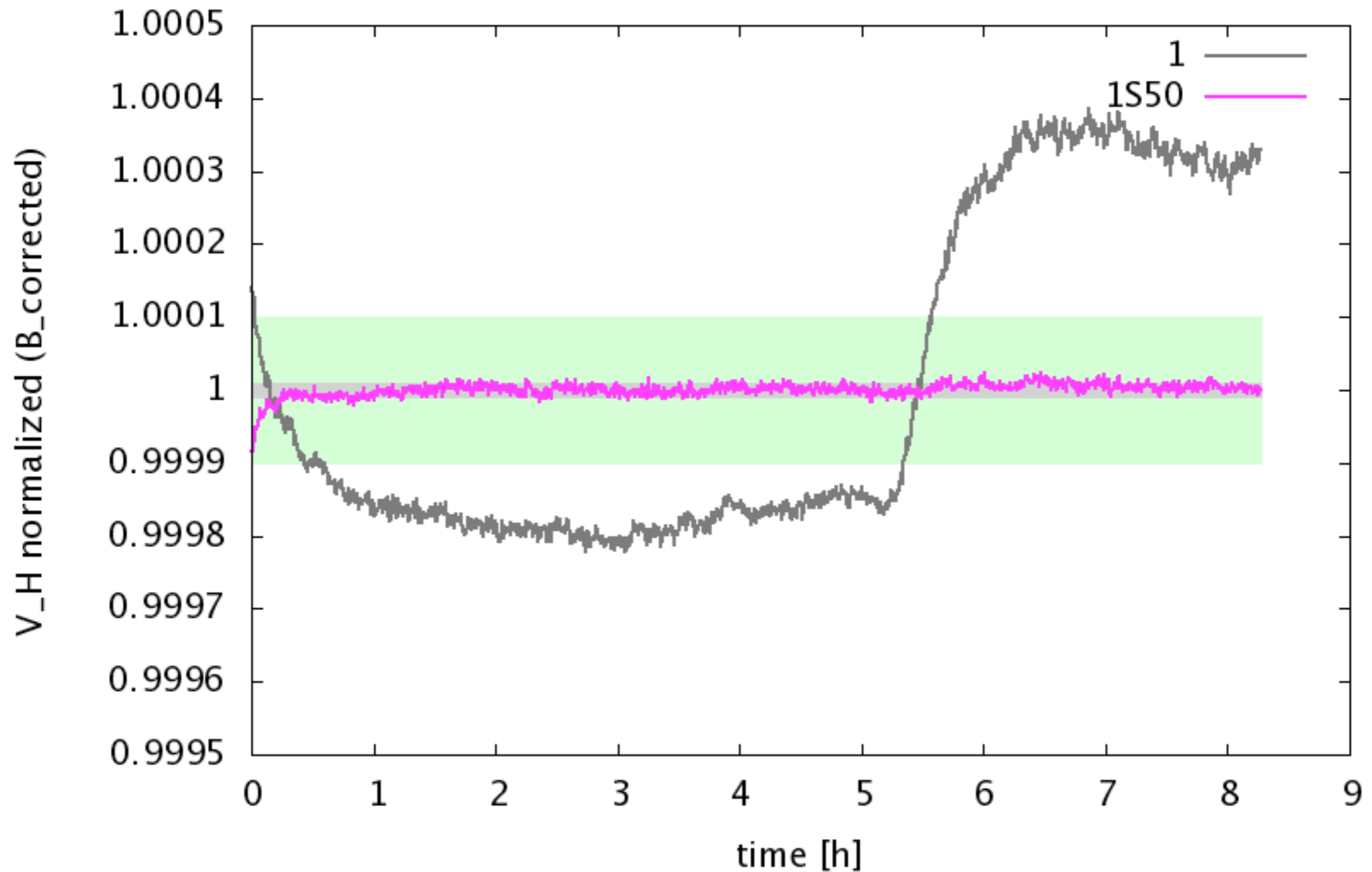
Cause?

Material, fabrication process, ~~measurement setup~~

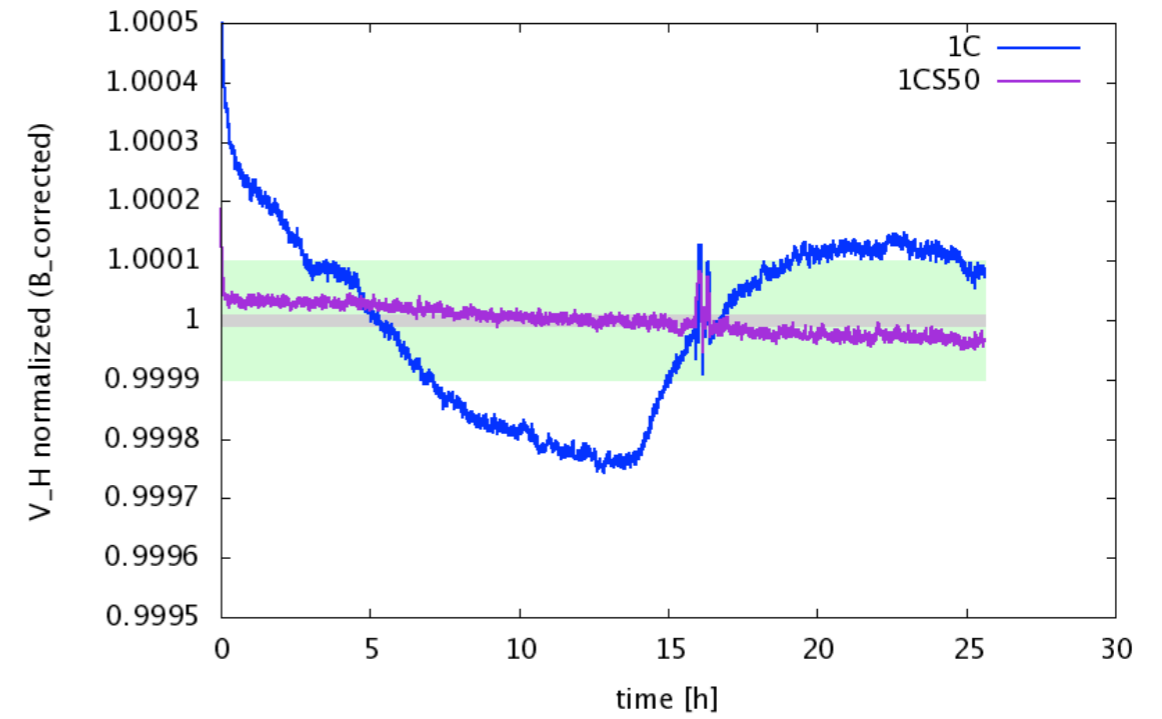
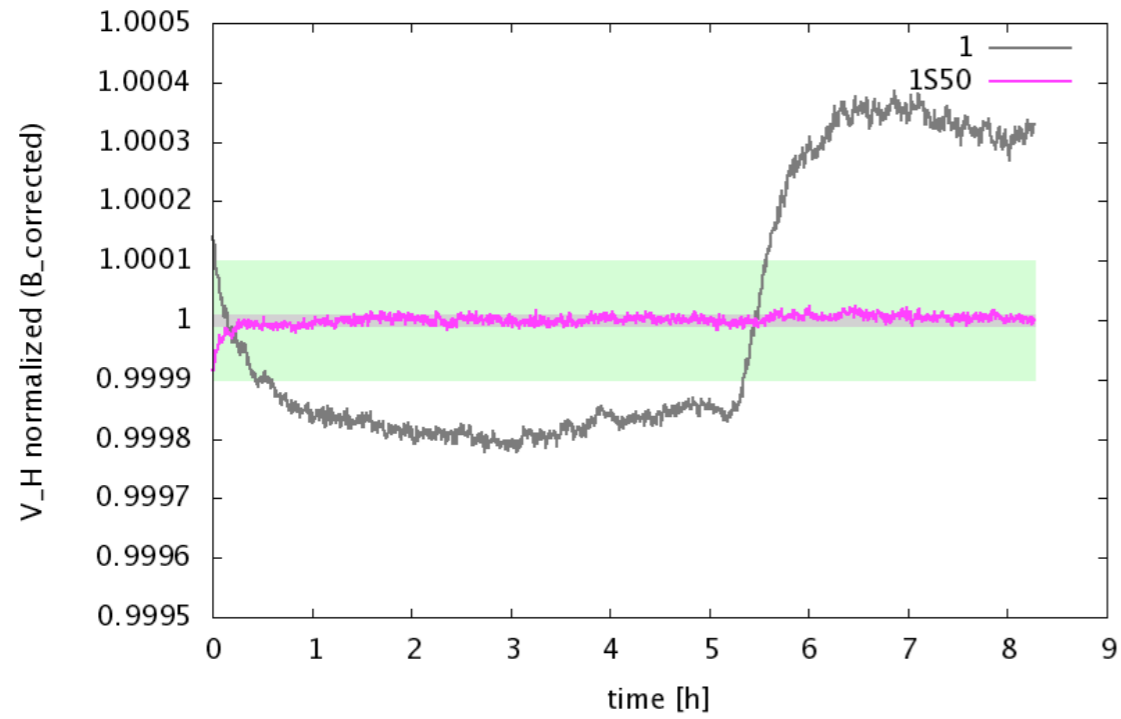
To do:

- Confirm necessity for SiN_x, optically inspect SiN_x quality, check repeatability
- Change material, cruciform dimensions

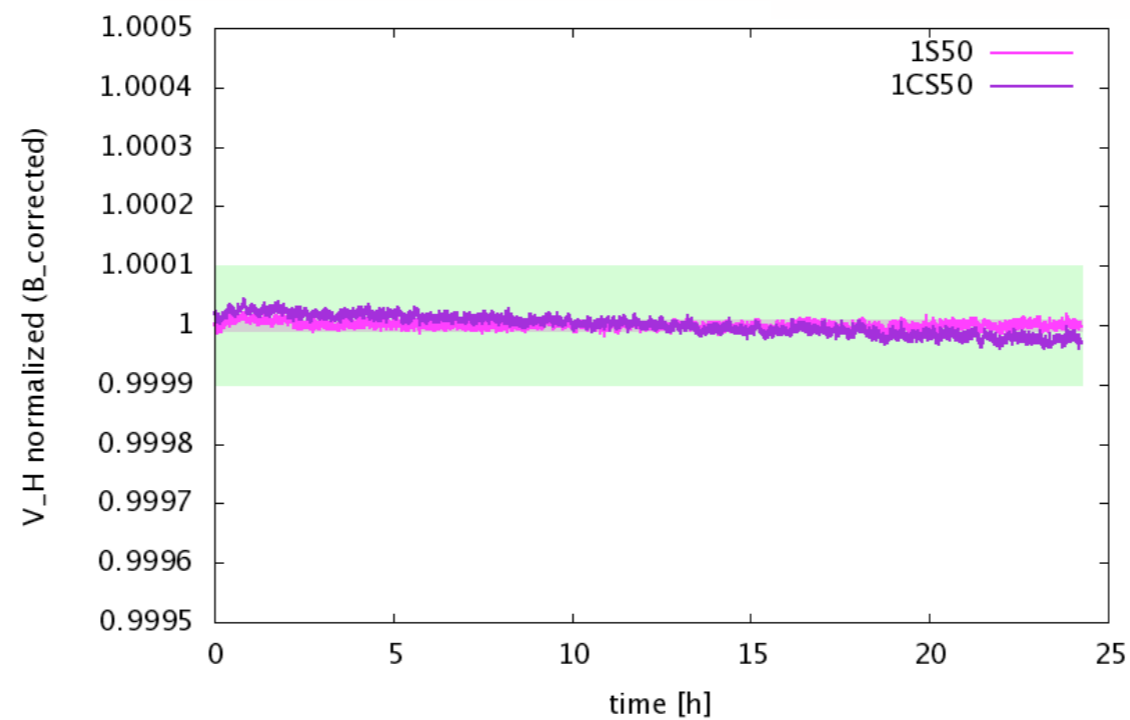
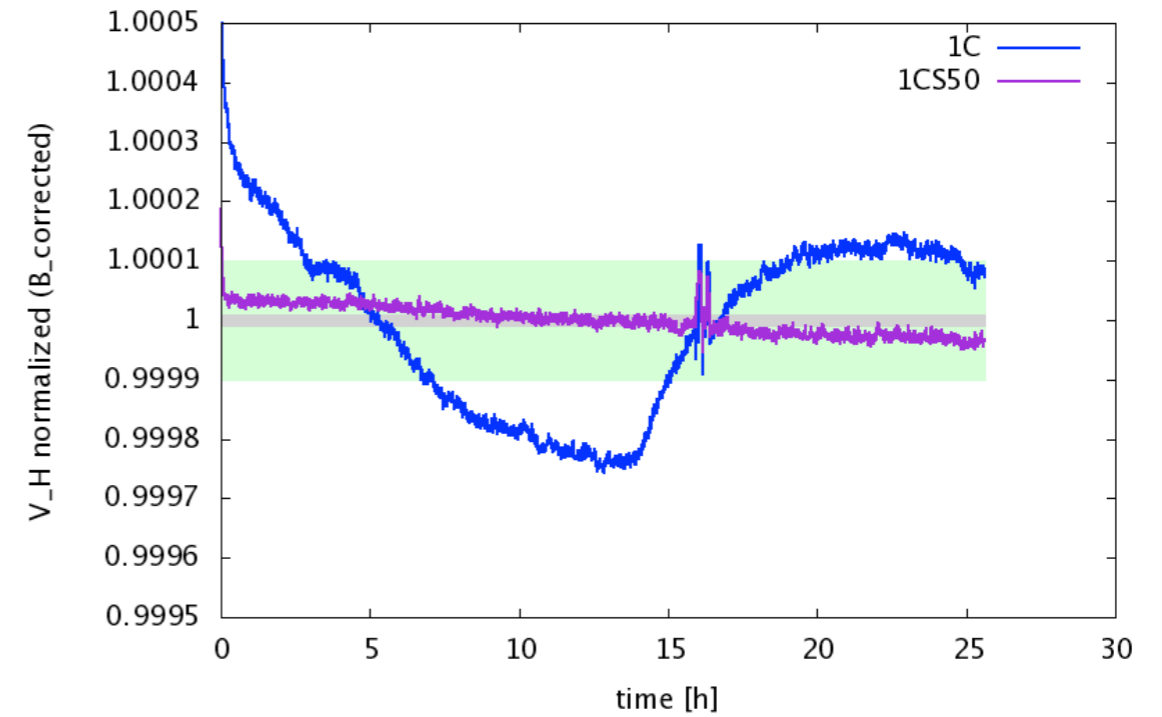
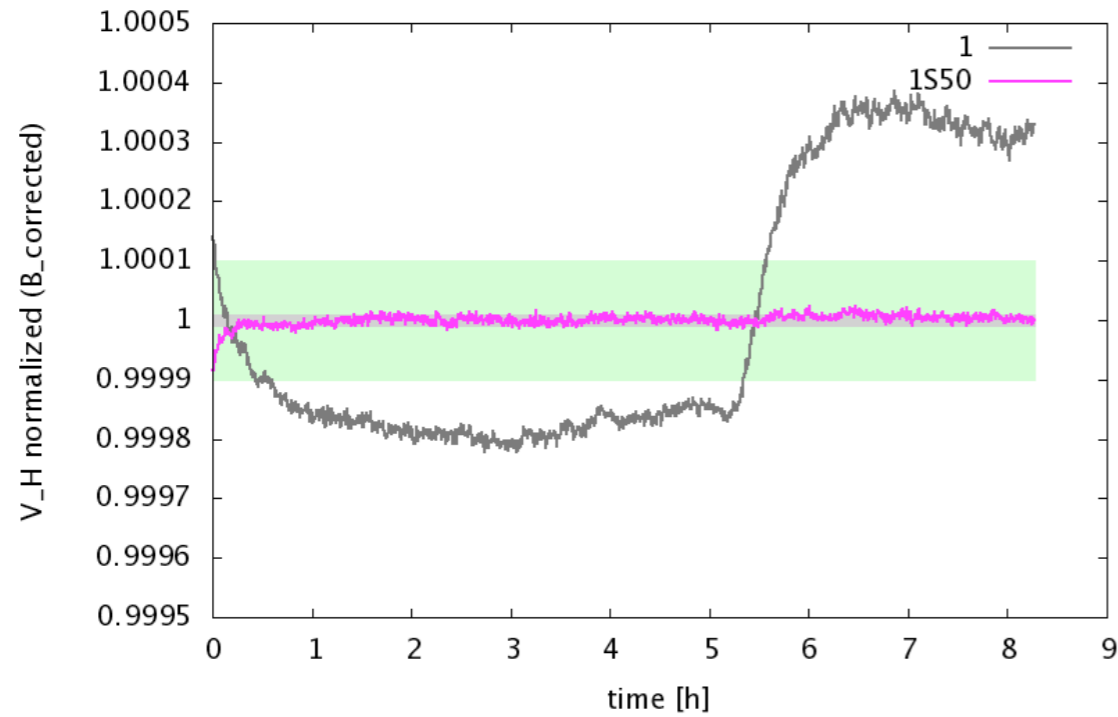
Effect of intact SiN_x passivation



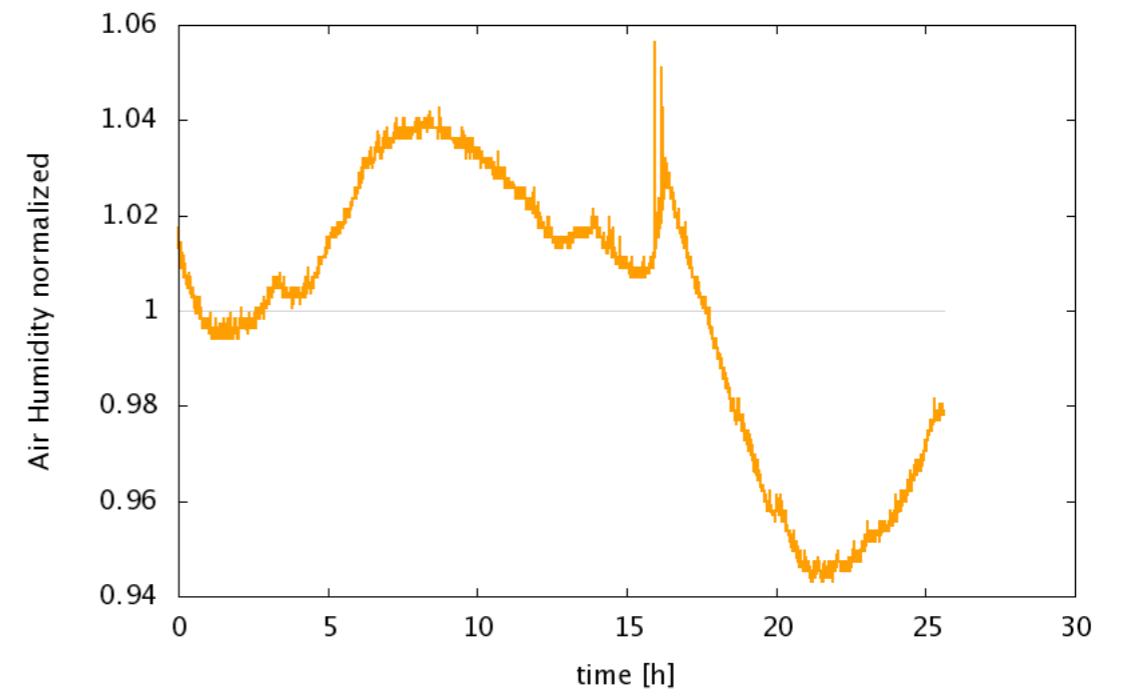
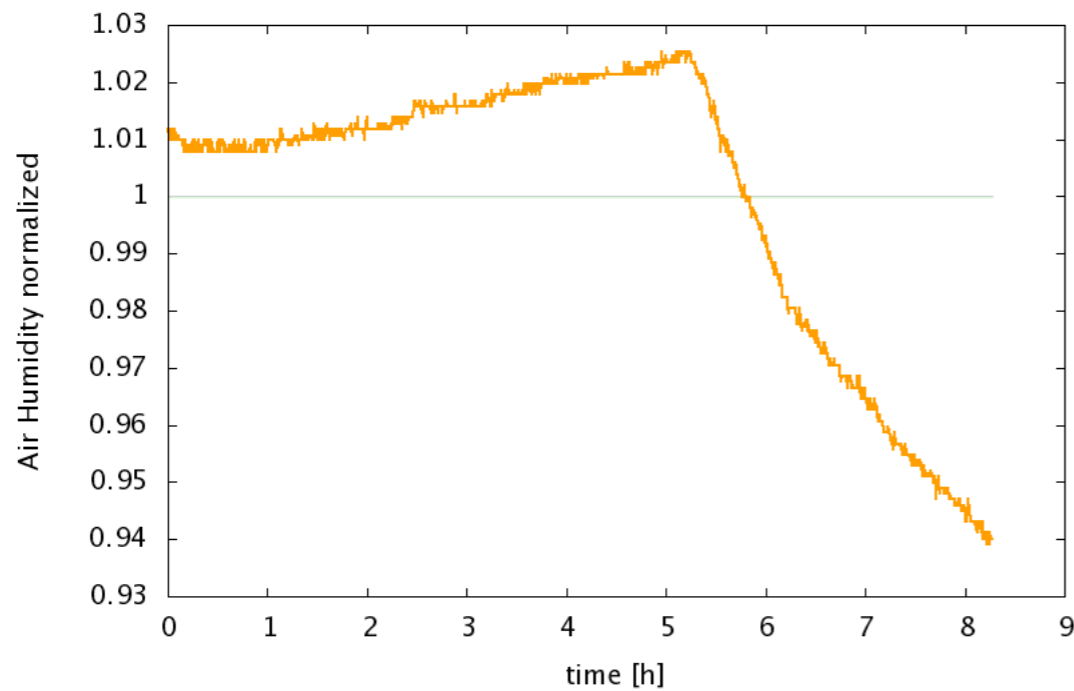
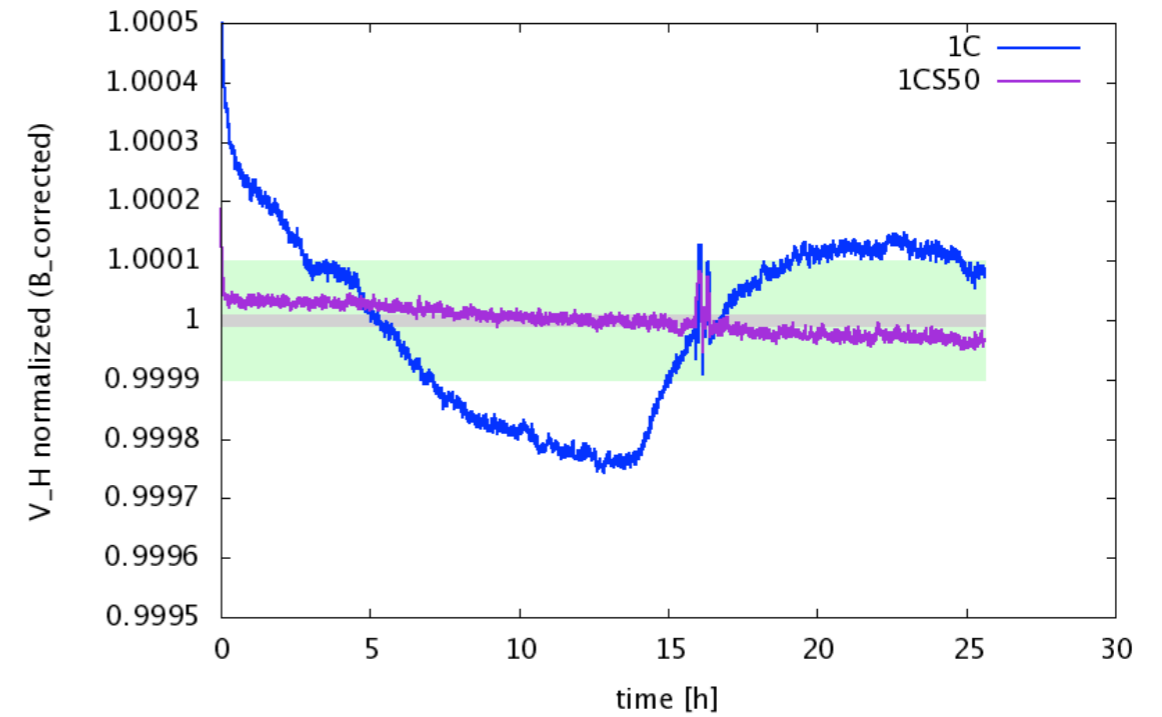
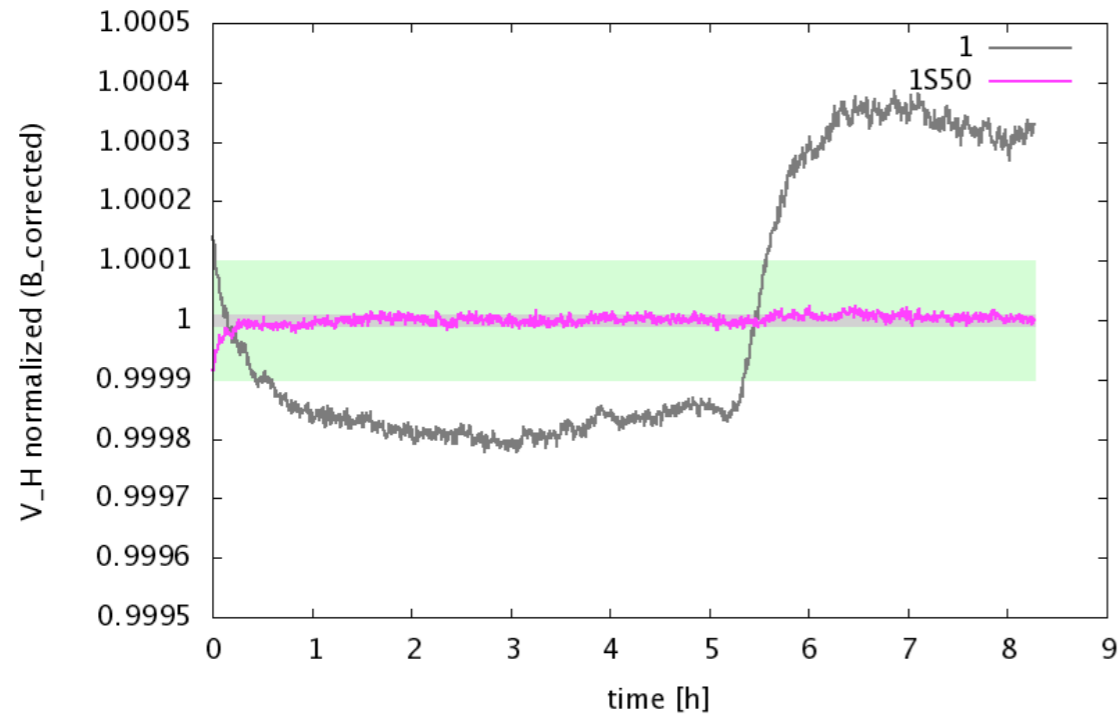
GaAs cap layer/no cap layer



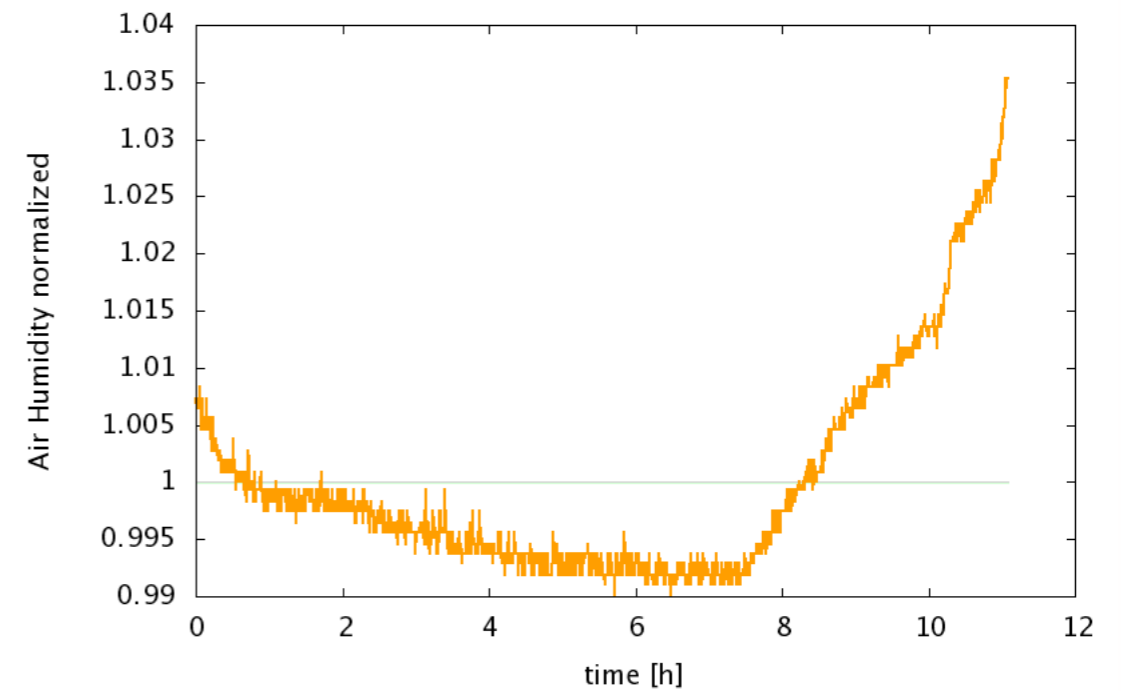
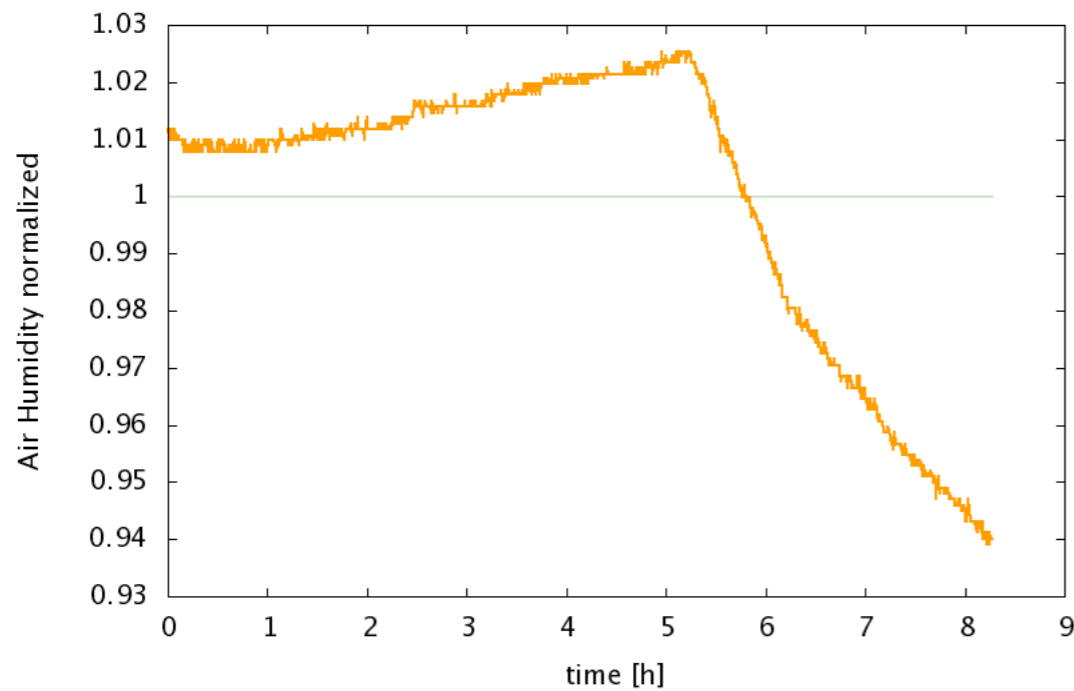
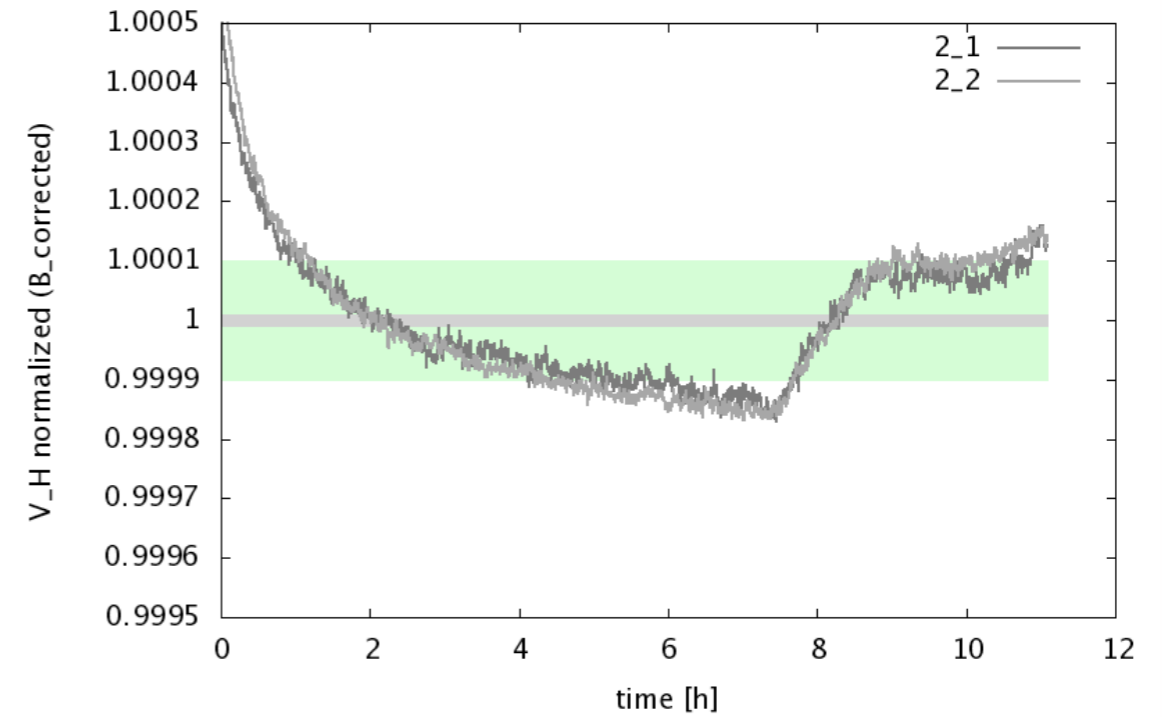
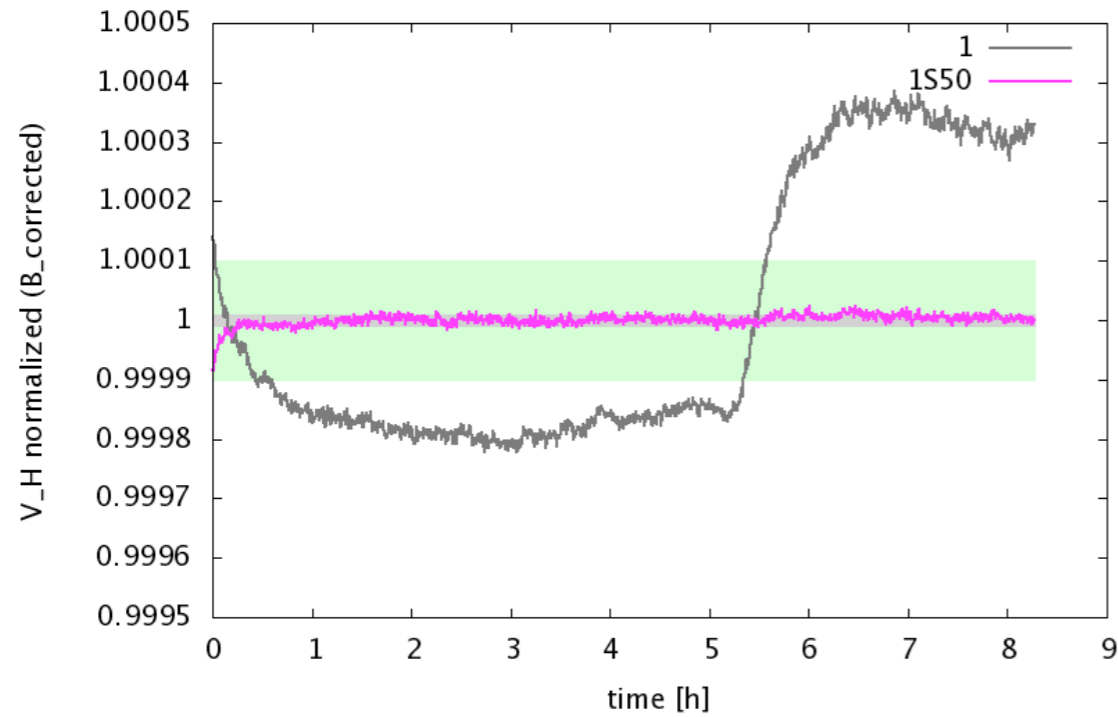
GaAs cap layer/no cap layer



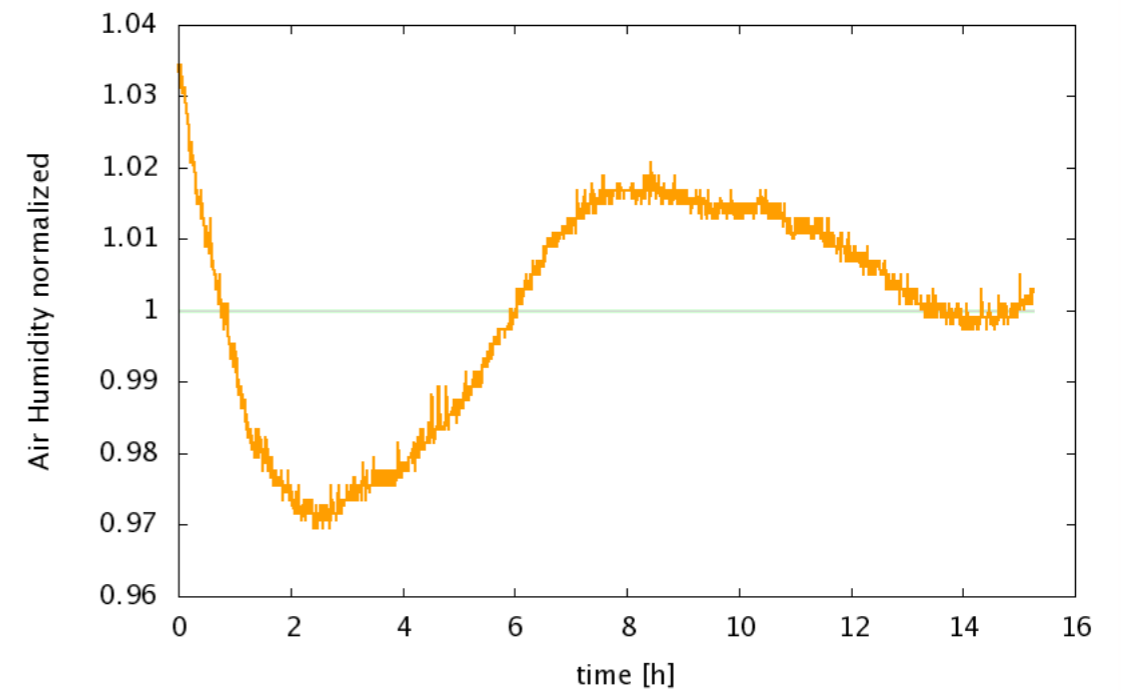
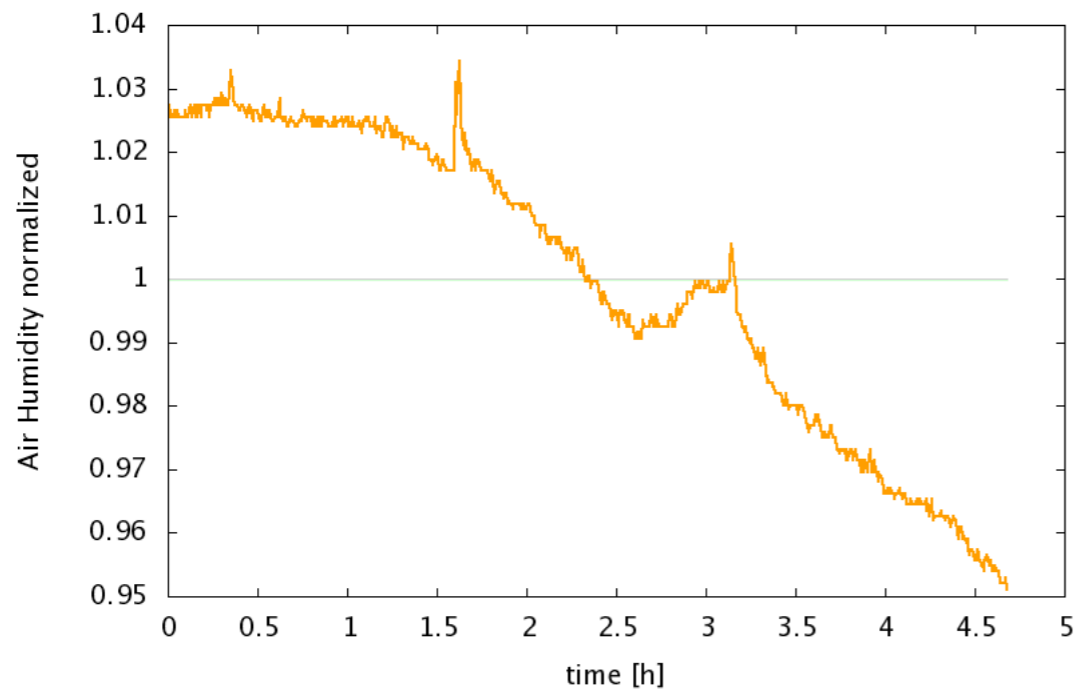
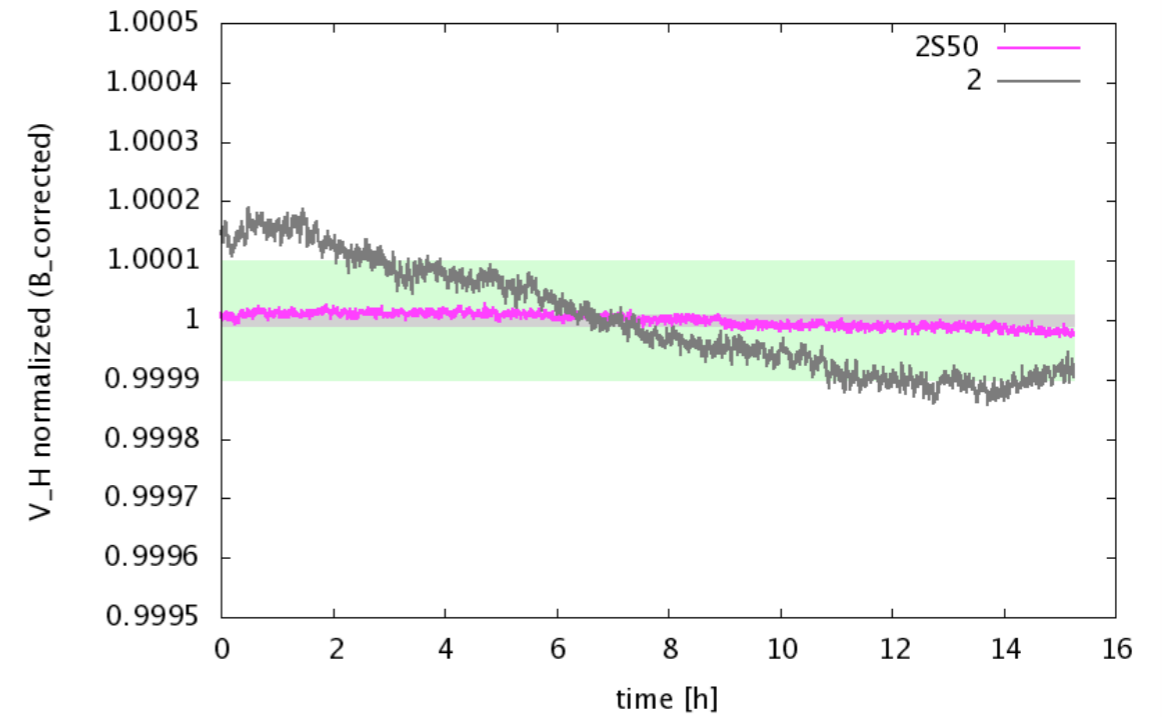
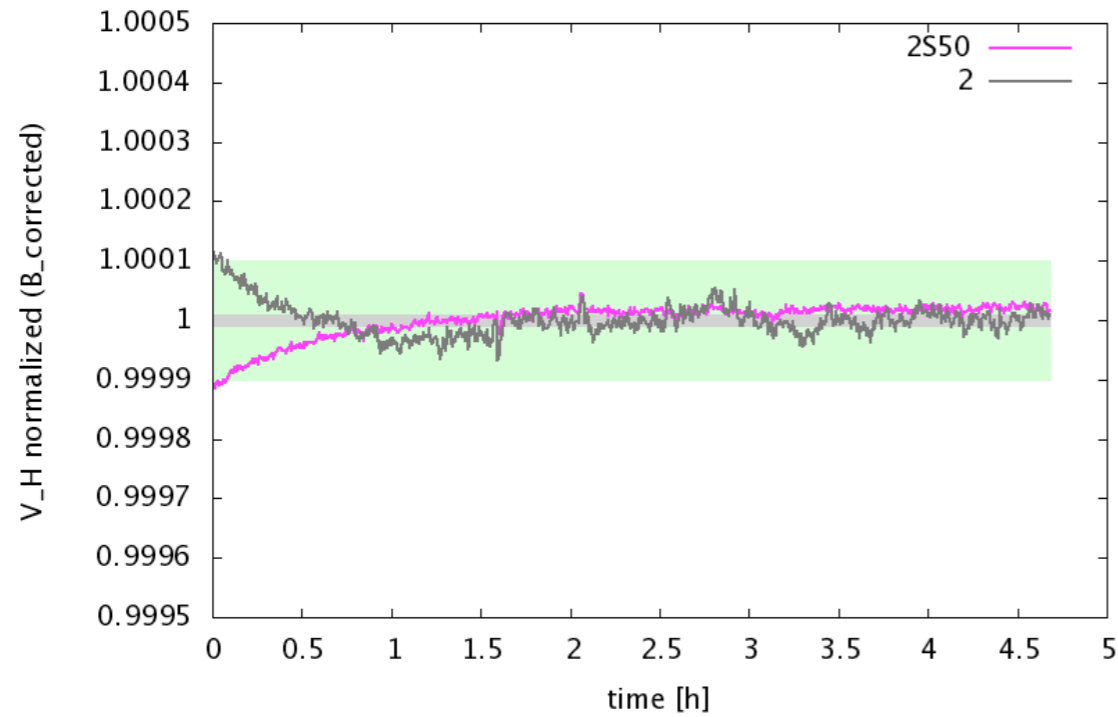
Humidity effect?



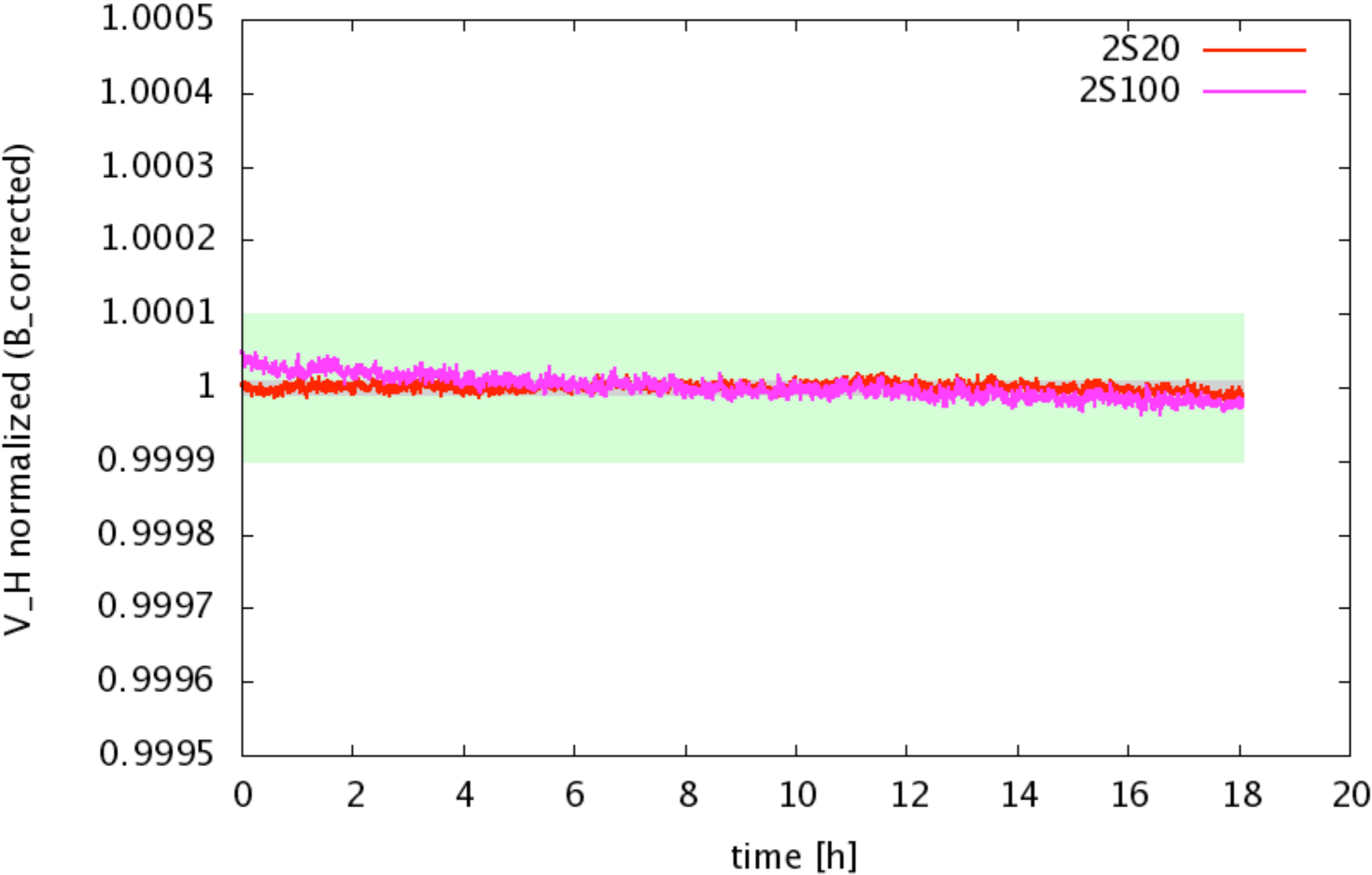
Humidity effect?



Humidity effect?



Thickness of SiN_x layer



Conclusions

- SiN_x (PECVD 300 °C) is crucial for long-term stability of the constituent GaAs Hall sensors in the Hallcube.
- Soldering at elevated temperature (in my case 400 °C) can severely degrade the of SiN_x layer and its passivation effect.
- (Insulated) Wire-bonding should be explored as an alternative to soldering.
- Removal of the GaAs cap layer seemingly has a further positive effect on sensor stability
- The SiN_x passivation layer should be <100 nm thick.
- No “ideal” thickness, if it exists, for SiN can be given yet from minimal testing.
- Sensor concept adaptable and also independent on semiconductor material, custom-made solutions possible.

- New, revised Hallcube version should be built now, parts have arrived (still confidential).

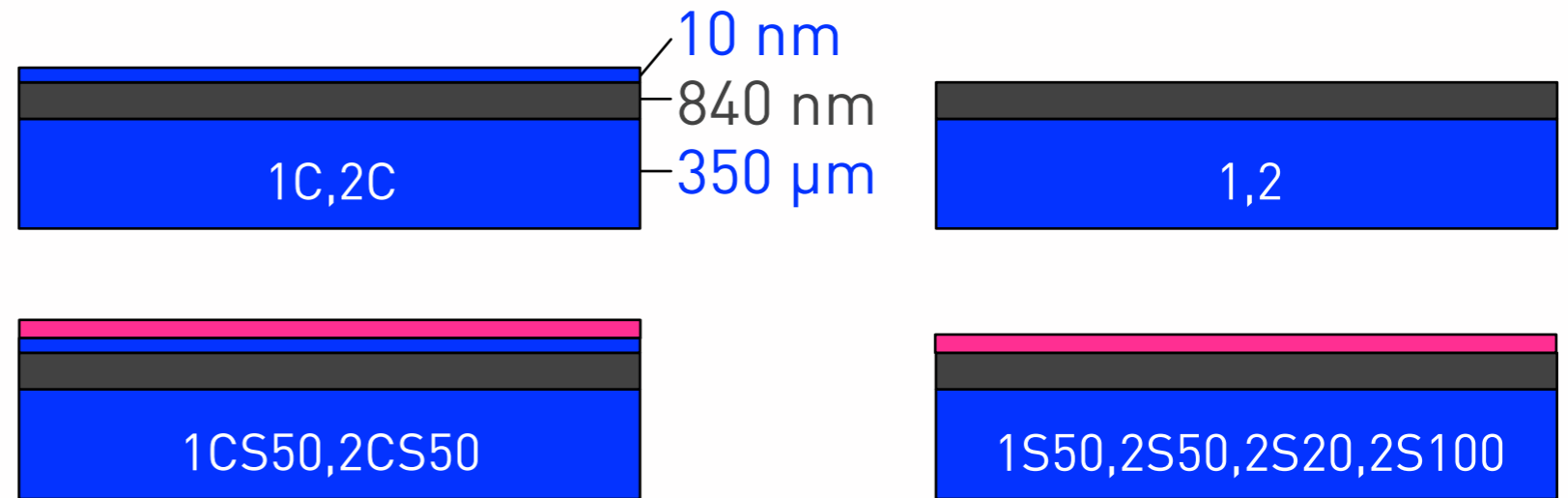
Approach

HPF6a wafer

■ Semi-insulating GaAs

■ n-type GaAs (Si: $n \approx 10^{17} \text{ cm}^{-3}$)

■ SiN_x



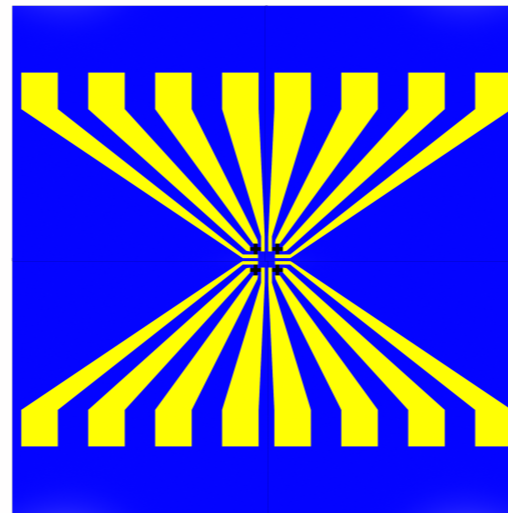
Repeatability on/among chip(s)

10 x 4 = 40 Hall crosses

- 1, 1S50, 1C, 1CS50
- 2, 2S50, 2C, 2CS50
- 2S20, 2S100

“C”: Cap, “S”: SiN_x, “50”: 50 nm

Lost during processing: 2C, 3/4 of 2S50



Cap/mesa etch: piranha

SiN_x deposition: PECVD 300 °C

Ohmics: GeAuCrAu (e-beam evaporation)

“Packaging”: epoxy, pcb, wire-bond

Considerations

Periodic field  high gradients, in this case up to 75 Tm^{-1}

PHE compensation?

200 μm spatial separation of Hall sensors

 150 Gauss difference in in-plane field component

Error < 0.3 Gauss and due to averaging < 0.15 Gauss

Interpolation error?

For $d = 200 \mu\text{m}$ and for a tolerable error of 10^{-4} : fields up to 10.000 Tm^{-2}

getting close: 9475 Tm^{-2}

Measurement scheme U50

$$B_y = B_{\max} \sin\left(\frac{2\pi z}{\lambda}\right)$$

0.6 T 50 mm

at any position s along z :

$$B_{\text{avg}} = \frac{1}{\Delta} \int_{s-\frac{\Delta}{2}}^{s+\frac{\Delta}{2}} B_{\max} \sin\left(\frac{2\pi z}{\lambda}\right) dz \qquad B_{z=s} = B_{\max} \sin\left(\frac{2\pi s}{\lambda}\right)$$

$B_{\text{avg}} - B_{z=s}$ max at $s = \lambda/4$

$B_{\text{avg}} - B_{z=s} < 0.1$ Gauss for $\Delta < 160 \mu\text{m}$

for Hall voltage integration time 20 ms: $v_{\max} = 8 \text{ mm/s}$

Hall sensor data acquisition:

$I_{\text{Hall}} = 0.1\text{mA}$ (Keithley 6221)

Hall voltages read by Agilent 3458A voltmeters

$v_{\text{scan}} = 2.1 \text{ mm/s}$

External trigger every $112 \mu\text{m}$ (5000 points in 560 mm)

$x = 0, \pm 0.5 \text{ mm}$

$y = 0, \pm 0.125 \text{ mm}$

$z = 0-560 \text{ mm}$